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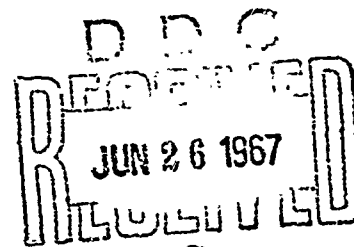
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RESULTS ON LOCATION AND SCALE PARAMETER ESTIMATION WITH APPLICATION TO THE EXTREME-VALUE DISTRIBUTION

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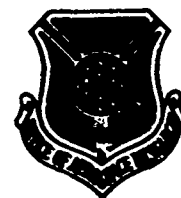
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**AEROSPACE RESEARCH LABORATORIES
OFFICE OF AEROSPACE RESEARCH
UNITED STATES AIR FORCE
WRIGHT-PATTERSON AIR FORCE BASE, OHIO**

FOREWORD

The major portion of the work summarized in this interim technical report was sponsored by the Aerospace Research Laboratories, Office of Aerospace Research, United States Air Force, Wright-Patterson Air Force Base, Ohio under Contract AF33(615)-2818. Work on this contract, technically monitored by Dr. H. L. Harter, is documented under Project 7071, Research in Applied Mathematics. The tables for obtaining the best linear invariant estimates of parameters of the extreme-value distribution which appear in Appendix C were calculated under the auspices of the Reliability Subdivision of the Liquid Rocket Division at Rocketdyne, with the support of Contract NAS 8-19 (J2 Engine System Development). The initial work on the tables appearing in Appendix D was also performed under the NAS contract.

ABSTRACT

This report gives results concerning estimation of location and scale parameters. Most of the work pertains to the first extreme-value distribution of smallest values, the distribution of the natural logarithms of failure times having the two-parameter Weibull distribution. Experimental designs are derived, under the assumption that log failure times are polynomial functions of the reciprocal of stress level and have the extreme-value distribution, for over-stress life tests. These designs yield least-squares curves with minimum variance at a specified (nominal) stress level below the levels at which the life test is conducted. An estimate of the extreme-value location parameter u associated with the nominal stress level and the relationship between u and stress level can be obtained from the least-squares curve. Other extreme-value results apply to a life test conducted at a single fixed stress level.

Interval estimators (confidence bounds) are derived for the extreme-value scale parameter b and for any location parameter of the form $x_R = u + b \log \log(1/R)$ where R is specified (the $100(1-R)$ percent point of the distribution). The bounds for b and x_R are, respectively, based on two and three of the first m extreme-value order statistics, $X_1, \leq X_2, \dots, \leq X_m$, and are of the form $k_b(X_q - X_p)$ and $X_v + k_R(X_q - X_p)$. For each combination of values of sample size n , censoring number m , confidence level $1-\alpha$, and survival proportion R , an optimum choice of p, q , and v has been made. The criterion used in the selection is that the expected squared deviation of the bound from the parameter should be minimized. For samples up to size 22, values of the constant k_b corresponding to the optimum combination of p and q are presented. Tables of values of k_R are also in preparation.

For $2 \leq n \leq 25$, $2 \leq m \leq n$, tables are given for estimating b and x_R , where the estimator is best among linear estimators with expected loss invariant under translations. These best linear invariant (BLI) estimators have uniformly smaller expected loss than the Gauss-Markov best linear unbiased (BLU) estimators and are simple linear functions of the BLU estimators.

Expressions are derived for Cramér-Rao bounds for invariant estimators of general location and scale parameters. These bounds are applied to the extreme-value distribution, and compared with the expected losses of BLI and BLU estimators of u , b , and x_R , for certain values of R , for $2 \leq n \leq 25$, $2 \leq m \leq n$.

The one problem considered which concerns the Gaussian rather than the extreme-value distribution is the outlier problem for a size-three sample. One approach to the problem involves a simplified Bayesian analysis. This leads to recommendations for estimators of the Gaussian location parameter which depend only on the observations and a prior probability that the largest (or smallest) observed value is an outlier.

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EXTREME-VALUE DISTRIBUTION

EVALUATION OF CONFIDENCE BOUNDS FOR DISTRIBUTION PERCENTAGE POINTS AND FOR THE SCALE PARAMETER

Appendix B gives an analysis of the problem of obtaining confidence bounds on reliability parameters when the natural logarithms of failure times have the Type I extreme-value distribution of smallest values, and $(n-m)/n$ of the size n sample of ordered observations is censored from above. Exact lower confidence bounds on log reliable life x_R (the $100(1-R)$ percent point, where R is a specified survival proportion) are derived. These have smallest mean squared deviation from x_R among bounds of a specified form based on three order statistics only. The computer program and various subroutines for generating the tables for obtaining these bounds have been written. The subroutines, which perform the numerical integration for calculating distribution percentage points, calculate the risk (the expected squared deviation) of the bounds, read from tape the expected values, variances, and covariances of the reduced extreme-value order statistics, generate first guesses for percentage points, sort and order the risks for the various combinations of order statistics, etc., are all working as desired. The calculations based on the program will be made on the Wright-Patterson direct-coupled system due to the fact that a great deal of computer time will be required. This is true even though an approximation is being made in order to decrease substantially the number of distribution percentage points which will be calculated. If no such approximation is made, then for each combination of confidence level γ and specified R there are 20,615 percentiles which must be calculated, if only sample sizes 2, 3, ..., 20 are considered. Since several seconds, at

least, appear to be required for calculating each percentage point, it might take well over 2 days of computer time to determine the necessary values if only 2 values each of γ and R are considered.

It has therefore been decided to choose the three order statistics on which to base the bounds before calculating any percentage points. For each combination of sample size n , censoring number m , and specified survival proportion R , the estimator of x_R with smallest risk among those based on a linear combination, with risk invariant under translations, of one order statistic and the difference of two order statistics will be selected. The three order statistics specified by this estimation rule will then provide the basis for bounds at all confidence levels for each corresponding combination of m , n , and R . Indications are that very little increase in risk for the bounds will result from this procedure; and the number of computations will be decreased by a factor of over 100.

There is no apparent method of comparing the bounds directly with bounds, such as those obtained by Monte Carlo procedures by Johns and Lieberman [3], based on all of the first m order statistics. It is possible, however, to compare the risks for the three-order-statistic estimators described above with those of the best linear invariant (BLI) estimators, approximations to which form the basis for the bounds obtained by Johns and Lieberman. This has been done for sample sizes 2, 3, ..., 17, and demonstrates that the ratio of the risks of the BLI estimator and the best three-order-statistic estimator of $x_{.90}$ as described above is 0.877 for n as large as 17 and m equal to n . Ratios of this type are being determined for certain combinations of n , m , R , and will appear in a future report. Also included will be ratios of risks of the BLI estimator and the best estimator

of the extreme-value scale parameter b based on the two order statistics yielding the bound with smallest risk, for certain combinations of n , m , and γ .

Table B.I, which provides the means for calculation of the upper confidence bounds on b with smallest mean squared deviation from b among bounds based on two order statistics only, is included in Appendix B. At the same time distribution percentage points were being calculated as a basis for Table B.I, the power function of the tests associated with the bounds were also calculated for three prescribed values of b/b_0 (where the hypothesis tested is $H: b \geq b_0$). The calculations showed that the two-order-statistic bound with smallest risk seems to be either uniformly most powerful, locally most powerful, or most powerful for b/b_0 close to zero among two-order-statistic bounds. Moreover, when another two-order-statistic bound has greater power than the one with smallest risk for one of the prescribed values of b/b_0 , the difference between the calculated values of the two is almost negligible.

CRAMÉR-RAO EFFICIENCIES OF BEST LINEAR INVARIANT ESTIMATORS

The paper included as Appendix D gives the derivation of Cramér-Rao type bounds for invariant estimators of a scale parameter θ_2 and location parameters of the form $\theta_1 + k\theta_2$, where (θ_1, θ_2) is a location-scale parameter (that is, $f_{\theta_1, \theta_2}(x) = \frac{1}{\theta_2} g\left(\frac{x-\theta_1}{\theta_2}\right)$, for some g). These bounds, which are appropriate for the case in which any proportion of the sample observations may be censored, are shown to be functions of the bounds for unbiased estimators. They are applied specifically to invariant estimators of percentage points of the first extreme-value distribution of smallest values

for the case in which $(n-m)/n$ of a size n sample of ordered observations is censored from above. The Cramér-Rao efficiencies of the best linear invariant estimators are then tabulated (see Table D.III) for the 10 percent point (reliable life for a specified survival proportion R of 0.90) and $2 \leq n \leq 18$. Also tabulated on the basis of previous computations and the derived result (see Table D.I and Table D.II) are the mean squared errors of the best linear invariant and the best linear unbiased estimators, along with their respective Cramér-Rao bounds, for the extreme-value location parameter u , for the scale parameter b , and for the first and tenth percentiles of the distribution.

This paper was written as an extra task under the contract for the symposium on reliability and life-testing presented by the Society for Industrial and Applied Mathematics (SIAM) in Seattle, November 14-15, 1965. A special issue of the journal of the society was planned to include many of the papers presented at the symposium, and this material was submitted for consideration. The plans for the special issue were apparently dropped, however, so that the paper was accepted for publication in a regular issue of the SIAM Journal, subject to a few revisions in the introduction and an incorporation of the appendices into the body of the paper. Also, Table D.I and Table D.II will not be included. The elimination of these two tables provides part of the motivation for including this paper in this report, since, for example, there is no source other than Table D.II from which one may directly obtain the variances of the best linear unbiased estimators of the extreme-value parameters for $n = 21, 22, \dots, 25$. (They may be obtained indirectly from Table D.I or from Table C.I in Appendix C). The values of the two types of bounds, too, are of interest for comparison with each other and with the risks of other types of estimators.

TABLES FOR OBTAINING BEST LINEAR INVARIANT ESTIMATES

The entries for Table C.I, which appears in Appendix C, are based on computations made in part at the Health Sciences Computing Facility at the University of California at Los Angeles and in part at Rocketdyne, under the auspices of the Liquid Rocket Division with the support of Contract NAS 8-19. The values computed at that time (weights for obtaining best linear unbiased estimates of extreme-value parameters) were modified according to theory recently derived to obtain the weights for the best linear invariant (BLI) estimates. These weights for the BLI estimates were then published as part of a Rocketdyne research report under the contract. The report is included here because it has elicited considerable interest and appears to warrant a wide distribution. The paper has been submitted for publication but may present something of a problem in this respect because of the length of the tables.

DESIGN OF OVER-STRESS LIFE-TEST EXPERIMENTS

Appendix A gives the derivation of results specifying designs with certain optimum properties for life-test experiments under particular assumptions concerning the failure times of the population of items under consideration. A two-parameter Weibull model is assumed for the probability density function of the failure times; and further it is supposed that the logarithm of failure time is a polynomial function of the reciprocal of stress level. Finally, it is assumed that the level of stress to which the population of items being considered is subjected during normal usage (the nominal stress level), is not sufficient to produce a failure of an item within any reasonable amount of time after the application of the stress. Thus it is supposed that the life test,

which will allow one to estimate certain properties of the distribution of the failure times at the nominal stress level, is conducted at levels above nominal stress.

The designs derived under these assumptions specify where (at what stress levels) within a given interval of stress the life tests should be conducted and what proportion of the total number of items should be assigned to each testing level when all of the items are tested until failure and when least-squares estimation procedures are to be applied. Certain properties are demonstrated for the least-squares curve at the various testing levels and at the nominal stress level when a design of the form derived is used.

It should be noted that the assumption originally proposed for this task concerning a change of level of stress applied to an item during a life test was not incorporated in this work. The reason for this was the fact that the following became apparent after some analysis. For testing at various stress levels where any failure-time distribution parameter depends upon stress level, it is not possible to estimate such a parameter efficiently at any level unless the relationship between the parameter and the stress level can also be estimated. When stress level is changed during testing, it is not clear how one should determine or define the actual stress which has been applied to produce the failure. In other words, the testing level is not actually defined for this situation so that it is not possible to estimate the relationship between stress level and failure-time parameters.

THE OUTLIER PROBLEM FOR SAMPLES OF SIZE THREE

DEFINITION OF THE PROBLEM

Suppose three observations on a normally distributed random variable are made, and the largest (or smallest) is suspected of being an outlier. The chemist's approach to the problem of estimating the mean μ of the distribution has traditionally been to discard the observed value of the possible outlier and average the other two values. Use of a Winsorized estimator of μ , often recommended when outlying values are suspect, involves changing the observed value of the outlier to the value of the second ordered observation, and then averaging all three values. Sometimes the median of the three observations is used. Clearly, if the suspected value is not an outlier, or if the amount by which it is displaced is very small compared with the distribution standard deviation then the arithmetic mean of all three observed values is best for estimating μ . What if, however, the amount of displacement is moderate or large or there is a fairly high probability that the observation in question is an outlier? The following analysis gives some insight into this problem.

COMPARISON OF ESTIMATORS FOR THE MEAN

Assume that $Y_1 \leq Y_2 < Y_3$, and that either $\theta_0: Y_1, Y_2$, and Y_3 are order statistics from $N(\mu, \sigma)$, or $\theta_\Delta: Y_1$ and Y_2 are order statistics from $N(\mu, \sigma)$ and Y_3 is a size 2 sample from $N(\mu + \Delta, \sigma)$. Because of the symmetry of the distribution, the case in which Y_1 is the observation which is suspect can also be handled.) The risk (expected loss, where loss is squared error divided by σ^2) can then be calculated for any estimator under the two alternatives θ_0 and θ_Δ . All values given below are correct to within a unit in the final decimal place shown. Values which are exact are given in fractional form. The moments of the normal

order statistics used to calculate these values appear in [4].

Consider $\hat{\mu}_0 = \frac{1}{3}(Y_1 + Y_2 + Y_3)$

$$\hat{\mu}_1 = \frac{1}{2}(Y_1 + Y_2)$$

$$\hat{\mu}_2 = \frac{1}{3}(Y_1 + 2Y_2)$$

and $\hat{\mu}_3 = Y_2$.

If $R_k(\mu, \hat{\mu}_j)$ is the risk for estimator $\hat{\mu}_j$ ($j=0,1,2,3$) when θ_k ($k=0$ or Δ) is true, then

$$R_0(\mu, \hat{\mu}_0) = \frac{1}{3}$$

$$R_\Delta(\mu, \hat{\mu}_0) = \frac{1}{3} + \Delta^2/9\sigma^2$$

$$R_0(\mu, \hat{\mu}_1) = .569$$

$$R_\Delta(\mu, \hat{\mu}_1) = \frac{1}{2}$$

$$R_0(\mu, \hat{\mu}_2) = .464$$

$$R_\Delta(\mu, \hat{\mu}_2) = .556$$

$$R_0(\mu, \hat{\mu}_3) = .449$$

$$R_\Delta(\mu, \hat{\mu}_3) = 1$$

Of the three estimators $\hat{\mu}_1, \hat{\mu}_2$, and $\hat{\mu}_3$, $\hat{\mu}_2$ has minimax risk (minimizes the maximum risk for all Δ, μ , and σ). It is not the true minimax estimator, however. Assume σ is not known and consider all estimators which are linear functions of Y_1 and Y_2 and which have expected loss independent of μ and σ . These linear invariant estimators will be of the form $\hat{\mu}(a_1) = a_1 Y_1 + (1-a_1) Y_2$ [5].

When θ_0 is true, the best linear unbiased estimators of μ and σ based on Y_1 and Y_2 are simply $\mu_0^* = Y_2$ and $\sigma_0^* = 1.1816 (Y_2 - Y_1)$

with the variances and covariance of these estimators respectively given by $V(\mu_o^*) = .4487\sigma^2 \equiv A_o\sigma^2$, $V(\sigma_o^*) = .6378\sigma^2 \equiv C_o\sigma^2$, $C(\mu_o^*, \sigma_o^*) = .2044\sigma^2 \equiv B_o\sigma^2$. Thus, by the results in [], when θ_o is true the best linear invariant estimator based on Y_1 and Y_2 is $\tilde{\mu}_o = \mu_o^* - [B_o/(1 + C_o)]\sigma_o^*$ $= .1475Y_1 + .8525Y_2$. When θ_Δ is true $\mu_\Delta^* = \hat{\mu}_1 = \frac{1}{2}(Y_1 + Y_2)$ and $\sigma_\Delta^* = -.8862Y_1 + .8862Y_2$ are, respectively, the best linear unbiased estimators of μ and σ . Since the covariance $B_\Delta\sigma^2$ of μ_Δ^* and σ_Δ^* is equal to zero, the best linear invariant estimator $\tilde{\mu}_\Delta$ based on Y_1 and Y_2 for θ_Δ true is equal to μ_Δ^* . The risk $R_k(\mu, \tilde{\mu}_j)$ for $\tilde{\mu}_j$ when $\theta_k(j, k=0, \Delta)$ is true is given as follows

$$R_o(\mu, \tilde{\mu}_o) = .423$$

$$R_\Delta(\mu, \tilde{\mu}_o) = .748$$

$$R_o(\mu, \tilde{\mu}_\Delta) = .569$$

$$R_\Delta(\mu, \tilde{\mu}_\Delta) = \frac{1}{2}$$

Now, since $\tilde{\mu}_o$ is not equal to $\tilde{\mu}_\Delta$, which would imply $R_o(\mu, \tilde{\mu}_o) = R_o(\mu, \tilde{\mu}_\Delta)$ and $R_\Delta(\mu, \tilde{\mu}_o) = R_\Delta(\mu, \tilde{\mu}_\Delta)$, there is no guarantee that $\tilde{\mu}_\Delta$ has minimax risk among all linear functions of the form $\hat{\mu}(a_1)$. In fact, $\tilde{\mu}_\Delta = \hat{\mu}_1$ has larger maximum risk than $\hat{\mu}_2$, as was noted earlier. Define $\hat{\mu}_4$ to be the minimax-risk linear invariant estimator, that is, the one such that $\max[R_o(\mu, \hat{\mu}_4), R_\Delta(\mu, \hat{\mu}_4)]$ is the minimum of $\max[R_o(\mu, \hat{\mu}(a_1)), R_\Delta(\mu, \hat{\mu}(a_1))]$, $-\infty < a_1 < \infty$. The maximum risk of $\hat{\mu}_4$ can be no smaller than $\max[R_o(\mu, \tilde{\mu}_o), R_\Delta(\mu, \tilde{\mu}_\Delta)] = R_\Delta(\mu, \hat{\mu}(1/2)) = \frac{1}{2}$. Furthermore, $R_o(\mu, \hat{\mu}(a_1))$ and $R_\Delta(\mu, \hat{\mu}(a_1))$ are continuous quadratic

functions of a_1 , each with a unique minimum. Therefore, if the value \bar{a}_1 of a_1 defined by

$$R_0(\mu, \hat{\mu}(\bar{a}_1)) = R_\Delta(\mu, \hat{\mu}(\bar{a}_1)) \quad (1)$$

is such that $.1475 < \bar{a}_1 < \frac{1}{2}$ (note that $\bar{\mu}_0 = \hat{\mu}(.1475)$ and $\bar{\mu}_\Delta = \hat{\mu}(1/2)$), then $\hat{\mu}(\bar{a}_1)$ is the minimax estimator $\hat{\mu}_4$. Solution of equation (1) gives $\bar{a}_1 = .42265$. Therefore, $\hat{\mu}(\bar{a}_1) = \hat{\mu}_4 = .42265Y_1 + .57735Y_2$, with $R_0(\mu, \hat{\mu}_4) = R_\Delta(\mu, \hat{\mu}_4) = .512$. Moreover, $\hat{\mu}_4$ can be expressed as $.5(Y_1 + Y_2) + .0830[.8862(Y_2 - Y_1)] = \mu_\Delta^* + .0830\sigma_\Delta^*$, with σ_Δ^* equivalent to the unique best unbiased estimator of σ for sample size 2. Therefore, for θ_Δ true, distribution percentage points of $\frac{\hat{\mu}_4 - \mu}{\sigma^*}$ can be calculated from percentage points of the central t distribution.

In a real situation one might not want to use the minimax estimator, particularly if $|\Delta/\sigma|$ is apt to be small. A simplified Bayesian analysis may be employed to gain insight into how large $|\Delta/\sigma|$ must be before one would prefer another estimator to $\hat{\mu}_0$. Let γ be the prior probability of situation θ_Δ , with $|\Delta/\sigma|$ fixed, and $1-\gamma$ the probability of θ_0 . For comparative purposes the estimators $\hat{\mu}_0, \hat{\mu}_1, \hat{\mu}_2, \hat{\mu}_3$, and $\hat{\mu}_4$ will be used.

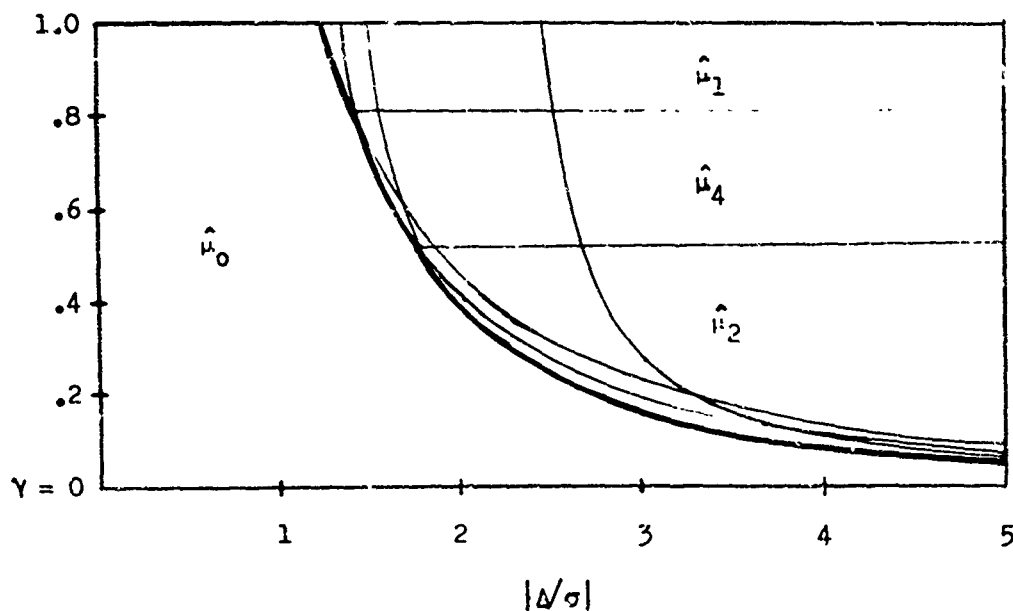
The risk using the estimator $\hat{\mu}_0$ is $1/3$ with probability $1-\gamma$ and $1/3 + \Delta^2/9\sigma^2$ with probability γ . The risk function for $\hat{\mu}_0$ can thus

be expressed as a function of γ and Δ , $R(\mu, \hat{\mu}_0, \gamma, \Delta) = 1/3 + \gamma(\Delta^2/9\sigma^2)$.
 For $\hat{\mu}_i$, $i=1,2,3,4$, the risk function $R(\mu, \hat{\mu}_i, \gamma, \Delta)$ is independent of Δ and can be expressed in terms of γ alone:

i	$R(\mu, \hat{\mu}_i, \gamma, \Delta)$
0	$1/3 + \gamma\Delta^2/9\sigma^2$
1	$.569 - .070\gamma$
2	$.464 + .092\gamma$
3	$.449 + .551\gamma$
4	$.512$

The last four of these expressions indicate the following: Of the estimators $\hat{\mu}_1, \hat{\mu}_2, \hat{\mu}_3, \hat{\mu}_4, \hat{\mu}_1 = \frac{1}{2}(Y_1 + Y_2)$ is to be preferred for $\gamma > .82$, for $.52 < \gamma \leq .82$, $\hat{\mu}_4$, the minimax estimator, and for $.03 < \gamma \leq .52$, $\hat{\mu}_2$, the Winsorized estimator $\frac{1}{3}(Y_1 + 2Y_2)$, are preferable. The median $\hat{\mu}_3$ is preferable to the other three only for $\gamma < .03$.

Figure 1



In practical situations it is likely that γ would be of small or moderate size and that Δ/σ would be positive and moderate or large. (If in fact $|\Delta/\sigma|$ were small one would not be apt to suspect the presence of outliers.) Thus, any of $\hat{\mu}_0$, $\hat{\mu}_2$, or $\hat{\mu}_4$ might be the preferable estimator. The median would be preferred to the other four estimators only if both $\gamma < .03$ and $|\Delta/\sigma| \geq 6$. It seems clear from this analysis that for each γ there is an estimator $\hat{\mu}(a_1(\gamma)) = a_1(\gamma)Y_1 + (1-a_1(\gamma))Y_2$ which minimizes the value of $|\Delta/\sigma|$ required such that a two-order-statistic estimator is preferred to $\hat{\mu}_0$.

The expression for $a_1(\gamma)$ has been found to be given by

$$a_1(\gamma) = \frac{.17301(1-\gamma) + \gamma}{1.17301(1-\gamma) + 2\gamma}.$$

Hence,

$$a_1(1) = \frac{1}{2}, \quad \hat{\mu}(a_1(1)) = \frac{1}{2}(Y_1 + Y_2),$$

and

$$a_1(.5) = .3697, \quad \hat{\mu}(a_1(.5)) = .3697Y_1 + .6303Y_2,$$

$$a_1(0) = .1474, \quad \hat{\mu}(a_1(0)) = .1474Y_1 + .8526Y_2,$$

where $\hat{\mu}(a_1(1))$ is $\hat{\mu}_\Delta$, the best linear invariant (BLI) estimator when θ_Δ is true, and $\hat{\mu}(a_1(0))$ is $\hat{\mu}_0$, the BLI estimator when θ_0 is true. For $\hat{\mu}(a_1(\gamma))$ equal to the minimax estimator, $a_1(\gamma) = .42265$, so that γ is equal to .676.

It has also been demonstrated that $a_1(\gamma)$ increases monotonically with γ from .1474 for $\gamma = 0$ to .5 for $\gamma = 1$. Thus, the median would never be the two-order statistic estimator recommended in preference to $\hat{\mu}_0$.

A METHOD OF DEALING WITH THE UNKNOWN PARAMETER Δ/σ

A Monte Carlo analysis of a more general outlier problem is discussed in the final portion of Ferguson [2]. The results indicate that for a sample size as small as 3, there are no discernible differences between the values of the power functions of the locally most powerful test of $\Delta/\sigma = 0$ versus $\Delta/\sigma > 0$, based on the coefficient of skewness and two other tests, one of which is based on $R_{10} = (X_n - X_{n-1}) / (X_n - X_1)$ with $X_1 \leq X_2 \leq \dots \leq X_{n-1} \leq X_n$, proposed by Dixon in [1].

Suppose we consider $\left(\frac{1}{R_{10}} - 1\right)^{-1} = \left\{ \left[(Y_3 - Y_2)/(Y_3 - Y_1) \right]^{-1} - 1 \right\}^{-1}$
 $= (Y_3 - Y_2)/(Y_2 - Y_1)$. Note that if $Z_{1,n}$ is the i^{th} order statistic
from a size n sample from the standard normal distribution,
 $\left[(Y_3 - Y_2)/(Y_2 - Y_1) \right] (Z_{2,2} - Z_{1,2}) + Z_{2,2} = \Delta/\sigma + Z_{1,1}$ with probability
 γ , and $\left[(Y_3 - Y_2)/(Y_2 - Y_1) \right] (Z_{2,3} - Z_{1,3}) + Z_{2,3} = Z_{3,3}$, with proba-
bility $1 - \gamma$, where $(Y_1 - \mu)/\sigma = Z_{1,2}$ ($i = 1, 2$), and $(Y_3 - \mu)/\sigma = \Delta/\sigma + Z_{1,1}$
with probability γ and $(Y_1 - \mu)/\sigma = Z_{1,3}$ and $(Y_3 - \mu)/\sigma = Z_{3,3}$ with
probability $1 - \gamma$. Let $\left[(Y_3 - Y_2)/(Y_2 - Y_1) \right] (Z_{2,2} - Z_{1,2}) + Z_{2,2} - Z_{1,1}$
be identically equal to $t(Z_{2,2} - Z_{1,2}) + Z_{2,2} - Z_{1,1} = W(t)$, and let $\overline{\Delta/\sigma} > 0$
be specified. Then $\Pr[\Delta/\sigma > \overline{\Delta/\sigma}] = \Pr[\theta_\Delta \text{ is true}] \times \Pr[\Delta/\sigma > \overline{\Delta/\sigma} \mid \theta_\Delta \text{ is true}]$
or

$$\Pr[\Delta/\sigma > \overline{\Delta/\sigma}] = \gamma \int_{\overline{\Delta/\sigma}}^{\infty} dF[W(t)] .$$

The expression on the right-hand side of this equation can be calculated by
considering the joint density of $Z_{1,2}$, $Z_{2,2}$ and $Z_{1,1}$. From this, one obtains

$$\gamma \int_{\overline{\Delta/\sigma}}^{\infty} dF[W(t)] = \gamma \left\{ 1 - \frac{1}{\sqrt{3(2t+1)}} \left\{ 3 \left[\Pr\left(Z < \frac{(2t+1)\overline{\Delta/\sigma}}{\sqrt{6(1+t+t^2)}}\right) \right]^2 \left[\Pr\left(Z > \frac{(2t+1)\overline{\Delta/\sigma}}{\sqrt{6(1+t+t^2)}}\right) \right] \right. \right. \\ \left. \left. + \left[\Pr\left(Z < \frac{(2t+1)\overline{\Delta/\sigma}}{\sqrt{6(1+t+t^2)}}\right) \right]^3 \right\} \right\} ,$$

where Z is the standard normal deviate and t is greater than zero.

The expression $\frac{2t+1}{\sqrt{6(1+t+t^2)}}$ is equal to $\frac{2Y_3 - Y_2 - Y_1}{\sqrt{6[(Y_3 - Y_2)^2 + (Y_3 - Y_2)(Y_2 - Y_1) + (Y_2 - Y_1)^2]}}$
 and $2t + 1$ equals $\frac{2Y_3 - Y_2 - Y_1}{Y_2 - Y_1}$.

An appropriate value for Δ/σ in terms of γ alone can be obtained by substituting $a_1(\gamma)$ into the original expression from which the value for $a_1(\gamma)$ is derived. This gives

$$\Delta/\sigma = \left[\frac{2}{\gamma} \frac{(.18853\gamma^3 + .99076\gamma^2 - .20923\gamma + 1.029932)}{(.68391\gamma^2 + 1.9401\gamma + 1.3759)} - \frac{2}{\gamma} \right]^{\frac{1}{2}}.$$

Therefore, for any prior probability γ , that θ_A is true, the probability that Δ/σ is sufficiently large so that the risk of a two-order-statistic estimator is smaller than the risk of $\hat{\mu}_0$ can be calculated as a function of γ and the observations only. One could then choose some fixed value P , $0 < P < 1$ (a good choice might be $P = .5$), and for any known γ , estimate μ by $\hat{\mu}_0 = \frac{1}{3}(Y_1 + Y_2 + Y_3)$ if $\Pr[\Delta/\sigma > \Delta/\sigma]$ is less than P and by $\hat{\mu}(a_1(\gamma))$ otherwise.

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APPENDIX A

DESIGN OF OVER STRESS LIFE-TEST EXPERIMENTS WHEN FAILURE TIMES HAVE THE TWO-PARAMETER WEIBULL DISTRIBUTION

SUMMARY

The following paper deals with the situation in which estimation of reliability parameters associated with a failure-time distribution requires that life testing be conducted at stress levels above that which would normally be applied in standard usage (the nominal stress level). This situation may prevail when an inordinate amount of time is required to obtain a failure at the nominal stress level.

A range of stress for testing is prescribed, and a two-parameter Weibull model for failure times (a type I extreme-value distribution of smallest values for log failure time) is assumed. The extreme-value location parameter u , the logarithm of the Weibull scale parameters, is assumed to be a polynomial function of known degree k of the reciprocal of stress level. The Weibull shape parameter b , which is also the extreme-value scale parameter, is assumed to be independent of stress level.

The number n of items in the total sample to be life tested is given, and it is assumed that stress level for each life test is sufficiently high so that each item can be tested until failure. The problem considered is that of determining the design for obtaining the least-squares-curve intercept with minimum variance at the nominal stress level. The design to be determined consists of the number and location of stress levels in the prescribed range at which the life tests will be conducted and proportion of total sample to be randomly allocated to each testing level.

The results of Hoel and Levine in [2] concerning determination of designs for minimum-variance polynomial extrapolation cannot be applied directly because the models for which these results are appropriate are those in which the observations are normally distributed, uncorrelated, and have uniform variance. In our model the logarithms of observed failure times have the Type I extreme-value distribution of smallest values, unequal variances, and covariances that are not zero except between stress levels. It is shown that the methods of proof utilized by Hoel and Levine are applicable, however, and rules for determining designs yielding the "approximately" minimum-variance least-squares intercept for the prescribed model are derived.

One of the interesting results in the derivation of the design is the delineation of the point through which the least-squares curve for the observations passes at the α^{th} stress level, $\alpha = 0, 1, \dots, k-1$, when the number k of stress levels at which observations are made is $k+1$. This point is $\frac{1}{\sigma_\alpha}, X^*\left(\frac{1}{\sigma_\alpha}\right)$, where $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is a weighted average of the ordered observations and where the i^{th} weight consists of the elements in the i^{th} row, $i = 1, 2, \dots, m_\alpha$, of the covariance matrix of the m_α ordered observations made at the α^{th} level, $\alpha = 0, 1, \dots, k$. For $m_\alpha \geq 2$, $X^*\left(\frac{1}{\sigma_\alpha}\right)$ can also be expressed as a specific function of the Gauss-Markov least-squares best linear unbiased estimators $u^*\left(\frac{1}{\sigma_\alpha}\right)$ and b_α^* at $\sigma = \sigma_\alpha$ of u_α (the value of u at the α^{th} testing level) and

b , respectively, the variance of b_{α}^* and the covariance of $u^*\left(\frac{1}{\sigma_{\alpha}}\right)$ and b_{α}^* , $\alpha = 0, 1, \dots, k$. This particular result is independent of the distribution of the observations and applies whether or not n_{α} is equal to n_{α} , where $n_{\alpha} = p_{\alpha}n$ and p_{α} is the proportion of the sample randomly assigned to the α^{th} sample point, $\alpha = 0, 1, \dots, k$, (that is, there may be censoring). It is shown that there is no linear combination $\bar{X}\left(\frac{1}{\sigma_{\alpha}}\right)$ of ordered observations at the α^{th} testing level and no point along that ordinate such that the mean squared deviation of $\bar{X}\left(\frac{1}{\sigma_{\alpha}}\right)$ from the point is less than or equal to the variance of $X^*\left(\frac{1}{\sigma_{\alpha}}\right)$ for all u_{α} and b , $\alpha = 0, 1, \dots, k$. Similar properties are demonstrated for the least-squares intercept at the nominal stress level under the design prescribed by the derived results.

INTRODUCTION

Often an engineer may want an estimate of a parameter associated with the reliability of a population of items which are to be subjected to a fixed (or nominal) level of stress and fairly constant environmental conditions during normal usage. If a required life t_0 is specified, then he will want to estimate the reliability at time t_0 after the stress is applied. If, on the other hand, a survival proportion R is specified, then he will be interested in estimating the reliable life, or the time after the application of the stress at which $100(1-R)\%$ of the population of items will have failed.

He may know from theoretical considerations the family of distributions to which the failure times associated with the population of items belong. If so, he can conduct a life test by applying the nominal level of stress under appropriate environmental conditions to a sample chosen from the population of items and thus he can obtain an efficient estimate of the parameter of interest as a function of estimates of the distribution parameters (parameters of the failure-time distribution). These estimates will be based on the failure times observed during the life test.

Suppose, however, that the failure characteristics of the population are such that an excessively long period of time is required before even a single failure will occur at the nominal stress level. In such a case, the life test can be conducted at levels above nominal stress to obtain the failures required for estimation of the parameters, provided the form of the relationship between the parameters and the stress level is known. In the following discussion, the form of both this relationship and the failure-time distribution are assumed to be known from theory associated with the composition of the items.

It is assumed that in a life-testing situation the population failure times are identically distributed according to a given two-parameter Weibull law,

$$F(t) = \begin{cases} 1 - e^{-\left(\frac{t}{\xi}\right)^{\frac{1}{b}}}, & t \geq 0 \\ 0 & , \text{ otherwise } ; \xi, b > 0, \end{cases} \quad (1)$$

when the material and shape of the items tested, the environmental conditions of the test and the levels of stresses are fixed. We also assume that the size n sample which is tested has been randomly selected from a population of items composed of homogeneous material and that all environmental conditions are held fixed save level of stress σ for one type of stress of interest. Further, it is assumed, in agreement with [1], [8], and [9], that under these conditions the Weibull shape parameter b is constant and that only the scale parameter ξ changes as level of stress changes.

If the random variable T represents failure time, then X , the natural logarithm of T , has the Type I extreme-value distribution of smallest values with location parameter u (the natural logarithm of ξ) and scale parameter b , with $\pi^2 b^2/6$ the variance of X . We suppose that a given log failure time is a polynomial function of degree k of $1/\sigma$ (a special case of this assumption, $\log t = \beta_0 + \beta_1/\sigma$, is given in [1]). Finally, it

is assumed that the n_{α} failure times observable at the α^{th} of k experimental (or testing) stress levels are independent of those at any other of the $k - 1$ testing levels. This implies that the sample items are selected randomly for assignment to a stress level.

Under these assumptions it is desired to design the life test so that the least-squares curve (with expectation $x_{1/\sigma, b}$) has minimum variance at $\sigma = \frac{1}{\eta}$ when testing of the n sample items is conducted in the stress domain $c \leq \sigma \leq d$ and $\frac{1}{\eta} < c$. We define this to be optimum estimation for this situation, which is one of testing at levels above nominal stress. Because this is an over-stress situation, it is assumed here that the stress levels at which testing will be conducted are sufficiently high so that all items can be allowed to fail, with no consideration necessary for waiting time for failure. This over-stress problem is equivalent to one of obtaining an optimum design for linear estimation of the polynomial function $x_{1/\sigma, b}$ at a point outside the experimental range of the independent variable.

Specifically, it is necessary to determine (a) the value for k , the number of sample points, (b) where in the domain the k sample points should be assigned, and (c) the values of n_{α} , $\alpha = 0, 1, \dots, k - 1$, such that estimation is optimum for a given sample size n . The analysis involves approximation in terms of n_{α} , $\alpha = 0, 1, \dots, k - 1$, of the

variance of the least-squares curve at $\sigma = \frac{1}{\eta}$. Hence the optimal solution given is approximate.

It will be clear from the model given below that the results of Hoel and Levine in [2], which are applicable to the case in which the observations are independent, have equal variances, and are selected from a Gaussian distribution, cannot be used directly to provide the design for optimum estimation here.

THE MODEL

The derivations immediately following apply to the general case in which only the first m_α failure times, $m_\alpha \leq n_\alpha$, may be observed, so the assumptions $m_\alpha = n_\alpha$ will not be employed until later. Let $X_{1,\alpha}, X_{1,\alpha} \leq X_{2,\alpha} \leq \dots \leq X_{m_\alpha,\alpha} \leq \dots \leq X_{n_\alpha,\alpha}$, be the logarithm of the i th observed ordered failure time at the α th stress level and let

$$Y_{i,\alpha} = \frac{X_{i,\alpha} - u_\alpha}{b}, \quad i = 1, 2, \dots, m_\alpha,$$

where u_α represents the value of $u\left(\frac{1}{\sigma}\right) = \beta_0 + \beta_1\left(\frac{1}{\sigma}\right) + \dots + \beta_k\left(\frac{1}{\sigma}\right)^k$ at the α th stress level, $\alpha = 0, 1, \dots, l-1$. Then $Y_{i,\alpha}$ is the i th order statistic, $i = 1, 2, \dots, m_\alpha$, of a sample of size n_α , $\alpha = 0, 1, \dots, l-1$, from the distribution of $Y = \frac{X-u}{b}$, the

reduced first asymptotic distribution of smallest values.

Therefore,

$$E[X_{1,\alpha}] = u_\alpha + b E(Y_{1,\alpha}) \quad (2)$$

$$i = 1, 2, \dots, m_\alpha,$$

$$\alpha = 0, 1, \dots, l-1,$$

and Σ_X , the covariance matrix of the X 's, is given by

$$\Sigma_X = b^2 V. \quad (3)$$

Since it is assumed that the failure times at any given testing level are independent of those at any other level,

$$V = b^2 \begin{pmatrix} V_0 & & \\ & V_1 & \\ & & \ddots \\ & & & V_{l-1} \end{pmatrix}, \quad (4)$$

where V_α , $\alpha = 0, 1, \dots, l-1$, is the known covariance matrix of the first m_α of n_α order statistics of the distribution of Y . From (2), (3), and (4), it can be seen that the generalized Gauss-Markov Theorem, given in [4], applies. Hence, least-squares estimators having uniformly minimum variance among unbiased linear estimators can be obtained for u_α and b when l , m_α , $\alpha = 0, 1, \dots, l-1$, and testing levels for stress are fixed. The problem of determining these quantities for optimum estimation is now considered.

DESIGN FOR OPTIMUM ESTIMATION

The information matrix of the Gauss-Markov least-squares curve for any selection of n observations in the interval $c \leq \sigma \leq d$ can be duplicated by choosing at most $k + 1$ distinct stress levels in this interval and allocating the n observations appropriately to these new levels. We therefore let the number of stress levels (testing levels for the stress) be $k + 1$, and the α^{th} testing level be σ_α , $\alpha = 0, 1, \dots, k$, with $\sigma_0 < \sigma_1 < \dots < \sigma_k$.

If b is not known, it is necessary that m_α be at least 2 for at least one stress level in order that u_α be estimable (an unbiased estimator exist), $\alpha = 0, 1, \dots, k$. This is true because $E(X_{1,\alpha})$ is not equal to u_α , but rather $E(X_{1,\alpha}) = u_\alpha + b E(Y_{1,\alpha})$, with $E(Y_{1,\alpha}) \neq 0$, $\alpha = 0, 1, \dots, k$. Note that if $Z_{i,n}$ is the i^{th} order statistic, $i = 1, 2, \dots, n$, of a size n sample from a reduced Gaussian distribution, $E(Z_{1,1}) = 0$. If b is known, m_α can be 1, $\alpha = 0, 1, \dots, k$. Optimum estimation for b known will be considered in the section following this one.

Let $v^{i,j,\alpha}$ be the element in the $\alpha + i^{\text{th}}$ row and the $\alpha + j^{\text{th}}$ column, $i, j = 1, 2, \dots, m_\alpha$, $\alpha = 0, 1, \dots, k$, of V^{-1} , the inverse matrix of V . It can easily be shown that when m_α observations are made at each of $k + 1$ points, the least-squares estimator $x^*(\frac{1}{\sigma})$ of the expected value of the least-squares curve at $(\frac{1}{\sigma})$,

$x_{1/\sigma, b} = \beta_0 + \beta_1 \left(\frac{1}{\sigma}\right) + \dots + \beta_k \left(\frac{1}{\sigma}\right)^k + \kappa_0(b)$ (with $\kappa_0(b)$ defined below), passes through

$$\frac{1}{\sigma_\alpha}, \frac{\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{1,j,\alpha} x_{1,\alpha}}{\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{1,j,\alpha}} \quad (5)$$

and can be expressed in the form

$$x^*\left(\frac{1}{\sigma}\right) = \sum_{\alpha=0}^k L_\alpha\left(\frac{1}{\sigma}\right) \frac{\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{1,j,\alpha} x_{1,\alpha}}{\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{1,j,\alpha}} = \sum_{\alpha=0}^k L_\alpha\left(\frac{1}{\sigma}\right) x^*\left(\frac{1}{\sigma_\alpha}\right), \quad (6)$$

where $L_\alpha\left(\frac{1}{\sigma}\right)$ is the Lagrange polynomial

$$\frac{\left(\frac{1}{\sigma} - \frac{1}{\sigma_0}\right) \dots \left(\frac{1}{\sigma} - \frac{1}{\sigma_{\alpha-1}}\right) \left(\frac{1}{\sigma} - \frac{1}{\sigma_{\alpha+1}}\right) \dots \left(\frac{1}{\sigma} - \frac{1}{\sigma_k}\right)}{\left(\frac{1}{\sigma_\alpha} - \frac{1}{\sigma_0}\right) \dots \left(\frac{1}{\sigma_\alpha} - \frac{1}{\sigma_{\alpha-1}}\right) \left(\frac{1}{\sigma_\alpha} - \frac{1}{\sigma_{\alpha+1}}\right) \dots \left(\frac{1}{\sigma_\alpha} - \frac{1}{\sigma_k}\right)}, \quad (7)$$

$\alpha = 0, 1, \dots, k.$

This represents a generalization of the better known result used by Hoel and Levine in [2], where $m_\alpha = n_\alpha$ and the model is

$$E[W_{1,\alpha}] = u_\alpha = \beta_0 + \beta_1(z_\alpha) + \dots + \beta_k(z_\alpha)^k, \quad (8)$$

$$i = 1, 2, \dots, n_\alpha,$$

$$\alpha = 0, 1, \dots, k-1,$$

with

$$\Sigma_W = b^2 I, \quad (9)$$

and I the identity matrix. Here, $W_{i,\alpha}$ is the i^{th} Gaussian order statistic, $i = 1, 2, \dots, n_\alpha$, $\alpha = 0, 1, \dots, l-1$, and for $l = k+1$,

the least-squares estimator W^* of $w = \sum_{j=0}^k \beta_j z^j$ passes through

z_α, \bar{w}_α . W^* can be expressed in the form

$$\sum_{\alpha=0}^k L_\alpha(z) \bar{w}_\alpha,$$

with \bar{w}_α equal to $\frac{1}{n_\alpha} \sum_{i=1}^{n_\alpha} W_{i,\alpha}$, $\alpha = 0, 1, \dots, k$, and $L_\alpha(z)$

defined by (7). It might be noted that $\sum_{\alpha=0}^k L_\alpha(z) = 1$.

The variance $\text{Var} \left(X^* \left(\frac{1}{\sigma} \right) \right)$ of the least-squares estimator $X^* \left(\frac{1}{\sigma} \right)$ of $x_{1/\alpha,b}$ is simply the sum of the variances at the $k+1$ testing levels,

or

$$\text{Var} \left(X^* \left(\frac{1}{\sigma} \right) \right) = b^2 \sum_{\alpha=0}^k L_\alpha^2 \left(\frac{1}{\sigma} \right) \frac{\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v_{i,j,\alpha} \sum_{r=1}^{m_\alpha} v_{i,r,\alpha} \sum_{s=1}^{m_\alpha} v_{s,j,\alpha}}{\left(\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v_{i,j,\alpha} \right)^2}$$

which reduces to

$$\text{Var} \left(X^* \left(\frac{1}{\sigma} \right) \right) = b^2 \sum_{\alpha=0}^k L_\alpha^2 \left(\frac{1}{\sigma} \right) / \sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v_{i,j,\alpha}. \quad (10)$$

Here, $v_{i,j,\alpha}$ is the element in the $\alpha + i^{\text{th}}$ row and the $\alpha + j^{\text{th}}$ column, $i, j = 1, 2, \dots, m_\alpha$, $\alpha = 0, 1, \dots, k$, of v .

Let $u^*\left(\frac{1}{\sigma_\alpha}\right)$ be

$$-\frac{\sum_{s=1}^{m_\alpha} \sum_{r=1}^{m_\alpha} \left[\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} E(Y_{i,\alpha}) v^{i,j,\alpha} E(Y_{r,\alpha}) v^{i,s,\alpha} - \sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} E(Y_{i,\alpha}) E(Y_{j,\alpha}) v^{i,j,\alpha} v^{r,s,\alpha} \right] x_{s,\alpha}}{\Delta}$$

and b_α^* be

$$\frac{\sum_{s=1}^{m_\alpha} \sum_{r=1}^{m_\alpha} \left[\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{i,j,\alpha} E(Y_{r,\alpha}) v^{r,s,\alpha} - \sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} E(Y_{i,\alpha}) v^{i,j,\alpha} v^{r,s,\alpha} \right] x_{s,\alpha}}{\Delta},$$

where

$$\Delta = \sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} v^{i,j,\alpha} \sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} E(Y_{i,\alpha}) E(Y_{j,\alpha}) v^{i,j,\alpha} - \left(\sum_{j=1}^{m_\alpha} \sum_{i=1}^{m_\alpha} E(Y_{i,\alpha}) v^{i,j,\alpha} \right)^2.$$

The expressions $u^*\left(\frac{1}{\sigma_\alpha}\right)$ and b_α^* are the least-squares uniformly minimum - variance unbiased linear estimators of $u\left(\frac{1}{\sigma}\right)$ and b at the α^{th} sample point. Let the variance of the b_α^* be $\text{Var}(b_\alpha^*)$, the variance of $u^*\left(\frac{1}{\sigma_\alpha}\right)$ be $\text{Var}\left(u^*\left(\frac{1}{\sigma_\alpha}\right)\right)$, and the covariance of $u^*\left(\frac{1}{\sigma_\alpha}\right)$ and b_α^* be $\text{Cov}\left(u^*\left(\frac{1}{\sigma_\alpha}\right), b_\alpha^*\right)$. Then $\text{Var}\left(u^*\left(\frac{1}{\sigma_\alpha}\right)\right)$, as given by (10), can be shown to be equal to

$$\left[\text{Var}\left(u^*\left(\frac{1}{\sigma_\alpha}\right)\right) - \text{Cov}^2\left(u^*\left(\frac{1}{\sigma_\alpha}\right), b_\alpha^*\right) / \text{Var}(b_\alpha^*) \right], \quad (11)$$

and it can also be shown that

$$u^*\left(\frac{1}{\sigma_\alpha}\right) = \left[u^*\left(\frac{1}{\sigma_\alpha}\right) - \text{Cov}\left(u^*\left(\frac{1}{\sigma_\alpha}\right), b_\alpha^*\right) b_\alpha^* / \text{Var}(b_\alpha^*) \right], \quad (12)$$

for $m_\alpha \geq 2$, $\alpha = 0, 1, \dots, k$. For $m_\alpha = 1$, $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is simply $X_{1,\alpha}$, $\alpha = 0, 1, \dots, k$, with variance $\pi^2 \frac{b^2}{6}$. It can be seen from (12) that

$$x_0(b) \text{ in } x_{1/\sigma} b = u\left(\frac{1}{\sigma}\right) + x_0(b) \text{ is equal to } \frac{1}{\sum_{\alpha=0}^k L_\alpha\left(\frac{1}{\sigma}\right)} \frac{\text{Cov}\left(u^*\left(\frac{1}{\sigma_\alpha}\right), b_\alpha^*\right)}{\text{Var}(b_\alpha^*)} b.$$

The expression (11) also defines, for $m_\alpha \geq 2$, the variance of

$$\bar{w}_\alpha = \sum_{i=0}^{n_\alpha} W_{i,\alpha}, \text{ described by (8) and (9) with } z_\alpha = \frac{1}{\sigma_\alpha} \text{ and } m_\alpha = n_\alpha,$$

where $u^*\left(\frac{1}{\sigma_\alpha}\right)$ and b_α^* are the least-squares best linear unbiased estimators of u and b , respectively, at the α^{th} sample point, $\alpha = 0, 1, \dots, k$.

When the density function of \bar{w}_α is symmetric about the location parameter

u , however, as when $W_{i,\alpha}$, $i = 0, 1, \dots, n_\alpha$, $\alpha = 0, 1, \dots, k$ is a

Gaussian order statistic, then the covariance between the least-squares

estimators $u^*\left(\frac{1}{\sigma_\alpha}\right)$ and b_α^* of the location parameter u_α , $\alpha = 0, 1, \dots, k$,

and the scale parameter b , respectively, is zero, as is shown in [4].

In this case the variance of \bar{w}_α is simply equal to the variance of

$u^*\left(\frac{1}{\sigma_\alpha}\right)$, as in [2], where $u^*\left(\frac{1}{\sigma_\alpha}\right) = \bar{w}_\alpha$, $\alpha = 0, 1, \dots, k$.

For $m_\alpha = 1$, $\text{Var}\left(X^*\left(\frac{1}{\sigma_\alpha}\right)\right) = \text{Var}(X_{1,\alpha}) = \pi^2 b^2 / 6 \approx 1.64493 b^2$. Also it is

possible for any given combination of values of m_α and n_α , $2 \leq m_\alpha \leq n_\alpha$,

to calculate a value for the variance of $X^*\left(\frac{1}{\sigma_\alpha}\right)$ using (11) and the tables

$$1 \text{ Where any } m_\alpha \text{ is equal to 1, } \frac{\text{Cov}\left(u^*\left(\frac{1}{\sigma_\alpha}\right), b_\alpha^*\right)}{\text{Var}(b_\alpha^*)} \text{ is taken to be } E(Y_{1,\alpha}),$$

$\alpha = 0, 1, \dots, k$.

in [3] for $n_\alpha \leq 6$, [10] for $n_\alpha \leq 20$, or [6] for $n_\alpha \leq 25$. For $m_\alpha = n_\alpha$, one obtains (to within a unit in the fifth decimal place),

n_α	$\text{Var } X^*\left(\frac{1}{\sigma_\alpha}\right)$
1	1.64493 b^2
2	.65373 b^2
3	.40108 b^2
4	.28810 b^2
.	.
.	.
.	.
$n_\alpha \rightarrow \infty$	$b^2/n_\alpha, \alpha = 0, 1, \dots, k.$

A general expression for $\text{Var } X^*\left(\frac{1}{\sigma_\alpha}\right)$ in terms of n_α , for $m_\alpha = n_\alpha$, can then be given approximately (to almost within a unit in the second significant figure) by $b^2/(n_\alpha - 0.43)$, $\alpha = 0, 1, \dots, k$.

Let $m_\alpha = n_\alpha$ and $p_\alpha = n_\alpha/n$, $\alpha = 0, 1, \dots, k$, so that $\sum_{\alpha=0}^k p_\alpha = 1$.

The variance of the least-squares estimator $X^*(\eta)$ at the stress level $1/\eta$ is of the approximate form

$$(b^2/n) \sum_{\alpha=0}^k L_\alpha^2(\eta)/(p_\alpha - 0.43/n). \quad (13)$$

For any choice of testing levels $\sigma_0, \sigma_1, \dots, \sigma_k$, the approximate variance given by (13) will be minimized, under the constraint

$$\sum_{\alpha=0}^k p_{\alpha} = 1, \text{ with } 0 \leq p_{\alpha} \leq 1 \text{ and with } \frac{1}{\eta} \neq \sigma_{\alpha}, \text{ if}$$

$$p_{\alpha} = \frac{(1 - 0.43(k+1)/n) |L_{\alpha}(\eta)|}{\sum_{j=0}^k |L_j(\eta)|} + \frac{0.43}{n}, \quad \alpha = 0, 1, \dots, k. \quad (14)$$

This result is obtained, as is Lemma 1 of [2], simply by standard calculus techniques. If the proportion p_{α} of the sample assigned to the stress level σ_{α} is given by (14), the variance of the least-squares estimator is approximately

$$(b^2/n) \left(\sum_{\alpha=0}^k |L_{\alpha}(\eta)|^2 / (1 - 0.43(k+1)/n) \right) \quad (15)$$

for η as defined.

Clearly, the expression (15) will be minimized if $\sum_{\alpha=0}^k |L_{\alpha}(\eta)|$ is

minimized. Therefore, the theorem below follows immediately from the proof by Hoel and Levine (consisting of a minimization of

$\sum_{\alpha=0}^k |L_{\alpha}(\eta)|$, $\eta > 1/c$) of a similar theorem in [2] for the model given

by (8) and (9) plus the normality assumption.

THEOREM I. Under the assumptions (2), (3), and (4), let p_α , given by formula (14), be the proportion of the sample of n items tested at the stress level σ_α , $\sigma_0 \leq \sigma_1 \leq \dots \leq \sigma_k$, in the range $c \leq \sigma_\alpha \leq d$, $\alpha = 0, 1, \dots, k$, and let $1/\eta$ be less than c . The value of $\frac{1}{\sigma_\alpha}$ that will minimize the expression (15) giving the approximate variance of $X^*(\eta)$, the point on the least-squares curve at $\sigma = 1/\eta$, is

$$\frac{1}{\sigma_\alpha} = \left\{ -\cos\left[(k - \alpha)\pi/k\right] \right\} \left(\frac{1}{c} - \frac{1}{d} \right)/2 + \left(\frac{1}{c} + \frac{1}{d} \right)/2, \quad \alpha = 0, 1, \dots, k. \quad (16)$$

Theorem I then gives the solution to the problem of obtaining the least-squares curve with minimum-variance intercept at $\sigma = 1/\eta$ under the assumptions (2), (3), and (4). In the following section, properties of this minimum-variance intercept and the least-squares curve in general will be considered.

PROPERTIES OF THE LEAST-SQUARES CURVE UNDER THE GENERAL MODEL

An interesting property of the least-squares curve which holds at the $k + 1$ testing levels is first demonstrated. Consider any distribution with unknown location-scale parameter $\theta = (\theta_1, \theta_2)$ such that $f_\theta(x) = \frac{1}{\theta_2} g\left(\frac{x - \theta_1}{\theta_2}\right)$ for some g . Let θ_1^* and θ_2^* be the unique (with probability 1) uniformly minimum-variance unbiased estimators of θ_1 and θ_2 , respectively, in some class of estimators (linear estimators, for example, or all possible

estimators). Let $A\theta_2^2$ and $C\theta_2^2$ be the variances of θ_1^* and θ_2^* , respectively, and $B\theta_2^2$ their covariance, and let loss be squared error divided by θ_2^2 . It is shown in [7] that (1) for any given function of the form $\hat{\theta} = k_1 \theta_1 + k_2 \theta_2$ the unique estimator with smallest expected loss among estimators in the class invariant under transformations of location and scale (when the best unbiased estimator of $\hat{\theta}$ in the class

is $k_1 \theta_1^* + k_2 \theta_2^*$) is

$$\tilde{\theta} = k_1 \theta_1^* + (k_2 - k_1 B) \theta_2^* / (1+C) \quad (17)$$

and (2) if $\tilde{\theta}$ is linear in the observed x 's, then it is the unique admissible¹ minimax linear estimator of $\hat{\theta}$. The proof of (1) is very similar to the derivation in [6] of the expression for Cramér-Rao type bounds for invariant estimators of location parameters of the form $\theta_1 + k\theta_2$.

Let $\text{Var}\left(u^*\left(\frac{1}{\sigma_\alpha}\right)\right)$ be $A_\alpha b^2$, $\text{Var}(b_\alpha^*)$ be $C_\alpha b^2$, and $\text{Cov}\left(u^*\left(\frac{1}{\sigma_\alpha}\right), b_\alpha^*\right)$ be $B_\alpha b^2$. Then, by (17), the unique admissible¹ minimax linear estimators of u_α and b at the α^{th} stress level are $\tilde{u}\left(\frac{1}{\sigma_\alpha}\right) = u^*\left(\frac{1}{\sigma_\alpha}\right) - B_\alpha b_\alpha^* / (1+C_\alpha)$ and $\tilde{b}_\alpha = b_\alpha^* / (1+C_\alpha)$, respectively, $\alpha = 0, 1, \dots, k$. Furthermore, it can be very readily seen that $X^*\left(\frac{1}{\sigma_\alpha}\right) = u^*\left(\frac{1}{\sigma_\alpha}\right) - B_\alpha b_\alpha^* / C_\alpha$ can also be expressed as $X^*\left(\frac{1}{\sigma_\alpha}\right) = \tilde{u}\left(\frac{1}{\sigma_\alpha}\right) - B_\alpha \tilde{b}_\alpha / C_\alpha$, and that $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is the best

¹The proof of linear admissibility for $\tilde{\theta}$, which had been shown in [5] to be the best linear invariant estimator of $\hat{\theta}$, was outlined in detail to this author by M. R. Mickey of the University of California at Los Angeles by personal communication.

linear invariant estimator of $x_{1/\sigma_\alpha, b}$, its expected value,
 $\alpha = 0, 1, \dots, k$. This result is related to the fact that $X^*\left(\frac{1}{\sigma_\alpha}\right)$ and
 b_α^* have zero covariance, $\alpha = 0, 1, \dots, k$.

Another property of the least-squares curve which will be demonstrated
below is the following. Under the assumptions (2), (3), and (4), there
exists no linear combination of the ordered observations at stress
level σ_α and no point $u_\alpha + \zeta b$, $-\infty < \zeta < \infty$, along the $\frac{1}{\sigma_\alpha}$ ordinate
such that the expected squared deviation of this linear combination
from $u_\alpha + \zeta b$ is smaller than that of $X^*\left(\frac{1}{\sigma_\alpha}\right)$, the intercept of the
least-squares curve at $\sigma = \sigma_\alpha$, from its expected value,

$x_{1/\sigma_\alpha, b} = \beta_0 + \beta\left(\frac{1}{\sigma_\alpha}\right) + \dots + \beta_k\left(\frac{1}{\sigma_\alpha}\right)^k + \kappa_0(b)$, for at least one com-
bination of values of u_α and b and at least as small for all combina-
tions of values of u_α and b , $\alpha = 0, 1, \dots, k$. We say then that the
"admissibility" of the linear combination $X^*\left(\frac{1}{\sigma_\alpha}\right)$ will be demonstrated.

It will also be shown that when loss is squared error divided by
 b^2 , $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is a minimax linear combination of the observations (has
smaller maximum expected loss from $x_{1/\sigma_\alpha, b}$ as a function of u_α
and b than any other linear combination from any point $u_\alpha + \zeta b$, $-\infty < \zeta < \infty$,
along the $\frac{1}{\sigma_\alpha}$ ordinate), $\alpha = 0, 1, \dots, k$. Properties of the least-
squares curve at $\sigma = \frac{1}{\eta}$ will also be demonstrated.

Let $X_T^*(\eta)$ be the intercept on the least-squares curve at $\sigma = \frac{1}{\eta}$ when n observations are made at $\sigma_1 \leq \sigma_2 \leq \dots \leq \sigma_k$, with $c \leq \sigma_\alpha \leq d$ and $\frac{1}{\eta} < c$, and when σ_α and p_α , the proportion of the n failure times observed at the α^{th} level, are those specified by Theorem I. Assume (13) gives the exact variance of $X^*(\eta)$, defined by (10). The following theorem will now be proved.

THEOREM II. Let loss be squared error divided by b^2 . Under the assumptions (2), (3) and (4), $X^*\left(\frac{1}{\sigma_\alpha}\right)$, the intercept of the least-squares curve at $\frac{1}{\sigma_\alpha}$, is the unique admissible minimax linear combination of the ordered observations made at $\sigma = \sigma_\alpha$. $X_T^*(\eta)$, defined above, is the unique admissible minimax linear combination of n observations extrapolated to $\sigma = \frac{1}{\eta}$, when it is assumed that (15) gives its exact variance. $X_T^*(\eta)$ is also the linear function with uniformly smallest expected loss of best linear invariant estimators of u and b at $k+1$ stress levels at which life testing may occur, extrapolated to $\sigma = \frac{1}{\eta}$ (when it is assumed that (15) gives the exact variance of $X_T^*(\eta)$).

PROOF

Each of the statements in the demonstration of the proof of the first statement of Theorem II holds for $\alpha = 0, 1, \dots, k$. Let us suppose that there exists a linear function $\tilde{X}\left(\frac{1}{\sigma_\alpha}\right)$ of the ordered observations

$X_{1,\alpha}, X_{2,\alpha}, \dots, X_{n_\alpha,\alpha}$ and a point $u_\alpha + \zeta b$, $-\infty < \zeta < \infty$, along the $\frac{1}{\sigma_\alpha}$ ordinate, such that the expected squared deviation of $\bar{X}(\frac{1}{\sigma_\alpha})$ from $u_\alpha + \zeta b$ is at least as small as that of $X^*(\frac{1}{\sigma_\alpha})$ from $x_{1/\sigma_\alpha}, b$ for all combinations of values of u_α and b and smaller for at least one combination of values of u_α and b . Hence it is supposed that $X^*(\frac{1}{\sigma_\alpha})$ is an inadmissible linear combination of the ordered observations.

Suppose that $\bar{X}(\frac{1}{\sigma_\alpha})$ is not of the form $L_1 u^*(\frac{1}{\sigma_\alpha}) + L_2 b_\alpha^*$. Then by the generalized Gauss-Markov Theorem [4] there exists $\bar{\bar{X}}(\frac{1}{\sigma_\alpha})$ of the form $L_1 u^*(\frac{1}{\sigma_\alpha}) + L_2 b_\alpha^*$ such that $E(\bar{\bar{X}}(\frac{1}{\sigma_\alpha})) = E(\bar{X}(\frac{1}{\sigma_\alpha}))$ and $\text{Var}(\bar{\bar{X}}(\frac{1}{\sigma_\alpha})) < \text{Var}(\bar{X}(\frac{1}{\sigma_\alpha}))$ for all u_α and b . Thus,

$$\text{Var}(\bar{\bar{X}}(\frac{1}{\sigma_\alpha})) + [E(\bar{\bar{X}}(\frac{1}{\sigma_\alpha})) - (u_\alpha - \zeta b)]^2 < \text{Var}(\bar{X}(\frac{1}{\sigma_\alpha})) + [E(\bar{X}(\frac{1}{\sigma_\alpha})) - (u_\alpha - \zeta b)]^2$$

for all u_α and b . Hence, it may as well be supposed that

$$\bar{\bar{X}}(\frac{1}{\sigma_\alpha}) = S_{1,\alpha} u^*(\frac{1}{\sigma_\alpha}) + S_{2,\alpha} b_\alpha^*.$$

Then the expected loss function for $\bar{X}(\frac{1}{\sigma_\alpha})$ is

$$S_{1,\alpha}^2 A_\alpha + 2S_{1,\alpha} S_{2,\alpha} B_\alpha + S_{2,\alpha}^2 C_\alpha + [(S_{1,\alpha} - 1)u_\alpha + (S_{2,\alpha} - \zeta)b]^2 / b^2$$

which is assumed to be less than $A_\alpha - B_\alpha^2 / C_\alpha$ for all u_α and b . The value of $S_{1,\alpha}$ must then be equal to 1 if this inequality is to hold identically in u_α and b .

Thus, it is assumed that $\bar{X}\left(\frac{1}{\sigma_\alpha}\right) = u^*\left(\frac{1}{\sigma_\alpha}\right) + S_{2,\alpha} b_\alpha^*$ with expected loss given by

$$A_\alpha + 2S_{2,\alpha} B_\alpha + S_{2,\alpha}^2 C_\alpha + (S_{2,\alpha} - \zeta)^2 \quad (18)$$

The expression (18) is minimized with respect to ζ and $S_{2,\alpha}$ jointly when $\zeta = S_{2,\alpha} = -B_\alpha / C_\alpha$. Hence $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is an admissible linear combination of the observations at the α^{th} stress level, $\alpha = 0, 1, \dots, k$. The proof of admissibility for $X^*\left(\frac{1}{\sigma_\alpha}\right)$, $\alpha = 0, 1, \dots, k$, is similar to that referred to in the footnote on page 33. An alternative proof would begin with a demonstration that for every biased linear combination of the observations, there exists an unbiased combination with smaller risk (expected loss).

Suppose $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is not a minimax-risk linear combination of the observations. Then there exists a linear combination having maximum risk smaller than that of $X^*\left(\frac{1}{\sigma_\alpha}\right)$, which has constant risk with respect to u_α and b_α , $\alpha = 0, 1, \dots, k$, since loss is squared error divided by b_α^2 . The existence of such an estimator would thus imply that $X^*\left(\frac{1}{\sigma_\alpha}\right)$, $\alpha = 0, 1, \dots, k$, was inadmissible. Hence $X^*\left(\frac{1}{\sigma_\alpha}\right)$ is the unique (with probability 1) admissible minimax linear combination of the observations at the α^{th} stress level, $\alpha = 0, 1, \dots, k$. The uniqueness follows from the uniqueness of $u^*\left(\frac{1}{\sigma_\alpha}\right)$ and b_α^* , $\alpha = 0, 1, \dots, k$.

Now, consider

$$X_T^*(\eta) = \sum_{\alpha=0}^k L_\alpha(\eta) \left[u^*\left(\frac{1}{\sigma_\alpha}\right) - B_\alpha b_\alpha^* / C_\alpha \right],$$

the least-squares intercept at $\sigma = \frac{1}{\eta}$, where p_α , which represents the proportion of the n sample values tested at $\frac{1}{\sigma_\alpha}$, and $\frac{1}{\sigma_\alpha}$,

$\alpha = 0, 1, \dots, k$, are chosen according to the specifications of

Theorem I. It is assumed that $c \leq \sigma_\alpha \leq d$, $\alpha = 0, 1, \dots, k$, and $\frac{1}{\eta} < c$.

Let $\bar{X}(\eta) = \sum_{\alpha=0}^k L_\alpha(\eta) \sum_{i=1}^{n_\alpha} a_{i,\alpha} X_{i,\alpha}$, with $\sum_{\alpha=0}^k n_\alpha = n$, estimate a point

$u(\eta) + \zeta b$, $-\infty < \zeta < \infty$, on the ordinate η . Suppose that

a_i , $i = 1, 2, \dots, n_\alpha$, $p_\alpha = n_\alpha/n$, and σ_α , $\alpha = 0, 1, \dots, k$, are chosen so that the mean squared deviation of $\bar{X}(\eta)$ from $u(\eta) + \zeta b$ is less than or equal to the variance of $X_{i,\alpha}^*(\eta)$ for all b , $u(\eta)$, and u_α , $\alpha = 0, 1, \dots, k$. Suppose that the expectation of $\bar{X}(\eta)$ is not $u(\eta) + \zeta b$. Then the expected squared deviation of $\bar{X}(\eta)$ from its expected value is less than that of $\bar{X}(\eta)$ from $u(\eta) + \zeta b$. Hence, it is assumed that $E(\bar{X}(\eta)) = u(\eta) + \zeta b$ for all b , $u(\eta)$, and $u(\frac{1}{\sigma_\alpha})$, $\alpha = 0, 1, \dots, k$. Then when $\bar{X}(\eta)$ is of the form

$$\sum_{\alpha=0}^k L_\alpha(\eta) \left[u^*\left(\frac{1}{\sigma_\alpha}\right) + \tau_\alpha b_\alpha^* \right], \quad (19)$$

with variance

$$b^2 \sum_{\alpha=0}^k \left[L_\alpha^2(\eta) (A_\alpha + 2\tau_\alpha B_\alpha + \tau_\alpha^2 C_\alpha) \right], \quad (20)$$

it has uniformly smaller variance than any other linear combination with

uniform expectation $u(\eta) + \sum_{\alpha=0}^k L_{\alpha}(\eta) \tau_{\alpha} b = u(\eta) + \zeta b$ for any specified

combination of testing levels and allocation of the sample to the

$k+1$ levels. If any n_{α} is equal to 1, $u^*\left(\frac{1}{\sigma_{\alpha}}\right) + \tau_{\alpha} b_{\alpha}^*$ is taken to be $X_{1,\alpha}$ with variance $\pi^2 b^2/6$, $\alpha = 0, 1, \dots, k$.

The variance of $\bar{X}(\eta)$ is minimized independently of the value of p_{α} and $\frac{1}{\sigma_{\alpha}}$, $\alpha = 0, 1, \dots, k$ if $\tau_{\alpha} = -B_{\alpha}/C_{\alpha}$. Hence, $X^*(\eta)$ is admis-

sible among linear combinations of n sample observations when $\frac{1}{\sigma_{\alpha}}$

and p_{α} , $\alpha = 0, 1, \dots, k$, are fixed. Then by Theorem I and the

reasoning applied in proving the first statement of this theorem, $X_T^*(\eta)$

is the unique admissible minimax linear combination of n sample failure-

time logarithms observed at $\sigma_1, \sigma_2, \dots, \sigma_k$, $c \leq \sigma_{\alpha} \leq d$, $\alpha = 0, 1, \dots, k$,

and extrapolated to $\sigma = \frac{1}{\eta}$, $\frac{1}{\eta} < c$ (under the assumption that (15) gives the exact variance of $X^*(\eta)$).

On the basis of the preceding derivation and the assumption (concerning

the variance of $X^*(\eta)$) it follows immediately that

$$X_T^*(\eta) = \sum_{\alpha=0}^k L_{\alpha}(\eta) \left[u^*\left(\frac{1}{\sigma_{\alpha}}\right) - \frac{B_{\alpha} b_{\alpha}^*}{(1+C_{\alpha})} - \frac{B_{\alpha} b_{\alpha}^*}{C_{\alpha}(1+C_{\alpha})} \right], \text{ with expectation}$$

$$\sum_{\alpha=0}^k L_{\alpha}(\eta) \left[u_{\alpha} - \frac{B_{\alpha} b}{1+C_{\alpha}} - \frac{B_{\alpha} b}{C_{\alpha}(1+C_{\alpha})} \right] \text{ and variance } \sum_{\alpha=0}^k L_{\alpha}(\eta) \left[A_{\alpha} - B_{\alpha}^2/C_{\alpha} \right], \text{ is}$$

the linear combination with uniformly smallest expected loss of best linear invariant estimators of u and b at $k+1$ stress levels at which life testing may occur, extrapolated to $\sigma = \frac{1}{\eta}$. It is interesting to note that when the model is given by (8) and (9) plus the assumption of a Gaussian distribution for the observations,

$$b^2 \sum_{\alpha=0}^k L_{\alpha}^2(\eta)/n_{\alpha} \text{ is the exact variance of } X^*(\eta) = \sum_{\alpha=0}^k L_{\alpha} \sum_{i=1}^{n_{\alpha}} x_{i,\alpha} / n_{\alpha}.$$

A COMPARISON OF THE TRADITIONAL AND THE DERIVED DESIGNS

As an illustration of the result given by Theorem I, consider the following example. It is assumed that u is of the form $\beta_0 + \beta_1\left(\frac{1}{\sigma}\right) + \beta_2\left(\frac{1}{\sigma}\right)^2 + \beta_3\left(\frac{1}{\sigma}\right)^3 + \beta_4\left(\frac{1}{\sigma}\right)^4$ and that 10 items are to be tested until failure over the stress interval $\frac{1}{3\sqrt{2}} \leq \sigma \leq \frac{1}{\sqrt{2}}$. Using a traditional design specifying equal numbers of items tested at equal intervals over the testing domain, one obtains the following.

$$\begin{array}{ccccc} \frac{1}{\sigma_4} = \sqrt{2} & \frac{1}{\sigma_3} = 3\sqrt{2}/2 & \frac{1}{\sigma_2} = 2\sqrt{2} & \frac{1}{\sigma_1} = 5\sqrt{2}/2 & \frac{1}{\sigma_0} = 3\sqrt{2} \\ n_4 = 2 & n_3 = 2 & n_2 = 2 & n_1 = 2 & n_0 = 2 \end{array}$$

For optimum estimation at $\sigma = \frac{1}{4\sqrt{2}}$, the theorem specifies approximately the design given below.

$$\begin{array}{ccccc} \frac{1}{\sigma_4} = \sqrt{2} & \frac{1}{\sigma_3} = 2\sqrt{2}-1 & \frac{1}{\sigma_2} = 2\sqrt{2} & \frac{1}{\sigma_1} = 2\sqrt{2}+1 & \frac{1}{\sigma_0} = 3\sqrt{2} \\ n_4 = 1 & n_3 = 2 & n_2 = 2 & n_1 = 3 & n_0 = 2 \end{array}$$

The least-squares curves for the two sets of 10 observations have variances at $\sigma = \frac{1}{4\sqrt{2}}$ equal to approximately (to the nearest integer) $2912 b^2$ for the traditional design and $1238 b^2$ for the derived design specified by the theorem.

It is shown in [7] that for b known, the best linear invariant estimator of u_α , for $n_\alpha \geq 2$, is $\hat{u}(\frac{1}{\sigma_\alpha}) = u^*(\frac{1}{\sigma_\alpha}) - (B_\alpha/C_\alpha)(b_\alpha^* - b)$, with mean squared error (variance, since $\hat{u}(\frac{1}{\sigma_\alpha})$ is unbiased) $[A_\alpha - B_\alpha^2/C_\alpha] b^2$,

$\alpha = 0, 1, \dots, k$. The variance values given above for the two designs are, therefore, also appropriate for $\hat{u}(\eta) = \sum_{\alpha=0}^k L_\alpha(\eta) [X^*(\frac{1}{\sigma_\alpha}) + (B_\alpha/C_\alpha)b]$,

with B_α/C_α taken to be $-E(Y_{1,\alpha})$ for any n_α equal to 1, $\alpha = 0, 1, \dots, k$.

If b is not known, then the best linear unbiased estimator of this parameter based on any given design can easily be shown to be

$$\sum_{\alpha=0}^k \frac{b_\alpha^*/C_\alpha}{\sum_{\alpha=0}^k \left(\frac{1}{C_\alpha}\right)}, \text{ with variance } b^2 / \sum_{\alpha=0}^k \left(\frac{1}{C_\alpha}\right). \text{ The best linear invariant}$$

estimator of b based on any given design is then

$$\frac{\sum_{\alpha=0}^k b_{\alpha}^* / c_{\alpha}}{\sum_{\alpha=0}^k \left(\frac{1}{c_{\alpha}} \right) \left(1 + 1 / \sum_{\alpha=0}^k \left(\frac{1}{c_{\alpha}} \right) \right)} = \frac{\sum_{\alpha=0}^k b_{\alpha}^* / c_{\alpha}}{1 + \sum_{\alpha=0}^k \left(\frac{1}{c_{\alpha}} \right)} \quad \text{with mean squared error given by}$$

$$b^2 / \left(1 + \sum_{\alpha=0}^k \left(\frac{1}{c_{\alpha}} \right) \right).$$

For the traditional design the variance of the best linear unbiased estimator of b is $0.142 b^2$ and the mean squared error of the best linear invariant estimator is $0.125 b^2$. For the derived design, the two corresponding values for the expected squared deviation for estimators of b are based on those obtained at only the four stress levels for which n_{α} , $\alpha = 0, 1, \dots, k$, is greater than 1. They are equal to $0.141 b^2$ and $0.124 b^2$, respectively.

The uniformly minimum-variance unbiased estimator of u at $\sigma = \frac{1}{\eta}$ under either model is $u^*(\eta) = \sum_{\alpha=0}^k L_{\alpha}(\eta) u^*\left(\frac{1}{\sigma_{\alpha}}\right)$, where for any n_{α} equal to 1, $u^*\left(\frac{1}{\sigma_{\alpha}}\right)$ will be taken to be $X_{1,\alpha} - E(Y_{1,\alpha}) \sum_{i=0}^k a_{i,\alpha} b_i^*$, with

$$a_{i,\alpha} = \frac{L_{\alpha}(\eta) E(Y_{1,\alpha}) / c_i + \sum_{\substack{j=1 \\ j \neq i}}^k [L_i(\eta) B_j / (c_i c_j) - L_j(\eta) B_i / (c_i c_j)]}{L_{\alpha}(\eta) E(Y_{1,\alpha}) \sum_{j=1}^k (1/c_j)} \quad \alpha = 0, 1, \dots, k.$$

Here, the number of coefficients of the form $a_{1,\alpha}$ at the α^{th} level is equal to 1 minus the number of testing levels for which n_α is equal to 1; and $E(Y_{1,\alpha})$ is the negative of Euler's constant, or approximately $-.577216$, $\alpha = 0, 1, \dots, k$. For the traditional model the variance of $u^*(\eta)$ is $2936 b^2$, and for the derived model it is $1248 b^2$. The amount of improvement obtained by using the best linear invariant estimator of $u(\eta)$ rather than $u^*(\eta)$ is trivial in both of these cases.

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APPENDIX B

EXACT THREE-ORDER-STATISTIC CONFIDENCE BOUNDS ON RELIABILITY PARAMETERS UNDER WEIBULL ASSUMPTIONS

INTRODUCTION

Assume that a random sample of n items is subjected to a life test until m (with $2 \leq m \leq n \leq 25$) of the items have failed. Assume further that the random variable T which represents an observable failure time from the population from which the sample of failure times is selected has the two-parameter Weibull density given by

$$\lim_{\Delta t \rightarrow 0} \frac{P[t < T \leq t + \Delta t]}{\Delta t} = f_{\delta, b}(t) = \begin{cases} (1/\delta b)(t/\delta)^{(1/b)-1} \exp\{-(t/\delta)^{1/b}\}, & t > 0 \\ 0, & \text{otherwise} \end{cases}$$

with δ and b both positive.

(1)

There are two related problems which are among the most important associated with the life-testing situation. First, one may suppose that a required life t_g is specified and a lower confidence bound, based on the censored sample, is sought for reliability or the survival proportion, $R(t_g) = \exp\{-(t_g/\delta)^{1/b}\}$, at time t_g . For the second and alternative problem a survival proportion R is given. Then a lower confidence bound is sought for $t_R = \delta(\log(1/R))^b$, the reliable life corresponding to R or, equivalently, for $x_R = u + b \log \log (1/R)$, the log reliable life, where u is equal to $\log \delta$ and all logarithms are natural. The

parameter u is a location parameter of the distribution of $X = \log T$, and b is a scale parameter of this distribution.¹ The bounds for t_R and x_R are often referred to as lower tolerance limits, and are confidence bounds for the $100(1-R)$ percent points of the distributions of T and of X , respectively, where R is the specified proportion between 0 and 1.

A method of obtaining confidence bounds on reliability parameters widely used for the Weibull distribution as well as for many others is as follows. Consider the observed ordered failure times $T_1 \leq T_2 \leq \dots \leq T_m$. For any T_k , a lower confidence bound on $R(T_k)$ at level $1 - \alpha$ can be obtained from $v_{\alpha}(n-k+1, k)$, the 100α percent point of the beta distribution with $n-k+1$ and k degrees of freedom (see Kao and Goode [1]). This bound serves also as a conservative $(1 - \alpha)$ -level bound for $R(t_g)$, for any $t_g < T_k$. Similarly, if $v_{\alpha}(n-k+1, k)$ is greater than R for some k , a lower confidence bound on t_R , with level at least $1 - \alpha$, is given by the k^{th} observed failure time T_k .

This method, however, makes no use of information concerning the form of the underlying distribution of the populations sampled. It is in fact a nonparametric method requiring only the assumption that the unordered observations are independent and identically and continuously distributed. It seems likely that one could obtain improved bounds on the reliability parameters by assuming (correctly) that sampling is from the two-parameter Weibull distribution. In particular, one would ex-

¹ The distribution of the random variable X is the extreme-value distribution of smallest values.

pect a possible improvement when the required life t_g is small compared with the sample failure time which immediately follows it, or in the case in which a tolerance limit is desired, when v_α greatly exceeds R . If R is larger than any v_α , the nonparametric method is, in fact, completely inapplicable. In the following discussion, other methods for obtaining bounds are derived.

TESTS AND CONFIDENCE SETS FOR THE PARAMETER b

TESTS AND CONFIDENCE SETS BASED ON ALL THE ORDER STATISTICS

The two parameters, reliability and reliable life, for which confidence bounds are sought are

$R(t_g) = \exp\{-(t_g/\delta)^{1/b}\}$ and $x_R = u + b \log \log (1/R)$ or $t_R = \delta(\log(1/R))^b$, respectively. Thus, both are simply functions of the parameters δ (or u) and b . Therefore, bounds on the reliability parameters can be determined from distribution percentage points corresponding to appropriate functions of estimates of δ (or u) and b .

First consider estimates of b (functions of $T_1 \leq T_2 \leq \dots \leq T_m$) and confidence bounds, based on these estimates, which can be placed on b alone. The problem of obtaining such bounds, or tests from which such bounds are derived, is invariant under a change in scale in the time space or a change of location in log time space. A maximal invariant under this transformation is $Z = (Z_2, Z_3, \dots, Z_n) = (T_2/T_1, T_3/T_1, \dots,$

T_m/T_1) or equivalently, $\log Z = [\log (T_2/T_1), \log (T_3/T_1), \dots, \log (T_m/T_1)] = (X_2 - X_1, X_3 - X_1, \dots, X_m - X_1)$. Hence, tests concerning b and confidence bounds on b will be independent of δ or u if and only if they depend on T_1, T_2, \dots, T_m or X_1, X_2, \dots, X_m^1 only through Z .

The joint probability density function of $T_1 \leq T_2 \leq \dots \leq T_m$ is given by

$$f_{\delta, b}(t_1, t_2, \dots, t_m) = \frac{n!}{(n-m)!} \left(\frac{1}{b\delta}\right)^m \prod_{i=1}^m \left(\frac{t_i}{\delta}\right)^{(1/b)-1} \exp \left\{ - \left[\sum_{i=1}^{m-1} \left(\frac{t_i}{\delta}\right)^{1/b} + (n-m+1) \left(\frac{t_m}{\delta}\right)^{1/b} \right] \right\}, \quad 0 \leq t_1 \leq t_2 \leq \dots \leq t_m \leq t_n, \quad (2)$$

so that the joint density of $Z_2 \leq Z_3 \leq \dots \leq Z_m$ is

$$f_b(z_2, z_3, \dots, z_m) = \frac{n!(m-1)! \left(\frac{1}{b}\right)^{m-1}}{(n-m)!} \frac{\prod_{i=2}^m z_i^{(1/b)-1}}{\left[1 + \sum_{i=2}^{m-1} z_i^{1/b} + (n-m+1) z_m^{1/b} \right]^m}, \quad 1 \leq z_2 \leq z_3 \leq \dots \leq z_m. \quad (3)$$

Consider any invariant test $\phi = \phi(Z)$ of $H: b \geq b_0$ versus $K: b < b_0$ which accepts H when $\phi = 0$ and rejects H when $\phi = 1$. One chooses a significance level α , $0 < \alpha < 1$, and looks for an invariant test which rejects H with probability $\leq \alpha$ when $b \geq b_0$ and which, in some sense, maximizes $\mathbb{E} \phi$. X_1, X_2, \dots, X_m are order statistics from the extreme-value distribution of smallest values, the distribution of the random variate $X = \log T$.

the power $\beta_{\hat{\theta}}(b)$ (or probability of rejecting H) when $b < b_0$. The boundary of the acceptance region of a uniformly most powerful invariant test $\hat{\theta}_0$ (most powerful against all alternative hypotheses) yields a uniformly most accurate invariant upper bound \bar{b}_{\min} for b . Thus, $P_b\{b \leq \bar{b}_{\min}\} \geq 1-\alpha$ for all b , and furthermore, for any $b' > b$, $P_b\{\bar{b}_{\min} \geq b'\}$ is minimum among tests based on 2. It can be demonstrated that the Neyman-Pearson Fundamental Lemma (Lehmann [2]) applied to (3) for a given n and $m > 2$ and given simple hypothesis, $b = b_0$, will yield a most powerful invariant test which varies accordingly as the simple alternative $b = b_1$ changes. Thus, there is no test of H which is uniformly most powerful among invariant tests for all alternatives.

One might then naturally consider basing tests and confidence sets on estimators of b which have certain optimality properties in terms of their ability to estimate. From [3], [4] and [5] it might be concluded that likely candidates for such bases for tests, etc., would be the best linear invariant estimator and the maximum-likelihood estimator. Unfortunately, however, the derivations of the distributions of these estimators of b , u , and $x_R = u + b \log \log(1/R)$ for $m > 2$ are very difficult, if not impossible, to obtain except by simulation methods.¹

¹ Tables from which one may obtain confidence bounds on $R(t_g)$ or on t_R have been computed by Johns and Lieberman [6] by simulating the distribution of a function of approximations to the best linear invariant estimates of u and b . These tables can be used for n equal to 10, 15, 20, 30, 50, and 100, and 4 values of m for each n .

A locally most powerful invariant test depends upon the maximum-likelihood estimator of b .

Thus, one is faced with a situation in which statistics which may possibly be optimum in terms of their ability to estimate have not provided an analytical basis for exact tests concerning, or exact confidence bounds on, the parameters they are estimating.

One is thus led to consider estimators whose distributions can be determined exactly and then to compare the properties of these estimators with those of the best linear invariant estimators, the expected loss of which is known or can be calculated for $n \leq 25$. We first perform the following derivation proceeding from (3). Let $V_1 = 1$, $V_j = Z_j^{1/b}$, $j = 2, 3, \dots, m$. Then,

$$f(v_2, v_3, \dots, v_m) = \frac{n!(m-1)!}{(n-m)!} \frac{1}{\left[n + \sum_{i=2}^m (n-i+1)(v_i - v_{i-1}) \right]^m} \quad (4)$$

$$1 = v_1 \leq v_2 \leq \dots \leq v_m.$$

Thus, if

$$F = \sum_{i=2}^m \frac{n-i+1}{n(m-1)} (v_i - v_{i-1}) = \sum_{i=2}^m \frac{n-i+1}{n(m-1)} (Z_i^{1/b} - Z_{i-1}^{1/b}),$$

then

$$f(F) = \frac{(m-1)^m F^{m-2}}{[1+(m-1)F]^m}, \quad F \geq 0, \quad (5)$$

or

$$F^0 = \sum_{i=2}^m \frac{n-i+1}{n(m-1)} \left(Z_i^{1/b_0} - Z_{i-1}^{1/b_0} \right) \text{ is distributed as } F[2(m-1), 2], \text{ Snedecor's}$$

F with $2(m-1)$ and 2 degrees of freedom, when $b = b_0$. A test \hat{t}_A , at level α , based on the statistic F^0 will therefore reject $H: b \geq b_0$ when

$$\sum_{i=2}^m \frac{n-i+1}{n(m-1)} \left(Z_i^{1/b_0} - Z_{i-1}^{1/b_0} \right) \text{ is less than } F_{\alpha}[2(m-1), 2], \text{ the } 100\alpha \text{ percent point}$$

of the F distribution with the appropriate number of degrees of freedom. The value of $F_{\alpha}[2(m-1), 2]$ as a function of α and m can be calculated by letting

$$W^0 = [1 + (m-1)F^0]^{-1} = n \left[1 + \sum_{i=2}^{m-1} Z_i^{1/b_0} + (n-m+1)Z_m^{1/b_0} \right]^{-1}$$

and finding the distribution of W^0 when $b = b_0$. From (5) one obtains

$$f(W^0) = (m-1)(1-W^0)^{m-2}, \quad 0 \leq W^0 \leq 1,$$

and

$$P[F^0 \leq F_{\alpha}[2(m-1), 2]] = P[W^0 \geq \bar{W}^0] = (1-\bar{W}^0)^{m-1}. \quad (6)$$

If (6) is set equal to α , then \bar{W}^0 is seen to be $1 - \alpha^{1/(m-1)}$ and

$$F_{\alpha}[2(m-1), 2] \text{ is equal to } \frac{1}{m-1} \frac{\alpha^{1/(m-1)}}{1 - \alpha^{1/(m-1)}}.$$

An upper confidence bound at level $1-\alpha$ for b may be obtained by setting

$$F = \frac{\sum_{i=2}^m (n-i+1)(Z_i^{1/b} - Z_{i-1}^{1/b})}{n(m-1)} \text{ equal to } F_{\alpha}[2(m-1), 2] \text{ and solving for } b.$$

One then uses some good estimate of b as a first approximation and Newton-Raphson iteration procedures until $F-F_\alpha[2(m-1), 2]$ is sufficiently small.

TESTS AND CONFIDENCE SETS BASED ON TWO ORDER STATISTICS

Next it will be demonstrated that, for m sufficiently small, a family of confidence bounds based on $Z_m = T_m/T_1$ alone is preferable to that based on the test $\hat{\phi}_A$ (just derived). To obtain the density function for Z_m , one may successively integrate out $Z_2^{1/b}$, $Z_3^{1/b}$, ..., $Z_{m-1}^{1/b}$ from (3). Thus,

$$f(z_m) = \frac{n!}{(n-m)!(m-2)!} \sum_{k=0}^{m-2} \left(\frac{-1}{b}\right)^k \binom{m-2}{k} \frac{z_m^{(1/b)-1}}{\left[(m-k-1) + (n-m-k+1)z_m^{1/b}\right]^2}, \quad (7)$$

$$1 \leq z_m < \infty.$$

Now, let $V = Z_m^{1/b} \geq 1$. A test $\hat{\phi}_1$ based on Z_m , therefore, rejects $H: b \geq b_0$ whenever $V_0 = Z_m^{1/b_0}$ is less than $C_1(\alpha)$ (or $\log Z_m$ is less than $b_0 \log C_1(\alpha)$), with $C_1(\alpha)$ determined from the expression

$$\frac{n!}{(n-m)!(m-2)!} \sum_{k=0}^{m-2} (-1)^k \binom{m-2}{k} \frac{1/(n-m+k+1)}{\left[(m-k-1) + (n-m+k+1)C_1(\alpha)\right]} = 1 - \alpha. \quad (8)$$

An upper confidence bound $\bar{b}_1(\alpha)$ for b will then be given by

$\bar{b}_1(\alpha) = \log Z_m / \log C_1(\alpha) = \log Z_m / \log C_1(\alpha)$. In order to ascertain whether there is a unique root of the equation (8) which is greater than unity, let $D_1(\alpha) = C_1(\alpha) - 1$ and reject H when $Z_m^{1/b_0} - 1 < D_1(\alpha)$.

Then (8) may be expressed as a function of $D_1(\alpha)$

$$\frac{n!}{(n-m)!(m-2)!} \sum_{k=0}^{m-2} (-1)^k \binom{m-2}{k} \frac{1/(n-m+k+1)}{[n+(n-m+k+1)D_1(\alpha)]} = 1-\alpha$$

or as a polynomial $g(D_1(\alpha))$ given by

$$\begin{aligned} (1-\alpha) D_1(\alpha)^{m-1} \prod_{k=1}^{m-1} (n-m+k) - \alpha \left\{ D_1(\alpha)^{\binom{m-1}{1}} \sum_{i=1}^{m-2} n \prod_{\substack{k=1 \\ k \neq i}}^{m-1} (n-m+k) \right. \\ \left. + \dots + D_1(\alpha)^{\binom{m-1}{m-2}} \sum_{i=1}^{m-2} n^{m-2} (n-m+i) + n^{m-1} \right\} = 0. \end{aligned} \quad (9)$$

For $0 < \alpha < 1$, the coefficient of the first term of the polynomial is positive and each of the remaining $m-1$ terms is negative. Thus by Descartes' Rule of Signs [7], there is no more than one positive root. Also, since $g(0) < 0$ and $g(D_1(\alpha))$, for $D_1(\alpha)$ very large, is positive, there is at least one positive root. Therefore, there is a unique $D_1(\alpha) > 0$ and a unique $C_1(\alpha) = D_1(\alpha) + 1 > 1$.

It can be easily demonstrated from equation (9) that when n is sufficiently large compared with m , $D_1(\alpha) = \frac{\alpha^{1/(m-1)}}{1 - \alpha^{1/(m-1)}} = (m-1)F_\alpha[2(m-1), 2]$ and from Table IX in [8] it may be corroborated that, for $m \leq 20$, $LC_1(\alpha) = \log(1+D_1(\alpha))$ is approximately given by

$$\log \left[n \sum_{i=2}^m \frac{1}{n-i+1} \frac{\alpha^{1/(m-1)}}{(m-1)(1-\alpha^{1/(m-1)})} + 1 \right] \quad (10)$$

or

$$\log \left[n \sum_{i=2}^m \frac{1}{n-i+1} F_{\alpha}[2(m-1), 2] + 1 \right].$$

This result has been demonstrated empirically using the fact that (10) was used as a first approximation in the Newton-Raphson iterative procedure employed to generate $LC_1(\alpha)$ and the amount of deviation from this first guess is shown in the machine computation output to be small. Thus, except for large m , the test $\hat{\phi}_1$ rejects $H: b \geq b_0$ approximately when

$$\log Z_m / \left\{ b_0 \log \left[n \sum_{i=2}^m \frac{1}{n-i+1} F_{\alpha}[2(m-1), 2] + 1 \right] \right\} < 1.$$

COMPARISON OF BOUNDS BASED ON $\hat{\phi}_1$ AND $\hat{\phi}_A$

Very roughly, with probability $1 - \gamma$ the statistic $\log Z_m$ is greater

than $b \log \left[n \sum_{i=2}^m \frac{1}{n-i+1} F_{\gamma}[2(m-1), 2] + 1 \right]$ and with probability γ is

less than this value, as long as m is not large. Next, the statistic

$$\sum_{i=2}^m (n-i+1) \left(\frac{Z_i^{1/b_0} - Z_{i-1}^{1/b_0}}{n(m-1)} \right) = \frac{1}{n} \left[\sum_{i=2}^m \left(\frac{Z_i^{1/b_0} - 1}{m-1} \right) + (n-m+1) \left(\frac{Z_m^{1/b_0} - 1}{m-1} \right) \right], \quad Z_1 = 1,$$

upon which the test $\hat{\phi}_A$ is based can be considered to be $\frac{n-1}{n} \left(\frac{Z_{\mu}^{1/b_0} - 1}{m-1} \right)$

for some μ with $2 \leq j \leq \mu \leq k \leq m$, j , k , and m integers and

$Z_j \leq Z_\mu \leq Z_k$. (When $m = 2$, $\mu = 2$, and $\hat{\theta}_A$ is equivalent to $\hat{\theta}_1$). Then, from (5) H is rejected on the basis of $\hat{\theta}_A$ when

$$\log Z_\mu / b_0 \log \left[\frac{n(m-1)}{n-1} F_\alpha[2(m-1), 2] + 1 \right] < 1,$$

with the γ^{th} percentage point of the distribution of $\log Z_\mu$ equal to

$$b \log \left[\frac{n(m-1)}{n-1} F_\gamma[2(m-1), 2] + 1 \right].$$

For either of the two $(1-\alpha)$ -level confidence bounds based on $\hat{\theta}_1$ and $\hat{\theta}_A$ then, with approximate probability γ for small m , the upper bound \bar{b} is less than

$$\frac{b \log(F_\gamma[2(m-1), 2] x + 1)}{\log(F_\alpha[2(m-1), 2] x + 1)}, \quad (11)$$

where

$$x = \frac{n}{n-1}(m-1), \quad x = n \sum_{i=2}^m \frac{1}{n-i+1} \geq n \sum_{i=2}^m \frac{1}{n-i} = \frac{n(m-1)}{n-1} > 1.$$

(When $m=2$, the two expressions for x are equal.) At confidence level $1-\alpha$, therefore, the test ($\hat{\theta}_1$ or $\hat{\theta}_A$) which yields the larger value of (11) for $\gamma < \alpha$ ($1-\gamma > 1-\alpha$) may be considered superior since it is therefore the more accurate bound. Accuracy of the bound is in the sense of the definition of a most accurate bound as found in [2] and on page 5.

If the expression

$$\frac{\log(ax+1)}{\log(cx+1)}, \quad x > 0, \quad 0 < a < c, \quad (12)$$

is differentiated, one obtains

$$\frac{-\log(ax+1)\frac{c}{cx+1} + \log(cx+1)\frac{a}{ax+1}}{\log^2(cx+1)} = \frac{-\frac{ax+1}{ax}\log(ax+1) + \frac{cx+1}{cx}\log(cx+1)}{\frac{cx+1}{c} \cdot \frac{ax+1}{a} \cdot \frac{1}{x} \log^2(cx+1)} \quad (13)$$

Now consider $\frac{y+1}{y}\log(y+1)$ whose derivative is $\frac{1}{y} + \log(1+y)(-1/y^2)$.

Since $y > \log(1+y)$, this derivative is always positive and $\frac{y+1}{y}\log(1+y)$ is increasing in $\frac{1}{y}$. Therefore, since $a < c$, the right hand term in the numerator of (13) is larger than the left, (13) is always positive, and (12) is increasing in x . Hence the larger the value of x , $\frac{n(m-1)}{n-1}$ or $n \sum_{i=2}^m \frac{1}{n-i+1}$, the more desirable the associated confidence bound.

Then, since $n \sum_{i=2}^m \frac{1}{n-i+1} > \frac{-1}{-1}$ for $m > 2$, an upper confidence bound based on $\hat{\tau}_1$ is more accurate than one based on $\hat{\tau}_A$ for small m .

UNBIASEDNESS OF $\hat{\tau}_1$

The test $\hat{\tau}_1(Z_m)$ can be shown to be unbiased in the following manner.

The power function $\beta_{\hat{\tau}_1}(b)$ of $\hat{\tau}_1$ can be expressed as a function of $C_1(\alpha)$,

$$\beta_{\hat{\tau}_1}(b) = E_b(\hat{\tau}_1) = 1 - \frac{n!}{(n-m)!(m-2)!} \sum_{k=0}^{m-2} (-1)^k \binom{m-2}{k} \frac{1}{[(m-k-1)+(n-m+k+1)(C_1(\alpha))^b]^{b/b}} \quad (13)$$

¹ The form of the right side of (13) and this step of the proof were suggested by Prof. Wayne F. Smith of the University of California at Los Angeles.

and the derivative $\beta'_{\hat{\theta}_0}(b)$ thus has the form

$$\beta'_{\hat{\theta}_1}(b) = \frac{-n!}{(n-m)!(m-2)!} (C_1(\alpha))^{b_0/b} \log(C_1(\alpha))^{b_0} \sum_{k=0}^{m-2} \frac{(-1)^k}{b^2} \binom{m-2}{k} \frac{1}{[(m-k-1) + (n-m+k+1)(C_1(\alpha))^{b_0/b}]^2}.$$

(14)

Then from (5) and (7),

$$\beta'_{\hat{\theta}_1}(b) = -\frac{1}{b^2} (C_1(\alpha))^{b_0/b} \log(C_1(\alpha))^{b_0} \cdot f(v) \Big|_{v=(C_1(\alpha))^{b_0/b}} < 0$$

since $C_1(\alpha) > 1$. Hence, $\beta_{\hat{\theta}_1}(b)$ is monotonically decreasing in b . For $\hat{\theta}_1$ the two criteria for unbiasedness are satisfied, that is

$$\beta_{\hat{\theta}_1}(b) \leq \alpha \text{ for } b \geq b_0$$

$$\beta_{\hat{\theta}_1}(b) > \alpha \text{ for } b < b_0.$$

Satisfaction of the first of these criteria insures that the test is of size α or that $\sup \beta_{\hat{\theta}_1}(b) = \alpha$ for $b \geq b_0$ since $\beta_{\hat{\theta}_1}(b_0) = \alpha$.

INDUCED TESTS AND CONFIDENCE SETS FOR RELIABILITY AND RELIABLE LIFE

INDUCED TESTS AND CONFIDENCE SETS FOR RELIABILITY BASED ON ALL THE ORDER STATISTICS

Suppose that the matter of concern is the problem of testing that

$$R(t_g) = \exp[-(t_g/b)^{1/b}], \text{ the proportion of the population surviving}$$

at a specified time t_g , is less than some given R_0 . Let

$\xi = \delta^{1/b} = t_g^{1/b} / \log[1/R(t_g)]$. The distribution of

$$\frac{2m\hat{\xi}}{\xi} = \frac{2 \left(\sum_{i=1}^{m-1} T_i^{1/b} + (n-m+1)T_m^{1/b} \right)}{\xi}$$

is χ_{2m}^2 ; and when b is known (see [10]) a uniformly most powerful

α' -level test $\hat{\delta}_2$ of $H': \delta^{1/b} \leq \delta_0^{1/b}$, or equivalently, since $R(t_g) = \exp[-(t_g/\delta_0)^{1/b}]$, $H': R(t_g) \leq R_0 = \exp[-(t_g/\delta_0)^{1/b}]$ versus $K: R(t_g) > R_0$

is: Reject H' when $2m\hat{\xi}/t_g$ is greater than $\chi_{2m}^2(1-\alpha')/\log 1/R_0$ (accept otherwise). Therefore H is accepted at level α' if

$$2 \left[\sum_{i=1}^{m-1} \frac{T_i^{1/b}}{t_g} + (n-m+1) \frac{T_m^{1/b}}{t_g} \right] \leq \chi_{2m}^2(1-\alpha')/\log(1/R_0). \quad (15)$$

The left side of (15) increases monotonically as b decreases if

$t_g < T_1^{1/b} / \Delta^{1/b} \cdot T_2^{1/b} / \Delta^{1/b} \cdot (n-m+1)T_m^{1/b} / \Delta^{1/b}$, with $\Delta = T_1^{1/b} + T_2^{1/b} + \dots + (n-m+1)T_m^{1/b}$, and certainly if $t_g \leq (T_1 \cdot T_2 \cdot \dots \cdot T_m)^{1/m}$. Thus for

t_g sufficiently small, if H' is accepted under the assumption that $b = b_0$ when the value of b_0 is inserted for b in (15), then it would surely be accepted if b were greater than b_0 and the true value of b were somehow to be substituted for the symbol b in (15).

Hence one may form an induced test ϕ^* of H^* ($H: b \geq b_0$ is true and H' is true) versus K^* (H^* is not true) which uses the test ϕ_2 with $b = b_0$ in (15) to test H' only if the hypothesis H is accepted on the basis of the test ϕ_1 . Now, consider

$$m\hat{\xi} = \left[\sum_{i=1}^{m-1} T_1^{1/b} + (n-m+1)T_m^{1/b} \right] = \sum_{i=1}^m (n-i+1) (T_i^{1/b} - T_{i-1}^{1/b}), (T_0 = 0).$$

The joint density of $W_i = T_i^{1/b}$, $i = 1, 2, \dots, m$, is

$$f(w_1, w_2, \dots, w_m) = \left[\prod_{i=1}^m (n-i+1) \delta^{1/b} \right] \exp \left\{ -\frac{1}{\delta^{1/b}} [n w_1 + (n-1)(w_2 - w_1) + \dots + (n-m+1)(w_m - w_{m-1})] \right\},$$

$$0 \leq w_1 < \infty, \\ w_1 \leq w_2 < \infty, \\ w_{m-1} \leq w_m < \infty.$$

Thus the joint density of $S_i = (n-i+1)(W_i - W_{i-1}) = (n-i+1)(T_i^{1/b} - T_{i-1}^{1/b})$,

$T_0 = 0$, $i = 1, 2, \dots, m$, is

$$f(s_1, s_2, \dots, s_m) = \left(\frac{1}{\delta^{1/b}} \right)^m \exp \left[-\left(\frac{1}{\delta^{1/b}} \sum_{i=1}^m s_i \right) \right],$$

$$0 \leq s_i < \infty, i=1, 2, \dots, m$$

and each $S_i = (n-i+1) (T_i^{1/b} - T_{i-1}^{1/b})$, $i = 1, 2, \dots, m$, has an independent gamma distribution with scale parameter $\delta^{1/b}$. Therefore, by a result of Lukacs in [9], $m\hat{\xi} = \sum_{i=1}^m (n-i+1)(T_i^{1/b} - T_{i-1}^{1/b})$ is independent of any of $m-1$ linear combinations of

$$1, \frac{(n-1)[T_2^{1/b} - T_1^{1/b}]}{nT_1^{1/b}}, \frac{(n-2)[T_3^{1/b} - T_2^{1/b}]}{nT_1^{1/b}}, \dots \text{ and } \frac{(n-m+1)[T_m^{1/b} - T_{m-1}^{1/b}]}{nT_1^{1/b}}$$

which are equal to

$$1, \frac{n-1}{n} (Z_2^{1/b} - 1), \frac{n-2}{n} (Z_3^{1/b} - Z_2^{1/b}), \dots, \text{ and } \frac{(n-m+1)}{n} (Z_m^{1/b} - Z_{m-1}^{1/b}).$$

Therefore, $\hat{\xi}$ is independent of $Z_2^{1/b}$, $Z_3^{1/b}$, ..., and $Z_m^{1/b}$ and hence of Z_m . Darroch and Silvey [11] show that when the two tests which form the induced test are similar ($\beta_{\xi_1}(b_0) = \alpha$, $\beta_{\xi_2}(\xi_0) = \alpha'$), of size α and α' , respectively, and are based on independent test statistics,¹ then the induced test is similar and of size $1-(1-\alpha)(1-\alpha')$. Since unbiasedness of a test with a continuous power function implies both that the test is similar and that the size is equal to the significance level, these conditions are satisfied for both ξ_1 and ξ_2 (see [10]). Thus ξ^* is similar and of size $1-(1-\alpha)(1-\alpha')$.

Now, just as the tests ξ_1 and ξ_2 have been combined to form the induced test ξ^* , the boundaries of the acceptance regions of the two tests may be combined to form joint confidence bounds for b and $R(t_g)$ at confidence level $(1-\alpha)(1-\alpha')$. This is possible because ξ^* is similar and of size $1-(1-\alpha)(1-\alpha')$. From the acceptance region of the test ξ_2 of $H': R(t_g) \leq R_0$ versus $K': R(t_g) > R_0$, with probability $1-\alpha'$,

¹ The expression $\left[\sum_{i=1}^{m-1} (t_i)^{1/b} + (n-m+1)T_m^{1/b} \right]$ is considered a statistic even though it contains the parameter b since the value of b here is assumed known.

$$R(t_g) \geq \exp \left\{ - \frac{\chi_{2m}^2(1-\alpha')}{2 \left[(T_1/t_g)^{1/b} + (T_2/t_g)^{1/b} + \dots + (n-m+1)(T_m/t_g)^{1/b} \right]} \right\}, \quad (16)$$

where the right side of (16) is monotonically decreasing in b as long as

$$t_g < T_1^{1/b}/\Delta \cdot T_2^{1/b}/\Delta \cdot \dots \cdot T_m^{1/b}/\Delta \quad \text{with}$$

$$\Delta = T_1^{1/b} + T_2^{1/b} + \dots + (n-m+1)T_m^{1/b}, \text{ and certainly if } t_g \leq (T_1 \cdot T_2 \cdot \dots \cdot T_m)^{1/m}.$$

Thus, if $\bar{b} = \bar{b}_1(\alpha)$ (the boundary of the acceptance region of \bar{t}_1) is equal to $\log Z_m/LC_1(\alpha)$,

$$R(t_g) \geq \exp \left\{ - \frac{\chi_{2m}^2(1-\alpha)}{2 \left[(T_1/t_g)^{1/b} + (T_2/t_g)^{1/b} + \dots + (n-m+1)(T_m/t_g)^{1/b} \right]} \right\}^1$$

(for t_g sufficiently small) is true with probability at least $(1-\alpha)(1-\alpha')$.

INDUCED TESTS AND CONFIDENCE SETS BASED ON TWO OR THREE ORDER STATISTICS

Darroch and Silvey [11] show that the two statistics upon which an induced test is based need not be independent. As long as the tests are similar and of size α and α' , then the induced test will be similar and of size α'' with $\max(\alpha, \alpha') \leq \alpha'' \leq \alpha + \alpha'$. Moreover, even though $\hat{\xi}$ gives a uniformly most accurate confidence bound and uniformly most powerful tests for functions of $\xi = \delta^{1/b}$ when b is known, it does not necessarily follow that this situation holds when b is not known. We therefore consider the following one-order-statistic

¹ This inequality containing \bar{b} and the inequality $b \leq \bar{b}$ are jointly true with probability $(1-\alpha)(1-\alpha')$ exactly.

bound for ξ which allows for hand computation of test statistics and bounds for $R(t_g)$ with t_g specified and also for t_R , when alternatively a survival proportion R is specified. When b is known, a test ϕ_3 of $H': \xi \leq \xi_0 = \delta_0^{1/b}$ versus $K': \xi > \xi_0$ can be obtained from any one order statistic, say T_v , as shown in [12]¹. If one uses such a test, H' is rejected at level α' when

$$T_v^{1/b} > \xi_0 / B_v(\alpha'),$$

where $B_v(\alpha')$ is equal to $-\frac{1}{\log v_{\alpha'}(n-v+1, v)}$ and $v_{\alpha'}(n-v+1, v)$ is the $100\alpha'$ percent point of the beta distribution with $n-v+1$ and v degrees of freedom (see [13]). Then, since $R(t_g) = \exp [-(t_g/\delta)^{1/b}]$, $t_g > 0$, if t_g is specified, the hypothesis H' can be expressed as

$R(t_g) \leq R_{\delta_0, b}(t_g) = R_0$ and will be rejected when

$$(T_v/t_g)^{1/b} > [B_v(\alpha') \log(1/R_0)]^{-1} \quad (17)$$

Alternatively, if a survival proportion R is specified, H' may be expressed by $t_R \geq t_R^0 = \delta_0(\log(1/R))^b$ and rejected when

$$(B_v(\alpha') \log(1/R))^b > t_R^0 / T_v. \quad (18)$$

The left side of each of the two inequalities (17) and (18) is monotonically decreasing or increasing in b depending upon whether t_g is less than or greater than T_v or $B_v(\alpha') \log(1/R)$ is less than or greater than 1, respectively. Suppose $t_g < T_v$ or $B_v(\alpha') \log(1/R) < 1$ and H' is accepted

¹ In [12] T_v is actually the order statistic yielding smallest expected squared deviation of the bound, based on the acceptance region of ϕ_3 , from ξ .

at significance level α on the basis of Φ_3 and the assumption that b is equal to b_0 . Suppose also that the hypothesis $H: b \geq b_0$ has been accepted at level α on the basis of the test Φ_1 . Then the induced test of H^* (H and H' both true) has size and significance level α'' , and $\max(\alpha, \alpha') \leq \alpha'' < (\alpha + \alpha')$, as long as the test Φ_3 is similar and of size α' . As noted earlier, unbiasedness of a test with continuous power function and significance level α' implies that the test is similar and of size α' . Therefore, it is sufficient to demonstrate that Φ_3 is unbiased in order to guarantee that α'' , the size and the significance level of the induced test have the lower and upper limits $\max(\alpha, \alpha')$ and $\alpha + \alpha'$, respectively. This is shown in the following steps.

First, if X_v is the v^{th} order statistic of a size n sample from the Weibull distribution, then $(T_v)^{1/b}$ is equivalent to the v^{th} order statistic W_v of a size n sample from the negative exponential distribution with scale parameter ξ . Thus, the power function of the test Φ_3 is given by

$$\beta_{\Phi_3}(\xi) = \int_{\xi_0/B_v(\alpha')}^{\infty} \frac{n!}{(v-1)!(n-v)! \xi} e^{-(n-v+1) w_v/\xi} \left[1 - e^{-w_v/\xi} \right]^{v-1} dw_v$$

or

$$\beta_{\Phi_3}(\xi) = \frac{n!}{(v-1)!(n-v)!} \sum_{k=0}^{v-1} (-1)^k \binom{v-1}{k} \frac{e^{-(n-v+k+1) \xi_0/B_v(\alpha')}}{(n-v+k+1)}$$

Therefore,

$$\begin{aligned}\beta'_{\xi_3}(\xi) &= \frac{n!}{(v-1)!(n-v)!} \sum_{k=0}^{v-1} (-1)^k \binom{v-1}{k} \left[\xi_0 / \xi^2 B_v(\alpha') \right] e^{-[(n-v+k+1)\xi_0 / \xi B_v(\alpha')]} \\ &= \left[\xi_0 / (\xi B_v(\alpha')) \right] f(w_v) \Big|_{w_v = \xi_0 / B_v(\alpha')}\end{aligned}$$

Then, since ξ , ξ_0 , $B_v(\alpha')$, and $f(\xi_0/B_v(\alpha'))$ are each greater than zero, $\beta'_{\xi_3}(\xi)$ is positive for all ξ and the power function is monotonically increasing in ξ . (The power function of the dual test ξ_3 of K' versus H' can in like manner be shown to be monotonically decreasing in ξ .) Hence, both tests are unbiased, and the size and significance level of the induced test are equal to α'' .

A confidence bound for $R(t_g)$ or t_R can then be obtained from the boundary of the acceptance region of the test ξ_3 with

$$P\{R(t_g) \geq \exp[-(t_g/T_v)^{1/\bar{b}}/B_v(\alpha')]\} \geq 1-\alpha'', \quad t_g < T_v \quad (19)$$

or

$$P\{t_R \geq T_v [B_v(\alpha') \log(1/R)]^{\bar{b}}\} \geq 1-\alpha'', \quad B_v(\alpha') \log(1/R) < 1 \quad (20)$$

and $\bar{b} = \bar{b}_1(\alpha)$ the boundary of the acceptance region of ξ_1 at confidence level $1-\alpha$. Alternatively, then, one may write (19) as

$$\begin{aligned}P\left\{\log(\log(1/R(t_g))) \leq LC_1(\alpha) \frac{\log(t_g/T_v)}{\log(T_m/T_1)} - \log B_v(\alpha')\right\} &\geq 1-\alpha'', \\ t_g &< T_v,\end{aligned}$$

and (20) as

$$P\left\{\log t_R \geq \log \underline{t}_R = \log T_v + \left[\log(T_m/T_1)/LC_1(\alpha)\right] \left[\log(\log(1/R)) + \log B_v(\alpha')\right]\right\} \geq 1-\alpha. \quad (21)$$

for $\log(\log(1/R)) + \log B_v(\alpha') < 0$.

IMPROVEMENT OF DERIVED TESTS AND CONFIDENCE SETS

TESTS AND CONFIDENCE SETS CONCERNING b

Now, suppose one is no longer restricted to the use of the order statistics T_1 and T_m for obtaining tests and confidence sets for b , but instead considers any two order statistics as possible candidates upon which to base these tests and confidence sets. Suppose one uses as a criterion in choosing a confidence bound of the form $(\log T_q - \log T_p)/k_{p,q}$, smallest expected squared deviation of the bound from the parameter b (see Harter [14]). It can easily be shown that there exists a combination of n and m for which the combination of $\log T_1$ and $\log T_m$ does not provide the linear invariant two-order-statistic estimate of b that has smallest mean squared deviation from this parameter. Therefore, for each combination of n , m , and α considered, a coefficient, $LC_{p,q}(\alpha)$, yielding an upper bound $\bar{b}_{p,q}(\alpha) = (\log T_q - \log T_p)/LC_{p,q}(\alpha)$, $1 \leq p < q \leq m$ and the mean squared deviation of $\bar{b}_{p,q}(\alpha)$ from b have been calculated using

results obtained in [8]. The combination of p and q yielding the most efficient bound, that is, the one satisfying the specified criterion, is listed in Table B.I along with values of $LC = LC_{p,q}(\alpha)$ from which the bound may be obtained. Also in preparation is an additional table which will list, for selected values of α , the ratio of the mean squared errors of the best linear invariant estimators of b based on (1) all m available order statistics and (2) the combination of X_p and X_q yielding the most efficient bound.

Consider the power function $\beta_{\frac{1}{2}}(b)$ of the test $\frac{1}{2}_{p,q}$ of $H: b \geq b_0$ versus $K: b < b_0$ at significance level α which rejects the hypothesis when

$$(\log T_q - \log T_p)/b_0 \leq LC_{p,q}(\alpha).$$

Proceeding from (3) it can be shown that if $C_{p,q}(\alpha) = \exp(LC_{p,q}(\alpha))$, then $\beta_{\frac{1}{2}}(b)$ has the form

$$\beta_{\frac{1}{2}}(b) = E_b(\frac{1}{2}_{p,q}) = 1 - \frac{n!}{(p-1)!(q-p-1)!(n-q)!} \sum_{k=0}^{p-1} \sum_{j=0}^{q-p-1} (-1)^{k+j} \binom{p-1}{k} \binom{q-p-1}{j} \frac{1/(n-q+j+1)}{((q-p-j+k)+(n-q+j+1) (C_{p,q}(\alpha))^{b_0/b})}$$

Thus, as in the case in which $T_p = T_1$, $T_q = T_m$, and $C_{p,q}(\alpha) = C_1(\alpha)$, it follows that

$$\beta'_{\xi_{p,q}}(b) = -\frac{1}{b^2} \left(c_{p,q}(\alpha) \right)^{b_0/b} \log \left(c_{p,q}(\alpha) \right)^{b_0} f(s) \Big|_{s = \left(c_{p,q}(\alpha) \right)^{b_0/b}}$$

Then, as before, $c_{p,q}(\alpha)$ is greater than 1 (since p is less than q), and $\beta'_{\xi_{p,q}}(b)$ is negative. Therefore the power function is monotonically

decreasing in b . This insures that the test is unbiased and that an induced test of H^* ($H: b \geq b_0$ is true and $H': \xi \leq \xi_0$ is true) based on $\xi_{p,q}$ at significance level α and ξ_3 at significance level α' will be similar and of size α'' with $\max(\alpha, \alpha') \leq \alpha'' \leq \alpha + \alpha'$ as when

$\xi_{p,q} = \xi_{1,m} \equiv \xi_1$. The value of the power function $\beta_{\xi_{p,q}}(b)$ was calculated for b/b_0 equal to 0.25, 0.5 and 0.75 for each combination of p and q corresponding to each combination of n , m , and α so that the relative general sizes of the power functions of the tests for $b < b_0$ (related to the accuracy of the bound) could be compared with the relative sizes of the mean squared deviations of the bounds from the parameter.

It was found that the test based on the combination of p and q providing the most efficient bound for each combination of n , m , and α is not in general uniformly most powerful. That is, it is not always most powerful among tests based on two order statistics for all three of the values of b/b_0 calculated. In each case, however, the test corresponding to the most efficient bound appears to be if not uniformly most powerful, at least either locally most powerful or most powerful for b/b_0 close to zero. Furthermore, whenever a test

associated with a bound which is not the most efficient has higher power than that based on the most efficient combination of X_p and X_q for any value of b/b_0 calculated, the power functions of the two tests differ only slightly and the mean squared deviations of the two bounds are very nearly equal.

For example, the computed values of the power functions, for $\alpha = 0.05$, $n = m = 16$, and b/b_0 equal to 0.25, 0.50, and 0.75, are for the test based on the most efficient combination X_3 and X_{16} equal to 0.999997, 0.890903, and 0.296701, respectively, and for the test based on X_4 and X_{16} equal to 0.999999, 0.882135, and 0.283704, respectively. The expected squared deviations of the two corresponding bounds are 0.4289 and 0.4470, respectively.

TESTS AND CONFIDENCE SETS CONCERNING RELIABLE LIFE

It can also be shown that among lower bounds on x_R at confidence level $\geq 1 - \alpha'' \geq 1 - (\alpha + \alpha')$ of the form

$$\log T_v + \frac{\log \log (1/R) + B_v(\alpha')}{LC_{p,q}(\alpha)} (\log T_q - \log T_p), \quad 1 \leq p < q \leq m, \quad (22)$$

(as defined in (21)), the one with smallest expected squared deviation does not necessarily have $T_q = T_m$ and $T_p = T_1$ and $LC_{p,q}(\alpha) = LC_1(\alpha)$. Furthermore, an additional improvement can be made in the following

manner. Consider the identity,

$$X_v + \frac{\log \log (1/R) - Y_v}{Y_q - Y_p} (X_q - X_p) = u + b \log \log (1/R) = x_R, \quad (23)$$

$$1 \leq p < q \leq m,$$

where $Y_k = (X_k - u)/b$ and $X_k = \log T_k$ for any k . Hence, if

$$\frac{\log \log (1/R) - Y_v}{Y_q - Y_p} \geq \underline{V} \text{ with probability exactly equal to } 1 - \alpha^*, \text{ then}$$

$$P \left\{ X_q \geq X_v + \underline{V} (X_q - X_p) \right\} = 1 - \alpha^*.$$

Call $\frac{\log \log (1/R) + B_v(\alpha')}{LC_1(\alpha)}$ in (21), \underline{W} , and call the bound defined by

$$(22), \underline{x}_R(W). \text{ From (22) and (23) } \frac{\log \log (1/R) - Y_v}{Y_q - Y_p} \geq \underline{W} \text{ with proba-}$$

bility greater than or equal to $1 - (\alpha + \alpha')$. Thus, if $1 - \alpha^*$ is equal to $1 - (\alpha + \alpha')$, \underline{W} is less than or equal to \underline{V} and $X_v + \underline{W} (X_q - X_p)$ is less than or equal to $X_v + \underline{V} (X_q - X_p)$. It follows that for any value $x'_R < x_R$ the probability that $X_v + \underline{V} (X_q - X_p)$ is less than x'_R is smaller than or equal to the probability that $X_v + \underline{W} (X_q - X_p)$ is less than x'_R . The more accurate bound is therefore given by

$$\underline{x}_R(V) = X_v + \underline{V} (X_q - X_p).$$

Moreover, since the test associated with the bound $\underline{x}_R(W)$ is of size $\leq (\alpha + \alpha') = \alpha^*$, the test associated with the bound $\underline{x}_R(V)$ is also of

size $\leq \alpha^*$, hence of size α^* since α^* is the significance level.

Since it is not possible by calculation and examination of the power function to demonstrate that the test associated with the bound $x_R(V)$ is unbiased, this is of interest.

It was originally planned that the combination of p , q , and v yielding a most efficient bound for x_R would be determined for each combination of n , m , R , and α considered. Doing this, however, would require iterative calculations of 20,615 percentage points of the distribution of V from the expression (or an expression similar to that given) on page 77 for each combination of α and R , if only sample sizes 2, 3, ..., 20 were considered. Since several seconds, at least, appear to be required to perform the numerical integrations involved in calculating each percentage point, it has been decided to cut down on the number of necessary calculations by choosing the three order statistics on which to base the bounds before any values of V are computed. For each combination of sample size n , censoring number m , and specified survival proportion R , the estimator of x_R with smallest risk among those of the form $X_v + C(X_q - X_p)$, $1 \leq v \leq m$, $1 \leq p < q \leq m$, will be selected. The three order statistics specified by this estimation rule will then provide the basis for bounds at all confidence levels for each corresponding combination of n , m , and R . Indications are that very little increase in risk for the bounds will result from this procedure; and the number of percentage points to be calculated for each combination of α and R will be reduced to 171.

OBTAINING BOUNDS ON RELIABILITY FOR SPECIFIED REQUIRED LIFE

Suppose that required life t_g rather than a survival proportion R is specified. Then it will often be possible to use the values of \underline{V} which will be tabulated to obtain an upper confidence bound on $R(t_g)$, the proportion surviving at time $t_g = \exp(x_g)$.

The bounds on x_R or t_R , referred to immediately above, depend on the identity

$$x_R = u + b \log \log (1/R) \approx x_v + \frac{\log \log (1/R) - Y_v}{Y_q - Y_p} (x_q - x_p). \quad (24)$$

This can also be written in the form:

$$\log \log (1/R(t_g)) \approx \frac{x_v - u}{b} + \frac{x_g - x_v}{x_q - x_p} \frac{x_q - x_p}{b}$$

by subtracting u from both sides of the identity in (24), dividing by b , and replacing R by $R(t_g)$. Let x_g or t_g be specified so that $\frac{x_g - x_v}{x_q - x_p}$ can be calculated. Then a lower confidence bound on $R(t_g)$ is

given by the value of R corresponding to the \underline{V} which is equal to

$\frac{x_g - x_v}{x_q - x_p}$ and which represents a bound at the appropriate level on

$$V = \frac{\log \log (1/R) - Y_v}{Y_q - Y_p} = \frac{x_R - x_v}{x_q - x_p} \text{ when } R \text{ is specified. It will often}$$

be the case, of course, that the required value of \underline{V} is not available in the table, in which case a larger value can be used to provide a conservative bound on $R(t_g)$.

EXTENSION OF RESULTS

EXTENSION TO OTHER TWO-PARAMETER DISTRIBUTIONS

A natural extension of the results given above is the application of the methods used in obtaining confidence bounds to various other distributions. The fact that bounds based on three order statistics can be found for a percentage point x_R of the distribution of X (the extreme-value distribution of smallest values) depends, as noted above, upon the identity

$$x_v + \frac{y_R - y_v}{y_q - y_p} (x_q - x_p) \equiv x_R = u + b \log \log (1/R), \quad 1 \leq p < q \leq m \leq n \quad (25)$$

$$1 < v < m < n,$$

where $Y_k = (X_k - u)/b$ and $y_R = \log \log (1/R)$, with R a specified proportion of the population to the right of the point x_R . For the extreme-value distribution, R may represent a proportion of the population surviving at time x_R . The value of $y_R = -\log \log (1/R)$ has been tabulated in [15] for the extreme value distribution of largest values, but can also be calculated relatively easily. For other distributions, values of y_R can often also be calculated or have been tabulated. For any distribution which can be transformed to one having a location-scale parameter, that is, with density of the form

$$f_{\theta_1, \theta_2}(x) = \frac{1}{\theta_2} g\left(\frac{x - \theta_1}{\theta_2}\right), \quad \text{for some } g, \text{ the identity (25) holds. Three-}$$

order-statistic bounds can therefore be obtained on x_R for such a distribution if values of y_R are obtainable and if percentiles of $(y_R - Y_q)/(Y_q - Y_p)$ can be calculated. If the first and second moments of the distribution of the order statistics of the distribution are available as well, a most efficient one of these bounds can be found for various combinations of n , m , R and confidence level $1 - \alpha$. This method of obtaining bounds may be useful when samples from distributions for which classical bounds are available have been censored so that classical theory does not apply.

EXTENSION TO THREE-PARAMETER DISTRIBUTIONS

A further extension of the above results is to a random variable $T - \lambda$, with X equal to the natural logarithm of $T - \lambda$, and the distribution of X dependent upon a location-scale parameter $\theta = (\theta_1, \theta_2)$. These include the three-parameter log normal, the three-parameter Pareto and the three-parameter Weibull distributions. The latter distribution is applicable to the situation in which a threshold λ exists such that no failures can occur prior to the time λ . There is a proof given in Kaufman and Lipow [16] concerning confidence bounds on $t_R = \exp(x_R)$, which they have obtained as a function of order statistics T_1 and T_n from any distribution of the type described above. The following is a generalization of that proof.

Consider a specified proportion $R = 1 - F(y_R)$

$= 1 - F\left(\frac{\log(t_R - \lambda) - \theta_1}{\theta_2}\right)$ of a population and a lower confidence

bound \underline{t}_R which can be obtained on a percentage point t_R corresponding

to $1 - R$ when λ is zero. Let \underline{t}_R be of the form $\exp(x_R) = T_v(T_q/T_p)^{1/v}$,

$1 \leq p < q \leq m \leq n$, $1 \leq v \leq m < n$. Then $\underline{t}_R(\lambda) = \lambda + (T_v - \lambda) \left[(T_q - \lambda) / (T_p - \lambda) \right]^{1/v}$

gives a suitable bound for $t_R(\lambda) = \lambda + \exp(\theta_1 + \theta_2 y_R)$ when λ is known.

It will be shown that \underline{t}_R gives a conservative lower bound for $t_R(\lambda)$ as long as certain conditions are satisfied.

THEOREM I

If

$$P \left\{ t_R(\lambda) = \lambda + \exp(\theta_1 + \theta_2 y_R) \geq \underline{t}_R(\lambda) = \lambda + (T_v - \lambda) \left[(T_q - \lambda) / (T_p - \lambda) \right]^{1/v} \right\} = 1 - \alpha,$$

then $P \left\{ t_R(\lambda) \geq \underline{t}_R = \exp(x_R) \right\} \geq 1 - \alpha$, for \underline{v}

satisfying certain requirements dependent upon the relationship of T_v to T_p and T_q .

It is sufficient to demonstrate that $\underline{t}_R \leq \underline{t}_R(\lambda)$ or that $\underline{t}_R(\lambda)$ is non-decreasing in λ . Consider

$$\underline{t}_R(\lambda) = \lambda + (T_v - \lambda) \left[(T_q - \lambda) / (T_p - \lambda) \right]^{1/v}$$

The derivative of this expression with respect to λ is given by

$$\begin{aligned}
\frac{d t_R(\lambda)}{d \lambda} &= 1 - \underline{v} \left[(T_q - \lambda)(T_p - \lambda)^{V-1} \right] \left[(T_v - \lambda)/(T_p - \lambda) \right] \\
&\quad - \left[(T_q - \lambda)/(T_p - \lambda) \right]^V + \underline{v} \left[(T_v - \lambda)/(T_p - \lambda) \right] \left[(T_q - \lambda)/(T_p - \lambda) \right]^V \quad (26) \\
&= 1 - \left[(T_q - \lambda)/(T_p - \lambda) \right]^V - \underline{v} \left[(T_v - \lambda)/(T_p - \lambda) \right] \left\{ \left[(T_q - \lambda)/(T_p - \lambda) \right]^{V-1} \right. \\
&\quad \left. - \left[(T_q - \lambda)/(T_p - \lambda) \right]^V \right\}
\end{aligned}$$

Now let $\eta = (T_q - \lambda)/(T_p - \lambda)$, which is greater than or equal to 1 since $\lambda \leq T_1 \leq T_p \leq T_q$. Then (26) can be written

$$1 - \eta^V - \underline{v} \left[(T_v - \lambda)/(T_p - \lambda) \right] \eta^{V-1} (1 - \eta)$$

and it is required to demonstrate that this expression is non-negative or that

$$1 \geq \eta^V + \underline{v} \left[(T_v - \lambda)/(T_p - \lambda) \right] \eta^{V-1} (1 - \eta). \quad (27)$$

Assume $T_p \leq T_v \leq T_q$. Then if $\underline{v} \leq 0$, $\underline{v} \eta^{V-1} (1 - \eta) \geq 0$ and the right side of (27) has its highest (or worst) value when T_v is equal to T_q . T_q is therefore substituted for T_v in (27), which becomes

$$1 \geq \eta^V + \underline{v} \eta^V (1 - \eta) \quad (28)$$

Then for $\underline{v} \leq 0$ the right side of (28) is equal to 1 and 0, respectively, for η equal to 1 and ∞ , respectively. Furthermore the right side of (28) is monotonically non-increasing in η for $\eta \geq 1$,

if and only if $\underline{v} \leq -1$ for $\underline{v} \leq 0$. Thus, the inequality (26) is satisfied, $t_R(\lambda)$ is non-decreasing in λ , and t_R is a conservative lower bound for t_R , for $T_p \leq T_v \leq T_q$ as long as a negative \underline{v} is less than or equal to -1. If \underline{v} is positive, then T_p gives the worst value for T_v and $1 + \frac{\underline{v}}{\eta} + \underline{v} \frac{\underline{v}-1}{\eta} (1-\eta)$ is equal to 1 for $\eta = 1$ and $-\infty$ for $\eta = \infty$ and is monotonically non-increasing in η for $\eta \geq 1$ if and only if $\underline{v} \geq 1$. For $T_v \leq T_p$ and for $T_v \geq T_q$ it can be shown by the method used above that t_R is a conservative lower bound for t_R if $\underline{v} \leq 0$ and if $\underline{v} \geq 0$, respectively.

CALCULATION OF THE COEFFICIENTS YIELDING THE EXACT BOUNDS AND USE OF THE TABLES

To obtain the coefficient of an exact upper confidence bound for b at level $1 - \alpha$ based on X_q and X_p one may proceed from (3) as in obtaining the power function. The coefficient $LC_{p,q}(\alpha)$ defining the bound is thus given by iteratively solving the equation

$$1 - \frac{n!}{(p-1)!(q-p-1)!(n-q)!} \sum_{k=0}^{p-1} \sum_{j=0}^{q-p-1} (-1)^{k+1} \binom{p-1}{k} \binom{q-p-1}{j} \frac{1/(n-q+j+1)}{((q-p-j+k)+(n-q+j+1)) C_{p,q}(\alpha)} = \alpha, \quad (29)$$

where $C_{p,q}(\alpha) = \exp(LC_{p,q}(\alpha))$.

The coefficient defining an exact upper bound for x_R at confidence level $1 - \alpha^*$, as described above, is the $100\alpha^*$ percent point of the

distribution of $V = \frac{\log \log (1/R) - X_v}{X_q - X_p}$. The expression from which

the distribution percentiles of V may be obtained differs accordingly as $v < p$, $v = p$, $p < v < q$, $v = q$, or $v > q$. For example, if $p < v < q$, the solution to

$$\int_1^{\infty} \frac{n!}{(p-1)!(v-p-1)!(q-v-1)!(n-q)!} \sum_{k=0}^{p-1} \sum_{j=0}^{v-p-1} \sum_{m=0}^{q-v-1} (-1)^{j+k+m} \binom{p-1}{k} \binom{v-p-1}{j} \binom{q-v-1}{m} \\ \left\{ -cs \exp \left\{ -c (n-p+k+1)s \right\} / (n-q+m+1)(n-v+m-j+k+1)s \right. \\ \left. + cs \exp \left\{ -c \left[(q-p-m+k)s + (n-q+m+1)s^{1-1/v} \right] \right\} / (n-q+m+1) \left[(q-v-j+k)s \right. \right. \\ \left. \left. + (n-q+m+1)s^{1-1/v} \right] \right. \\ \left. + cs \exp \left\{ -c \left[(n+v-q-p+j+1)s + (q-v-j+k)s^{1+1/v} \right] \right\} / (q-v-j+k) \left[(q-v-j+k)s^{1+1/v} \right. \right. \\ \left. \left. + (n-q+m+1)s \right] \right. \\ \left. - cs \exp \left\{ c (n+v-p+k+1)s \right\} / (q-v-j+k)(n-v+m-j+k+1)s \right\} ds = \alpha,$$

where $c = \log(1/R)$, defines the appropriate $v = \underline{v}$ when \underline{v} is negative or zero. For $0 < \underline{v} < \infty$, the limits of integration for s are 0 to 1, and $1 - \alpha$ rather than α appears on the right side of the equation. The equations to be solved for \underline{v} under other restrictions on v are slightly less complicated.

The values of $LC_{p,q}(\alpha) = LC_1(\alpha)$ for $X_p = X_1$ were calculated iteratively by means of both equation (29) and equation (9) so that any loss of accuracy with increasing number of terms of (29) could be determined. The calculations were made in Fortran IV built-in double precision (16 significant figures), and the values of $\exp[LC_1(\alpha)]$ calculated agreed to at least seven significant figures no matter how large the number of terms involved, through n equal to 20. An additional external check is given by the values of percentiles of

$$\frac{T_p^{1/b}}{T_q^{1/b} - T_p^{1/b}} = \left[\left(T_q/T_p \right)^{1/b} - 1 \right]^{-1} \quad \text{for } 2 \leq n \leq 10, 1 \leq p < q \leq n, \text{ ex-}$$

hibited in Table I of [17]. The values of LC given in Table B.I of this report are thus accurate to within a unit in the final decimal place shown.

Characteristic of the values of ratios of mean squared errors of best linear invariant estimators of b (based on all m order statistics and on the combination of X_p and X_q yielding a most efficient bound) is 0.793 for $n = m = 17$. For the same values of n and m , the corresponding ratio associated with the v , p , and q yielding a best invariant estimator of $x_{.90}$ of the form $X_v + C(X_q - X_p)$ is 0.877. The additional information contained in the v^{th} order statistic appears to contribute considerably to the efficiency of estimators and bounds.

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TABLE B.I - VALUES OF P, Q, AND LC FOR OBTAINING MOST EFFICIENT EXACT CONFIDENCE
 FORMS OF THE FORM $(\log T_Q - \log T_P) / LC$, FOR THE WEIBULL SHAPE PARAMETER,
 BASED ON ANY TWO OF THE FIRST M OF N WEIBULL ORDER STATISTICS, $T_1 \leq T_2 \leq \dots \leq T_M \leq \dots \leq T_N$

		CONFIDENCE LEVEL								
		0.99			0.95			0.90		
N	M	P	Q	LC	P	Q	LC	P	Q	LC
2	2	1	2	0.020	1	2	0.100	1	2	0.201
3	2	1	2	0.015	1	2	0.076	1	2	0.154
	3	1	3	0.213	1	3	0.482	1	3	0.693
4	2	1	2	0.013	1	2	0.068	1	2	0.130
	3	1	3	0.167	1	3	0.387	1	3	0.565
	4	1	4	0.481	1	4	0.847	1	4	1.099
5	2	1	2	0.013	1	2	0.064	1	2	0.130
	3	1	3	0.149	1	3	0.348	1	3	0.513
	4	1	4	0.392	1	4	0.706	1	4	0.928
	5	1	5	0.737	1	5	1.151	1	5	1.419
6	2	1	2	0.012	1	2	0.061	1	2	0.125
	3	1	3	0.139	1	3	0.327	1	3	0.483
	4	1	4	0.353	1	4	0.642	1	4	0.851
	5	1	5	0.617	1	5	0.983	1	5	1.226
	6	1	6	0.964	1	6	1.403	1	6	1.680
7	2	1	2	0.012	1	2	0.060	1	2	0.122
	3	1	3	0.133	1	3	0.314	1	3	0.465
	4	1	4	0.330	1	4	0.605	1	4	0.805
	5	1	5	0.560	1	5	0.902	1	5	1.133
	6	1	6	0.824	1	6	1.219	1	6	1.474
	7	1	7	1.164	1	7	1.618	2	7	1.284
8	2	1	2	0.011	1	2	0.058	1	2	0.120
	3	1	3	0.129	1	3	0.304	1	3	0.452
	4	1	4	0.315	1	4	0.581	1	4	0.775
	5	1	5	0.526	1	5	0.853	1	5	1.076
	6	1	6	0.754	1	6	1.127	1	6	1.371
	7	1	7	1.010	1	7	1.424	2	7	1.101
	8	1	8	1.340	2	8	1.263	2	8	1.479
9	2	1	2	0.011	1	2	0.056	1	2	0.118
	3	1	3	0.125	1	3	0.298	1	3	0.443
	4	1	4	0.305	1	4	0.564	1	4	0.754
	5	1	5	0.503	1	5	0.820	1	5	1.037
	6	1	6	0.710	1	6	1.069	1	6	1.306
	7	1	7	0.930	1	7	1.323	2	7	1.008
	8	1	8	1.177	2	8	1.091	2	8	1.286
	9	2	9	1.067	2	9	1.430	2	9	1.649
10	2	1	2	0.011	1	2	0.057	1	2	0.116
	3	1	3	0.123	1	3	0.292	1	3	0.435
	4	1	4	0.297	1	4	0.551	1	4	0.738
	5	1	5	0.486	1	5	0.796	1	5	1.009
	6	1	6	0.680	1	6	1.029	1	6	1.261
	7	1	7	0.878	1	7	1.259	2	7	0.950
	8	1	8	1.089	2	8	1.002	2	8	1.186
	9	2	9	0.923	2	9	1.250	2	9	1.450
	10	2	10	1.209	2	10	1.579	2	10	1.801
11	2	1	2	0.011	1	2	0.056	1	2	0.115
	3	1	3	0.121	1	3	0.288	1	3	0.429
	4	1	4	0.291	1	4	0.541	1	4	0.725
	5	1	5	0.473	1	5	0.778	1	5	0.988
	6	1	6	0.658	1	6	1.000	1	6	1.228
	7	1	7	0.843	1	7	1.214	2	7	0.910
	8	1	8	1.032	2	8	0.944	2	8	1.127
	9	2	9	0.846	2	9	1.154	2	9	1.345
	10	2	10	1.057	2	10	1.394	2	10	1.598
	11	2	11	1.338	2	11	1.713	2	11	1.936
12	2	1	2	0.011	1	2	0.056	1	2	0.114
	3	1	3	0.120	1	3	0.285	1	3	0.425
	4	1	4	0.286	1	4	0.532	1	4	0.715
	5	1	5	0.463	1	5	0.763	1	5	0.971
	6	1	6	0.641	1	6	0.977	1	6	1.202
	7	1	7	0.816	1	7	1.180	2	7	0.880
	8	1	8	0.992	2	8	0.904	2	8	1.077
	9	2	9	0.796	2	9	1.092	2	9	1.276
	10	2	10	0.974	2	10	1.293	2	10	1.488
	11	2	11	1.181	2	11	1.524	2	11	1.710
	12	2	12	1.457	2	12	1.835	2	12	2.059

TABLE B.I - CONTINUED

CONFIDENCE LEVEL									
0.99					0.95			0.90	
N	M	P	Q	LC	P	Q	LC	P	Q
13	2	1	2	0.011	1	2	0.055	1	2
	3	1	3	0.118	1	3	0.282	1	3
	4	1	4	0.282	1	4	0.526	1	4
	5	1	5	0.455	1	5	0.751	1	5
	6	1	6	0.627	1	6	0.959	1	6
	7	1	7	0.795	1	7	1.154	2	7
	8	1	8	0.961	2	8	0.874	2	8
	9	2	9	0.760	2	9	1.047	2	9
	10	2	10	0.919	2	10	1.227	2	10
	11	2	11	1.093	2	11	1.420	2	11
	12	2	12	1.295	2	12	1.643	3	12
	13	2	13	1.566	2	13	1.947	3	13
14	2	1	2	0.011	1	2	0.055	1	2
	3	1	3	0.117	1	3	0.280	1	3
	4	1	4	0.279	1	4	0.520	1	4
	5	1	5	0.449	1	5	0.742	1	5
	6	1	6	0.616	1	6	0.944	1	6
	7	1	7	0.778	1	7	1.133	2	7
	8	1	8	0.937	2	8	0.850	2	8
	9	2	9	0.733	2	9	1.014	2	9
	10	2	10	0.880	2	10	1.179	2	10
	11	2	11	1.034	2	11	1.350	2	11
	12	2	12	1.203	2	12	1.536	3	12
	13	2	13	1.401	3	13	1.427	3	13
	14	2	14	1.667	3	14	1.713	3	14
15	2	1	2	0.011	1	2	0.055	1	2
	3	1	3	0.116	1	3	0.278	1	3
	4	1	4	0.276	1	4	0.516	1	4
	5	1	5	0.443	1	5	0.734	1	5
	6	1	6	0.607	1	6	0.932	1	6
	7	1	7	0.765	1	7	1.116	2	7
	8	1	8	0.918	2	8	0.831	2	8
	9	2	9	0.712	2	9	0.987	2	9
	10	2	10	0.849	2	10	1.142	2	10
	11	2	11	0.991	2	11	1.300	2	11
	12	2	12	1.142	2	12	1.464	3	12
	13	2	13	1.306	3	13	1.326	3	13
	14	2	14	1.499	3	14	1.530	3	14
	15	3	15	1.476	3	15	1.811	3	15
16	2	1	2	0.011	1	2	0.055	1	2
	3	1	3	0.116	1	3	0.276	1	3
	4	1	4	0.273	1	4	0.512	1	4
	5	1	5	0.439	1	5	0.727	1	5
	6	1	6	0.599	1	6	0.922	1	6
	7	1	7	0.753	1	7	1.101	2	7
	8	1	8	0.902	2	8	0.816	2	8
	9	2	9	0.695	2	9	0.966	2	9
	10	2	10	0.825	2	10	1.113	2	10
	11	2	11	0.959	2	11	1.260	2	11
	12	2	12	1.096	2	12	1.411	3	12
	13	2	13	1.242	3	13	1.258	3	13
	14	2	14	1.403	3	14	1.427	3	14
	15	3	15	1.319	3	15	1.626	3	15
	16	3	16	1.565	3	16	1.901	3	16
17	2	1	2	0.011	1	2	0.054	1	2
	3	1	3	0.115	1	3	0.275	1	3
	4	1	4	0.271	1	4	0.508	1	4
	5	1	5	0.435	1	5	0.721	1	5
	6	1	6	0.593	1	6	0.913	1	6
	7	1	7	0.744	1	7	1.089	2	7
	8	1	8	0.888	2	8	0.803	2	8
	9	2	9	0.680	2	9	0.948	2	9
	10	2	10	0.806	2	10	1.089	2	10
	11	2	11	0.932	2	11	1.229	2	11
	12	2	12	1.061	2	12	1.370	3	12
	13	2	13	1.194	3	13	1.207	3	13
	14	2	14	1.336	3	14	1.356	3	14
	15	3	15	1.228	3	15	1.521	3	15
	16	3	16	1.406	3	16	1.716	3	16
	17	3	17	1.649	3	17	1.986	3	17

TABLE B.I - CONTINUED

		CONFIDENCE LEVEL								
		0.99			0.95			0.90		
N	M	P	Q	LC	P	Q	LC	P	Q	LC
18	2	1	2	0.011	1	2	0.054	1	2	0.111
	3	1	3	0.114	1	3	0.273	1	3	0.409
	4	1	4	0.270	1	4	0.505	1	4	0.681
	5	1	5	0.431	1	5	0.716	1	5	0.916
	6	1	6	0.587	1	6	0.905	1	6	1.121
	7	1	7	0.735	1	7	1.078	2	7	0.792
	8	1	8	0.877	2	8	0.792	2	8	0.951
	9	2	9	0.669	2	9	0.933	2	9	1.101
	10	2	10	0.790	2	10	1.070	2	10	1.244
	11	2	11	0.911	2	11	1.204	2	11	1.384
	12	2	12	1.033	2	12	1.337	3	12	1.189
	13	2	13	1.157	3	13	1.168	3	13	1.325
	14	2	14	1.286	3	14	1.304	3	14	1.466
	15	3	15	1.165	3	15	1.448	3	15	1.616
	16	3	16	1.313	3	16	1.609	3	16	1.783
	17	3	17	1.488	3	17	1.800	3	17	1.981
	18	3	18	1.727	3	18	2.066	3	18	2.261
19	2	1	2	0.011	1	2	0.054	1	2	0.111
	3	1	3	0.114	1	3	0.272	1	3	0.407
	4	1	4	0.268	1	4	0.503	1	4	0.678
	5	1	5	0.428	1	5	0.711	1	5	0.910
	6	1	6	0.582	1	6	0.899	1	6	1.113
	7	1	7	0.728	1	7	1.069	2	7	0.784
	8	1	8	0.867	2	8	0.782	2	8	0.940
	9	2	9	0.658	2	9	0.920	2	9	1.086
	10	2	10	0.776	2	10	1.053	2	10	1.276
	11	2	11	0.893	2	11	1.182	2	11	1.361
	12	2	12	1.009	2	12	1.310	3	12	1.162
	13	2	13	1.127	3	13	1.137	3	13	1.291
	14	2	14	1.247	3	14	1.263	3	14	1.423
	15	3	15	1.118	3	15	1.394	3	15	1.559
	16	3	16	1.248	3	16	1.535	3	16	1.704
	17	3	17	1.393	3	17	1.691	4	17	1.608
	18	3	18	1.565	3	18	1.878	4	18	1.799
	19	3	19	1.802	3	19	2.141	4	19	2.069
20	2	1	2	0.011	1	2	0.054	1	2	0.111
	3	1	3	0.113	1	3	0.271	1	3	0.406
	4	1	4	0.267	1	4	0.500	1	4	0.675
	5	1	5	0.425	1	5	0.707	1	5	0.905
	6	1	6	0.578	1	6	0.893	1	6	1.106
	7	1	7	0.722	1	7	1.061	2	7	0.777
	8	1	8	0.858	2	8	0.774	2	8	0.931
	9	2	9	0.650	2	9	0.909	2	9	1.074
	10	2	10	0.765	2	10	1.039	2	10	1.211
	11	2	11	0.878	2	11	1.164	2	11	1.342
	12	2	12	0.990	2	12	1.287	3	12	1.140
	13	2	13	1.102	3	13	1.111	3	13	1.264
	14	2	14	1.216	3	14	1.230	3	14	1.387
	15	3	15	1.081	3	15	1.352	3	15	1.514
	16	3	16	1.199	3	16	1.480	3	16	1.646
	17	3	17	1.327	3	17	1.616	4	17	1.532
	18	3	18	1.469	4	18	1.532	4	18	1.688
	19	3	19	1.638	4	19	1.712	4	19	1.875
	20	3	20	1.872	4	20	1.964	4	20	2.141

TABLE B.I - CONTINUED

CONFIDENCE LEVEL										
0.99					0.95			0.90		
N	M	P	Q	LC	P	Q	LC	P	Q	LC
21	2	1	2	0.011	1	2	0.054	1	2	0.110
	3	1	3	0.113	1	3	0.270	1	3	0.404
	4	1	4	0.265	1	4	0.498	1	4	0.672
	5	1	5	0.423	1	5	0.704	1	5	0.901
	6	1	6	0.574	1	6	0.887	1	6	1.100
	7	1	7	0.716	1	7	1.053	2	7	0.771
	8	1	8	0.851	2	8	0.767	2	8	0.922
	9	2	9	0.642	2	9	0.899	2	9	1.063
	10	2	10	0.754	2	10	1.025	2	10	1.197
	11	2	11	0.863	2	11	1.148	2	11	1.325
	12	2	12	0.973	2	12	1.267	3	12	1.122
	13	2	13	1.081	3	13	1.090	3	13	1.240
	14	2	14	1.190	3	14	1.203	3	14	1.358
	15	3	15	1.051	3	15	1.318	3	15	1.477
	16	3	16	1.161	3	16	1.436	3	16	1.599
	17	3	17	1.277	3	17	1.560	4	17	1.475
	18	3	18	1.401	4	18	1.459	4	18	1.611
	19	3	19	1.541	4	19	1.606	4	19	1.763
	20	3	20	1.708	4	20	1.783	4	20	1.947
	21	3	21	1.939	4	21	2.032	4	21	2.210
22	2	1	2	0.011	1	2	0.054	1	2	0.110
	3	1	3	0.113	1	3	0.269	1	3	0.403
	4	1	4	0.264	1	4	0.496	1	4	0.670
	5	1	5	0.421	1	5	0.700	1	5	0.897
	6	1	6	0.570	1	6	0.883	1	6	1.095
	7	1	7	0.711	1	7	1.047	2	7	0.766
	8	1	8	0.844	2	8	0.760	2	8	0.915
	9	2	9	0.635	2	9	0.891	2	9	1.054
	10	2	10	0.746	2	10	1.015	2	10	1.185
	11	2	11	0.853	2	11	1.135	2	11	1.310
	12	2	12	0.959	2	12	1.251	3	12	1.106
	13	2	13	1.063	3	13	1.071	3	13	1.220
	14	2	14	1.168	3	14	1.180	3	14	1.333
	15	3	15	1.027	3	15	1.289	3	15	1.447
	16	3	16	1.130	3	16	1.401	3	16	1.562
	17	3	17	1.237	3	17	1.515	4	17	1.430
	18	3	18	1.350	4	18	1.405	4	18	1.553
	19	3	19	1.472	4	19	1.533	4	19	1.655
	20	4	20	1.405	4	20	1.677	4	20	1.835
	21	4	21	1.565	4	21	1.851	4	21	2.016
	22	4	22	1.767	4	22	2.097	4	22	2.274

APPENDIX C

TABLES FOR OBTAINING THE BEST LINEAR INVARIANT ESTIMATES OF PARAMETERS OF THE WEIBULL DISTRIBUTION

SUMMARY

A censored life-test situation is considered and the assumption of a Weibull distribution for failure times is made. Tables are given for estimating log reliable life, where the estimator is best among linear estimators with expected loss invariant under translations. These best linear invariant (BLI) estimators have uniformly smaller expected loss than the Gauss-Markov best linear unbiased (BLU) estimators and are simple linear functions of the BLU estimators. The preliminary discussion involves a comparison of the BLI estimators with other widely used estimators. Solutions to the problem of obtaining confidence bounds are also discussed.

INTRODUCTION

Assume a random sample of n items is subjected to life test until $m \leq n$ failures occur. Assume further that the failure times associated with the n items are from a population of random variables identically distributed according to a two-parameter Weibull law. Let the random variable T represent failure time in this population. Then

$$\Pr[T \leq t] = F_{\delta, b}(t) = 1 - \exp\{-(t/\delta)^{1/b}\} \quad ,$$

for $t \geq 0$, and $F_{\delta, b}(t) = 0$ otherwise. Both parameters δ and b are positive. The logarithms of the failure times have the extreme-value distribution of smallest values. If $X = \log T$ and $u = \log \delta$, then

$$\Pr[X \leq x] = F_{u, b}(x) = 1 - \exp\{-\exp[(x-u)/b]\} \quad .$$

The parameter b is the scale parameter of the distribution of X ; the variance of X is $\frac{\pi^2 b^2}{6}$. The parameter u is a location parameter, the mode of the probability density function associated with the distribution of X .

The reliability function, which gives the proportion of the population surviving at log time x , is given by $R(x) = 1 - F(x)$, or

$$R_{u, b}(x) = \exp\{-\exp[(x-u)/b]\} \quad . \quad (1)$$

Suppose that a value R is specified for $R_{u,b}(x)$ and that the problem of interest is the estimation of the value of x , call it x_R , corresponding to the specified R on the basis of a censored sample. The value x_R is simply the log time at which 100R% of the population will have survived, and is often referred to as log reliable life. Since, from (1), $R = \exp\{-\exp[(x_R - u)/b]\}$, or $x_R = u + b \log \log(1/R)$, x_R is a parametric function of the location parameter u and the scale parameter b . In this report methods for estimating the general parametric function $\varphi = k_1 u + k_2 b$ (which includes u , b , and x_R) are considered.

MAXIMUM-LIKELIHOOD ESTIMATION

Because of the regularity properties of the Weibull density function (see Kimball [1]), maximum-likelihood estimators of Weibull parameters enjoy the properties of consistency, asymptotic efficiency, asymptotic unbiasedness and asymptotic normality. The maximum-likelihood estimates cannot, however, be calculated explicitly, but must be determined by iterative procedures applied to sample data. Since this is so, the expected squared error of a Weibull maximum-likelihood estimator cannot be determined except for large samples, for which the variances of these asymptotically unbiased estimators are given by the Cramér-Rao bounds for regular unbiased estimators. Thus, for small sample sizes, the expected loss of the estimator cannot be compared with that of other estimators whose exact mean squared error can be calculated. Furthermore, in [2] it is shown that when no censoring occurs, the n order statistics, $\{\log T_{(1,n)} \leq \log T_{(2,n)} \leq \dots \leq \log T_{(n,n)}\} = \{X_{(1,n)} \leq X_{(2,n)} \leq \dots \leq X_{(n,n)}\}$ from a size n sample are minimally sufficient for (u,b) . They are, therefore, minimally sufficient for (δ,b) or for any couple consisting of nonsingular functions of δ and b . In [3] this result is extended to show that in the case in which $\frac{n-m}{n}$ of a size n ordered sample is censored from above, the first m order statistics, $X_{(1,n)} \leq X_{(2,n)} \leq \dots \leq X_{(m,n)}$ are minimally sufficient so that for $m > 2$, the number of minimally sufficient statistics

exceeds the number of parameters to be estimated. Hence, there is no guarantee that when m is greater than 2 the maximum-likelihood estimators of Weibull parameters are the minimum-variance estimators of their expected values, as would be the case if the number of sufficient statistics equaled the number of parameters to be estimated (see Rao [4]). One cannot, therefore, claim the usual optimality properties for the maximum-likelihood estimators of the Weibull (or extreme-value) parameters when m is greater than two, but n is not large enough for asymptotic theory to apply. Moreover, it is not known when, for a given $p = m/n$, n is sufficiently large.

LINEAR ESTIMATION

For estimating the general parametric function $\varphi = l_1 u + l_2 b$, the generalized Gauss-Markov Theorem (see Lloyd [5]) specifies the least-squares estimator as the unique best one among unbiased linear functions of $X_{(1,n)}$, $X_{(2,n)}$, ..., and $X_{(m,n)}$ for all m and n . Weibull estimates obtained graphically from probability plots are simply approximations to the least-squares estimate, with the major source of error being the necessarily subjective visual fitting of the least-squares line. Let $\varphi^* = l_1 u^* + l_2 b^*$ be the true least-squares or best linear unbiased (BLU) estimator of φ based on the first m of n ordered sample observations, with u^* and b^* the BLU estimators of u and b , respectively. These estimators (u^* , b^* , and φ^*) enjoy all the large sample properties attributed to maximum-likelihood estimators, including that of asymptotic normality (see Blom [6]).

By analogy with other distributions such as the normal, one might expect u , being a location parameter, to be estimated most efficiently by a linear function of the sufficient statistics, $X_{(1,n)}$, $X_{(2,n)}$, ..., $X_{(m,n)}$. For a scale parameter such as b , however, one might conjecture that considerably more efficient estimation could be achieved by some other means. That such a conjecture may well be unjustified is demonstrated by Table A-8B(6) in Dixon and Massey [7]. This table demonstrates the

extremely high efficiency of the best linear unbiased estimator of the Gaussian scale parameter σ with respect to the uniformly minimum variance unbiased estimator which is nonlinear. The efficiency is 100% when $m = 2$, is at its lowest (98.8%) for $n = m = 6$, and increases with n for $n > 6$. This fact, along with results given in [8], supports the author's conjecture that the best linear unbiased estimator of b has very high efficiency with respect to any unbiased estimator of b which is obtainable. The least-squares estimator $\hat{\varphi}^*$ of φ also has an advantage in that the estimate can be calculated directly as a linear function $\sum_{i=1}^m w_i X_{(i,n)}$ of weights $\{w_i\} = \lambda_1 \{a_i\} + \lambda_2 \{c_i\}$, $i=1,2,\dots,m$, which can be determined from the first moments and second-moment matrix of the reduced order statistics, $Y_1, Y_2, \dots, Y_m = (X_{(1,n)} - u)/b, (X_{(2,n)} - u)/b, \dots, (X_{(m,n)} - u)/b$ for any given m and n . The weights $\{a_i\}$ and $\{c_i\}$ allow for calculation of the BLU estimates of u and b respectively. The first- and second-moment matrices of the reduced order statistics and the weights for obtaining the estimates were determined in [3] for $2 \leq n \leq 25$, $2 \leq m \leq n$. The variances σ_u^2 and σ_b^2 of u^* and b^* , respectively, and σ_{ub}^2 , the covariance of these estimators, were also calculated for the same values of m and n .

In [9], it is shown that for the class of linear estimators of φ based on the first m of n extreme-value order statistics and with expected squared-error loss independent of u , there is a unique best

one given by $\tilde{\varphi} = l_1(u^* - [\beta/(1+\gamma)]b^* + [l_2/(1+\gamma)]b^* \equiv l_1\tilde{u} + l_2\tilde{b}$, and with expected squared error equal to

$$\begin{aligned} & [l_1^2 E(LU) + 2l_1l_2 E(CP) + l_2^2 E(LB)]b^2 \equiv \\ & \{l_1^2\alpha + 2l_1l_2\beta + l_2^2\gamma - [(l_1\beta + l_2\gamma)^2/(1+\gamma)]\}b^2, \end{aligned} \quad (2)$$

for all m and n . Let loss be defined as squared error divided by b^2 . Then $\tilde{\varphi}$ is the best among linear estimators of φ invariant under location and scalar transformations (the best linear invariant estimator) and has been shown in [10] to be the unique admissible minimax linear estimator of φ based on $X_{(1,n)}, X_{(2,n)}, \dots, X_{(m,n)}$ for all m and n . It also has all the asymptotic properties of the BLU estimator plus that of asymptotic unbiasedness. Therefore, for the values of m and n for which tables of weights for obtaining the estimates based on the estimation rules u^* and b^* and tables of the covariance matrices of these estimators are available, weights $\{W_i\} = l_1\{A_i\} + l_2\{C_i\}$ for obtaining the BLI estimator $\tilde{\varphi}$ of φ , hence of u , b , or $x_R = u + b \log \log(1/R)$, are easily obtainable. The expected error for \tilde{u} , \tilde{b} , or \tilde{x}_R (the BLI estimator of x_R) can also be calculated from (2). The weights, $\{A_i\} = \{a_i - [\beta/(1+\gamma)]c_i\}$ and $\{C_i\} = \{c_i/(1+\gamma)\}$, functions of m and n , have been calculated and are given in Table C.I for $2 \leq n \leq 25$, $2 \leq m \leq n$. Values of $E(LU)$ and $E(LB)$, the expected losses of u and b , respectively, and

$E(CP) \equiv E(\tilde{ub} - ub)/b^2$ were also calculated and appear in Table C.I.

The indices n , m , and i all appear in Table C.I as capital letters since no lower-case letters are available for the computer output. The method of utilizing the weights for estimating the parameters is illustrated in Figure 1. In this example, the ordering of the failure times and the calculation of the estimates has been achieved via a computer program which uses tapes upon which both the BLU and BLI weights are stored. It is evident, however, that a hand calculation of the estimates can be made with little difficulty.

EXAMPLE SHOWING METHOD OF COMPUTING PARAMETER ESTIMATES FROM FAILURE-TIME DATA

FAILURE TIMES			WEIGHTS	
n = 24				
RANDOMIZED ORDER	ASCENDING ORDER	NATURAL LOGARITHMS	A_i	C_i
119.0000	6.0000	1.7917595	0.0112481	-0.0244931
138.0000	8.6000	2.1517622	0.0137390	-0.0298109
146.0000	17.9000	2.8791985	0.0160213	-0.0309171
151.0000	18.0000	2.8903718	0.0182155	-0.0314605
27.5000	27.5000	3.3141860	0.0203699	-0.0316140
69.0000	33.5000	3.5115454	0.0225141	-0.0314243
150.0000	50.5000	3.9219733	0.0246466	-0.0309303
8.6000	51.5000	3.9415818	0.0268383	-0.0300915
51.5000	69.0000	4.2341065	0.0290150	-0.0289885
89.0000	74.0000	4.3040651	0.0313289	-0.0274772
109.0000	74.0000	4.3040651	0.0335892	-0.0256841
6.0000	89.0000	4.4886364	0.0359094	-0.0234404
74.0000	109.0000	4.6913479	0.0385429	-0.0207397
118.0000	118.0000	4.7768847	0.0411308	-0.0175568
141.0000	119.0000	4.7791235	0.0439276	-0.0137101
18.0000	132.0000	4.9272537	0.0468615	-0.0091529
33.5000	141.0000	4.9487599	0.0500545	-0.0036386
144.0000	144.0000	4.9698133	0.0535307	0.0030549
17.8000	146.0000	4.9836066	0.0573800	0.0113897
153.0000	150.0000	5.0106353	0.0617825	0.0219454
153.1000	151.0000	5.0172799	0.0669268	0.0360073
153.2000	151.0000	5.0304379	0.0733312	0.0559322
50.5000	153.1000	5.0310913	0.0821530	0.0882378
74.0000	153.2000	5.0317443	0.1008632	0.1981225
			$\bar{u} = 4.61398$	$\bar{b} = 0.56889$
SUMMARY				
$\bar{u} = 4.61398$		$\bar{b} = 0.56889$		
$\log\log(1/.90) = -2.25037$		$\log\log(1/.95) = -2.97020$		
$\bar{x}_{.90} = \bar{u} + \bar{b}\log\log(1/.90) = 3.33376$		$\bar{T}_{.90} = 28.04366$		
$\bar{x}_{.95} = \bar{u} + \bar{b}\log\log(1/.95) = 2.92426$		$\bar{T}_{.95} = 18.62038$		
		$\bar{T}_R = \exp(\bar{x}_R)$		

Figure 1

ACCURACY OF THE TABLES

The calculation of the moments of the order statistics, the original BLU weights $\{a_i\}$ and $\{c_i\}$, and the estimator covariance matrices were all based on derivations and results of Lieblein in [11] and [12]. All of the computer programs involved in making these calculations incorporated Rocketdyne's N-precision (somewhat more accurate than double precision) subroutines. Three constants, $\pi^2/6$, $\pi^2/12$, and Euler's constant, correct to 22 significant figures, were read in. All other preliminary values used in the computations were generated by using N-precision floating-point arithmetic. Differencing of the tabled values indicated that the numbers given were accurate to within a unit in the eighth decimal place. It should be noted, too, that the weights and the covariance matrices agreed precisely with those given by White for $2 \leq n \leq 20$ in [13] for the number of significant figures listed by him. In our computations the variances and covariances of the estimators were given by the values of the Lagrange multipliers specifying the constraints of invariance and unbiasedness for u^* and b^* as indicated in [9], and thus did not require a separate calculation. The BLI weights with the expected losses were obtained directly from the BLU weights and the variances and covariances of u^* and b^* . Six decimal places only are given for the weights. The eight decimal places included for the expected losses imply additional accuracy for the weights.

ESTIMATION PROCEDURE FOR SAMPLES LARGER THAN 25

If n is greater than 25, the weights in Table C.I or the computer routine using these weights cannot be used directly. Estimates may be obtained, however, by randomly dividing the sample into an arbitrary number of sub-samples each of which has sample size less than 25. An estimate of b , u , or x_R is then obtained as an average of the best linear unbiased sub-estimates where each is weighted by the reciprocal of the variance of the sub-estimator. An approximation to the best linear invariant estimate of each parameter can then be obtained from this average which is an unbiased linear estimate. If the total sample is divided into a set of k uncensored sub-samples of equal size, the Cramér-Rao efficiency of the estimate obtained by averaging is a function of the size n_j of the sub-sample only, increasing with increasing n_j (see Lieblein [12]). For more irregular partitionings of the sample, the determination of efficiency becomes more complex. For a fixed number k of sub-samples, however, the manner in which the sample is divided (e.g., two equal sub-samples or one large and one small) has little effect on efficiency. In any case, when the total sample is greater than 25, it can be seen from [8] that the Cramér-Rao efficiency of the estimate of reliable life will not usually fall below 87% even for R close to 1 unless there is a great deal of censoring.

Obtaining the proper unbiased estimate of $l_1 u + l_2 b$ (for each sub-sample) from which a weighted average may be obtained involves converting the estimates obtained from \tilde{u} and \tilde{b} to unbiased estimates. To accomplish this, we note that since

$$\tilde{\varphi} = l_1 \tilde{u} + l_2 \tilde{b} = l_1 [u^* - (\beta/(1+\gamma))b^*] + [l_2/(1+\gamma)]b^*, \text{ for all } l_1 \text{ and } l_2, \text{ then } b^* = (1+\gamma)\tilde{b} \text{ and } u^* = \tilde{u} + (\beta/(1+\gamma))b^* = \tilde{u} + E(CP)b^*.$$

Furthermore, since $E(LB) = \gamma/(1+\gamma)$ and $E(CP) = \beta/(1+\gamma)$,

$$\gamma = E(LB)/[1-E(LB)], \quad b^* = \tilde{b}/[1-E(LB)], \text{ and } \beta = E(CP)/[1-E(LB)]. \text{ Thus}$$

$$u^* = \tilde{u} + [E(CP)/[1-E(LB)]]\tilde{b}. \text{ The variance } \alpha \text{ of } u^* \text{ is}$$

$$[E(LU) + \beta^2/(1+\gamma)]b^2 = [E(LU) + [E(CP)]^2/[1-E(LB)]]b^2. \text{ We let } k \text{ be}$$

the total number of sub-samples and we let Q_j be equal to

$$l_1^2 \alpha_j + 2l_1 l_2 \beta_j + l_2^2 \gamma_j, j = 1, 2, \dots, k.$$

Then the variance of the unbiased estimator formed by the weighted

$$\text{average, } \tilde{\varphi} = \frac{1}{\sum_{j=1}^k (1/Q_j)} \sum_{j=1}^k (1/Q_j)(l_1 u_j^* + l_2 b_j^*) \text{ is}$$

$$\frac{b^2}{\left[\sum_{j=1}^k (1/Q_j) \right]^2} \sum_{j=1}^k (1/Q_j)^2 (l_1^2 \alpha_j + 2l_1 l_2 \beta_j + l_2^2 \gamma_j) = \frac{b^2}{\sum_{j=1}^k (1/Q_j)^2}, \text{ where}$$

the subscript j indicates with which of the sub-samples a quantity is associated. It is simple to demonstrate that $\tilde{\varphi}$ has the minimum variance among unbiased estimators based on the sub-estimators based on the given sub-samples.

The estimator $\hat{\phi} = \bar{\phi} - \bar{\beta} \bar{b} / (1 + \sum_{j=1}^k (1/\gamma_j))$ (where $\bar{b} = \frac{1}{\sum_{j=1}^k \gamma_j} \sum_{j=1}^k (1/\gamma_j) b_j^*$

is the minimum-variance unbiased estimator of b based on the given sub-

estimators $\bar{\beta} = \frac{1}{\sum_{j=1}^k (1/Q_j) \sum_{j=1}^k (1/\gamma_j)} \sum_{j=1}^k (1/Q_j)(1/\gamma_j)(L_1 \beta_j + L_2 \gamma_j)$ is the

covariance between $\bar{\phi}$ and \bar{b}) is the invariant linear function of $\bar{\phi}$ and \bar{b} with smallest expected squared deviation from ϕ . It can be shown, by using methods very similar to those used in [8] to derive the form of the Cramér-Rao bound for invariant estimators of location parameters, that $\hat{\phi}$ is the best linear invariant estimator of ϕ based on the given sub-estimators.

An alternative method of handling samples larger than 25 has been derived by McCool and is explained in [14]. For large m , however, this method requires considerable additional computation until such time as additional tables combining McCool's results with those in Table C.I are made available. Another approach is described by Johns and Lieberman in [15]. The estimates which can be obtained from tables of weights given by Johns and Lieberman are good approximations to the best linear invariant estimates of u and b . These weights are given for n equal to 10, 15, 20, 30, 50, and 100 and four values of m for each n .

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TABLE C.I

WEIGHTS FOR OBTAINING BEST LINEAR INVARIANT ESTIMATES
OF PARAMETERS OF THE EXTREME-VALUE DISTRIBUTION

A(N,M,I) = WEIGHT FOR ESTIMATING U
C(N,M,I) = WEIGHT FOR ESTIMATING B
E(LU) = EXPECTED LOSS FOR ESTIMATE OF U
E(CP) = EXPECTED CROSS PRODUCT
E(LB) = EXPECTED LOSS FOR ESTIMATE OF B

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
2	2	1	0.110731	-0.421383	5	2	1	-0.481434	-0.472962
		2	0.889269	0.421383			2	1.481434	0.472962
E(LU)			0.65712995					1.24921018	
E(CP)			0.03757418		E(LU)			0.53379141	
E(LB)				0.41583918	E(CP)				0.47230837
					E(LB)				
3	2	1	-0.166001	-0.452110	5	3	1	-0.137958	-0.306562
		2	1.166001	0.452110			2	-0.025510	-0.257087
E(LU)			0.79546061				3	1.163468	0.563650
E(CP)			0.25750956		E(LU)			0.49029288	
E(LB)				0.45005549	E(CP)			0.16612899	
					E(LB)				0.29419192
3	3	1	0.081063	-0.278666	5	4	1	-0.006983	-0.217766
		2	0.251001	-0.190239			2	0.059652	-0.199351
		3	0.667936	0.468904			3	0.156664	-0.118927
E(LU)			0.40240741				4	0.790668	0.536044
E(CP)			-0.01842169		E(LU)			0.29062766	
E(LB)				0.25634620	E(CP)			0.03076329	
					E(LB)				0.20241854
4	2	1	-0.346974	-0.465455	5	5	1	0.052975	-0.158131
		2	1.346974	0.465455			2	0.103531	-0.155707
E(LU)			1.01477788				3	0.163808	-0.111820
E(CP)			0.41350875				4	0.246092	-0.005600
E(LB)				0.46438768			5	0.433593	0.431259
					E(LU)			0.23040495	
4	3	1	-0.044975	-0.297651				-0.02913523	
		2	0.088057	-0.234054				0.14284288	
		3	0.956918	0.531705	E(LU)				
E(LU)			0.42315147		E(CP)				
E(CP)			0.08477554		E(LB)				
E(LB)				0.28172930					
					6	2	1	-0.588298	-0.477782
4	4	1	0.064336	-0.203052			2	1.588298	0.477782
		2	0.147340	-0.182749	E(LU)			1.48102383	
		3	0.261510	-0.070109	E(CP)			0.63148980	
		4	0.526813	0.455910	E(LB)				0.47734078
E(LU)			0.29247651						
E(CP)			-0.02831210		6	3	1	-0.211474	-0.311047
E(LB)				0.18386193			2	-0.112994	-0.271381
							3	1.324468	0.583229
					E(LU)			0.57539484	
					E(CP)			0.23269670	
					E(LB)				0.30173252

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
6	4	1	-0.063569	-0.225141	7	6	1	0.013524	-0.138436
		2	-0.006726	-0.209083			2	0.041588	-0.140342
		3	0.079882	-0.146386			3	0.075499	-0.121821
		4	0.990412	0.580610			4	0.117461	-0.082938
E(LU)			0.31552097				5	0.172092	-0.015394
E(CP)			0.08035062				6	0.579635	0.498931
E(LB)			0.21242254		E(LU)			0.18269947	
					E(CP)			-0.00130057	
					E(LB)			0.12760617	
6	5	1	0.007521	-0.169920	7	7	1	0.038743	-0.108323
		2	0.048328	-0.166319			2	0.064086	-0.113479
		3	0.101608	-0.129510			3	0.090785	-0.103569
		4	0.172859	-0.054453			4	0.120971	-0.078748
		5	0.669685	0.520201			5	0.157657	-0.032632
E(LU)			0.22351297				6	0.207825	0.054727
E(CP)			0.00888019				7	0.319934	0.382022
E(LB)			0.15690540					0.16219070	
					E(LU)			-0.02578937	
					E(CP)			0.09836496	
					E(LB)				
6	6	1	0.044826	-0.128810	8	2	1	-0.752513	-0.483610
		2	0.079377	-0.132102			2	1.752513	0.483616
		3	0.117541	-0.111951				1.91861540	
		4	0.163591	-0.064666				0.78453314	
		5	0.226486	0.031796				0.48337662	
		6	0.368179	0.405733					
E(LU)			0.19030430		E(LU)				
E(CP)			-0.02771574		E(CP)				
E(LB)			0.11657671		E(LB)				
7	2	1	-0.676894	-0.481140	8	3	1	-0.323875	-0.317890
		2	1.676894	0.481140			2	-0.243808	-0.288231
E(LU)			1.70468001				3	1.567683	0.606120
E(CP)			0.71366553		E(LU)			0.76198737	
E(LB)			0.48082310		E(CP)			0.33734068	
					E(LB)			0.31047652	
7	3	1	-0.272195	-0.315369	8	4	1	-0.149973	-0.232805
		2	-0.184061	-0.281139			2	-0.105015	-0.220324
		3	1.456255	0.596507			3	-0.032257	-0.176675
E(LU)			0.66758707				4	1.287245	0.629805
E(CP)			0.28885432					0.39805551	
E(LB)			0.30681307		E(LU)			0.15928131	
					E(CP)			0.22335819	
					E(LB)				
7	4	1	-0.110274	-0.229691	8	5	1	-0.062656	-0.180231
		2	-0.060226	-0.215613			2	-0.032248	-0.176510
		3	0.018671	-0.164168			3	0.012767	-0.149566
		4	1.151829	0.609472			4	0.072446	-0.101642
E(LU)			0.35340223				5	1.009691	0.607948
E(CP)			0.12260834					0.25192092	
E(LB)			0.21884662		E(LU)			0.07129172	
					E(CP)			0.17037848	
					E(LB)				
7	5	1	-0.030368	-0.176203	8	6	1	-0.013509	-0.143834
		2	0.004333	-0.172399			2	0.010292	-0.145006
		3	0.052957	-0.141218			3	0.041357	-0.128393
		4	0.117599	-0.082820			4	0.080475	-0.095696
		5	0.855480	0.572649			5	0.130327	-0.043280
E(LU)			0.23316740				6	0.751058	0.556209
E(CP)			0.04212562		E(LU)			0.18599844	
E(LB)			0.16497315		E(CP)			0.02247163	
					E(LB)			0.13422386	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
8	7	1	0.015973	-0.116317	9	7	1	-0.004220	-0.120988
		2	0.036729	-0.120331			2	0.013386	-0.124245
		3	0.060439	-0.110582			3	0.035068	-0.115091
		4	0.088239	-0.088450			4	0.061198	-0.095508
		5	0.122062	-0.050995			5	0.093013	-0.064162
		6	0.165529	0.009700			6	0.132740	-0.017187
		7	0.511030	0.476975			7	0.668815	0.537180
E(LU)			0.15505149		E(LU)			0.15547192	
E(CP)			-0.00641304		E(CP)			0.01139509	
E(LB)			0.10726405		E(LB)			0.11278822	
8	8	1	0.034052	-0.093270	9	8	1	0.016797	-0.100711
		2	0.033552	-0.098886			2	0.032919	-0.104750
		3	0.073452	-0.093994			3	0.050582	-0.095608
		4	0.095062	-0.079752			4	0.070497	-0.086226
		5	0.119768	-0.053918			5	0.093635	-0.063541
		6	0.149934	-0.010179			6	0.121560	-0.028346
		7	0.191236	0.069325			7	0.157175	0.026525
		8	0.282943	0.360675			8	0.456836	0.455956
E(LU)			0.14136026		E(LU)			0.13496842	
E(CP)			-0.02386561		E(CP)			-0.00906894	
E(LB)			0.08501680		E(LB)			0.09236358	
9	2	1	-0.818444	-0.485517	9	9	1	0.030338	-0.081777
		2	1.818444	0.485517			2	0.045872	-0.087308
E(LU)			2.12272209				3	0.061368	-0.085084
E(CP)			0.84680378				4	0.077742	-0.076470
E(LB)			0.48532951				5	0.095769	-0.060667
9	3	1	-0.368833	-0.319786			6	0.116517	-0.035136
		2	-0.295280	-0.293621			7	0.141932	0.006001
		3	1.664113	0.613407			8	0.176764	0.078828
E(LU)			0.85621748				9	0.253697	0.341614
E(CP)			0.37995861		E(LU)			0.12529518	
E(LB)			0.31324611		E(CP)			-0.02209438	
9	4	1	-0.184461	-0.235080				0.07482425	
		2	-0.143505	-0.223891	10	2	1	-0.876869	-0.487022
		3	-0.075815	-0.185970			2	1.876869	0.487022
		4	1.403781	0.644941	E(LU)			2.31744054	
E(LU)			0.44625568		E(CP)			0.90232208	
E(CP)			0.19160927		E(LB)			0.48687150	
E(LB)			0.22671251		10	3	1	-0.408602	-0.321265
9	5	1	-0.090726	-0.183061			2	-0.340443	-0.297858
		2	-0.063541	-0.179515			3	1.749045	0.619124
		3	-0.021495	-0.155825	E(LU)			0.94907551	
		4	0.034159	-0.115133	E(CP)			0.41795081	
		5	1.141604	0.633534	E(LB)			0.31541467	
E(LU)			0.27605014		10	4	1	-0.214930	-0.236817
E(CP)			0.09715351				2	-0.177223	-0.226688
E(LB)			0.17429417				3	-0.113820	-0.193159
9	6	1	-0.037118	-0.147411			4	1.505973	0.656663
		2	-0.016377	-0.148150	E(LU)			0.49619736	
		3	0.012499	-0.133219	E(CP)			0.22047816	
		4	0.049305	-0.105060	E(LB)			0.22930885	
		5	0.053814	-0.062073					
		6	0.896078	0.595913					
E(LU)			0.19579592						
E(CP)			0.04378261						
E(LB)			0.13880129						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)		N	M	I	A(N,M,I)	C(N,M,I)
10	5	1	-0.115524	-0.185169		10	10	1	0.027331	-0.072734
		2	-0.090868	-0.181821				2	0.040034	-0.077971
		3	-0.051341	-0.160697				3	0.052496	-0.077242
		4	0.000975	-0.125311				4	0.065408	-0.071876
		5	1.250104	0.652997				5	0.079283	-0.061652
E(LU)			0.30344549					6	0.094638	-0.045420
E(CP)				0.1212305				7	0.112414	-0.020698
E(LB)				0.7727542				8	0.134239	0.017927
								9	0.164179	0.085070
10	6	1	-0.058017	-0.149985				10	0.230001	0.324597
		2	-0.039595	-0.150451	E(LU)				0.11252220	
		3	-0.012513	-0.136941	E(CP)				-0.02050852	
		4	0.022314	-0.112224	E(LB)				0.06679250	
		5	0.065750	-0.075721						
		6	1.022062	0.625321		11	2	1	-0.929310	-0.488243
E(LU)			0.20973843					2	1.929310	0.488243
E(CP)				0.06299841	E(LU)				2.50340024	
E(LB)				0.14219828	E(CP)				0.95239887	
					E(LB)				0.48812000	
10	7	1	-0.022198	-0.124170						
		2	-0.006909	-0.126894		11	3	1	-0.444245	-0.322452
		3	0.013224	-0.118392				2	-0.380642	-0.301277
		4	0.037994	-0.100924				3	1.824887	0.62729
		5	0.068153	-0.073988	E(LU)				1.03995578	
		6	0.105164	-0.035501	E(CP)				0.45220741	
		7	0.804572	0.579868	E(LB)				0.31715330	
E(LU)			0.16066059							
E(CP)				0.02762724		11	4	1	-0.242206	-0.238188
E(LB)				0.11670571				2	-0.207204	-0.228941
								3	-0.147490	-0.198888
10	8	1	0.001179	-0.104082				4	1.596900	0.666017
		2	0.014889	-0.108163	E(LU)				0.54681985	
		3	0.030998	-0.103119	E(CP)				0.24633583	
		4	0.049734	-0.090835	E(LB)				0.23138012	
		5	0.071745	-0.070902						
		6	0.098114	-0.041560		11	5	1	-0.137718	-0.186803
		7	0.130649	0.000799				2	-0.115110	-0.183651
		8	0.602892	0.517864				3	-0.077762	-0.164597
E(LU)			0.13403554					4	-0.028411	-0.133278
E(CP)				0.00474963				5	1.359000	0.668329
E(LB)				0.79704810	E(LU)				0.33282848	
					E(CP)				0.14129911	
10	9	1	0.016841	-0.087538	E(LB)				0.17962678	
		2	0.029807	-0.092405						
		3	0.043570	-0.089839		11	6	1	-0.076739	-0.151936
		4	0.058640	-0.081428				2	-0.060142	-0.152221
		5	0.075576	-0.066855				3	-0.034581	-0.135907
		6	0.095169	-0.044670				4	-0.001490	-0.117886
		7	0.118707	-0.011816				5	0.039510	-0.086131
		8	0.148575	0.038159				6	1.133434	0.648081
		9	0.413116	0.436394	E(LU)				0.22640907	
E(LU)			0.11965747		E(CP)				0.08045010	
E(CP)				-0.01043859	E(LB)				0.14483423	
E(LB)				0.08100409						
						11	7	1	-0.038349	-0.126507
								2	-0.024842	-0.128838
								3	-0.005964	-0.120951
								4	0.017632	-0.105219
								5	0.046354	-0.081602
								6	0.061182	-0.048929
								7	0.923987	0.612047
					E(LU)				0.16905710	
					E(CP)				0.04246025	
					E(LB)				0.11966982	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
11	8	1	-0.012943	-0.106922	12	3	1	-0.476530	-0.323426
		2	-0.001050	-0.110498			2	-0.416836	-0.304093
		3	0.013869	-0.105662			3	1.893367	0.627519
		4	0.031661	-0.094495	E(LU)		1.12857097		
		5	0.052723	-0.076693	E(CP)		0.48338667		
		6	0.077815	-0.051525	E(LB)		0.31859354		
		7	0.108161	-0.016860					
		8	0.729765	0.562564	12	4	1	-0.266888	-0.239300
E(LU)			0.13669382				2	-0.234180	-0.230796
E(CP)			0.01751192				3	-0.177681	-0.203562
E(LB)			0.10043756				4	1.678749	0.673657
					E(LU)		0.59748043		
11	9	1	0.004425	-0.091115	E(CP)		0.27026774		
		2	0.015498	-0.095437	E(LB)		0.23307201		
		3	0.028023	-0.092780					
		4	0.042178	-0.084833	12	5	1	-0.157792	-0.188109
		5	0.058340	-0.071581			2	-0.136884	-0.185142
		6	0.077093	-0.052182			3	-0.101445	-0.167790
		7	0.099349	-0.024880			4	-0.054640	-0.139693
		8	0.126592	0.013606			5	1.450761	0.680734
		9	0.548502	0.499201	E(LU)		0.36338878		
E(LU)			0.11809425		E(CP)		0.16042600		
E(CP)			0.00058414		E(LB)		0.18153147		
E(LB)			0.08503131						
					12	6	1	-0.093679	-0.153471
11	10	1	0.016502	-0.077717			2	-0.078561	-0.153632
		2	0.027205	-0.082449			3	-0.054320	-0.142329
		3	0.038291	-0.081388			4	-0.022769	-0.122474
		4	0.050160	-0.075977			5	0.016136	-0.094355
		5	0.063170	-0.066222			6	1.233193	0.666261
		6	0.077772	-0.051429	E(LU)		0.24490094		
		7	0.094625	-0.030120	E(CP)		0.09641022		
		8	0.114811	0.000537	E(LB)		0.14694548		
		9	0.140333	0.046381					
		10	0.377130	0.418384	12	7	1	-0.052987	-0.128308
E(LU)			0.10756449				2	-0.040893	-0.130339
E(CP)			-0.01109747				3	-0.023072	-0.123007
E(LB)			0.07207183				4	-0.000515	-0.107712
							5	0.026930	-0.087621
11	11	1	0.024850	-0.065444			6	0.059918	-0.059256
		2	0.035456	-0.070318			7	1.030620	0.637304
		3	0.045727	-0.070456	E(LU)		0.17967935		
		4	0.056215	-0.067076	E(CP)		0.05607919		
		5	0.067261	-0.060207	E(LB)		0.12200601		
		6	0.079220	-0.049300					
		7	0.092560	-0.033156	12	8	1	-0.025785	-0.109045
		8	0.108034	-0.009427			2	-0.015312	-0.112224
		9	0.127068	0.026879			3	-0.001353	-0.107627
		10	0.153197	0.089148			4	0.015634	-0.097276
		11	0.210412	0.309357			5	0.035853	-0.081361
E(LU)			0.10212039				6	0.059835	-0.059315
E(CP)			-0.01910164				7	0.088444	-0.029900
E(LB)			0.06030372				8	0.842684	0.596748
					E(LU)		0.14186580		
12	2	1	-0.976872	-0.489254	E(CP)		0.02930146		
		2	1.976872	0.489254	E(LB)		0.10304331		
E(LU)			2.68127021						
E(CP)			0.99799849						
E(LB)			0.48915157						

TABLE OF WEIGHTS (CONTINUED)

	N	M	I	A(N,M,I)	C(N,M,I)		N	M	I	A(N,M,I)	C(N,M,I)
	12	9	1	-0.006944	-0.093658		13	3	1	-0.506031	-0.324239
			2	0.002669	-0.097540				2	-0.449735	-0.306454
			3	0.014239	-0.094893				3	1.955765	0.630694
			4	0.027669	-0.087448	E(LU)				1.21490934	
			5	0.043189	-0.075371	E(CP)				0.51198847	
			6	0.061225	-0.058180	E(LB)				0.31979363	
			7	0.082441	-0.034802		13	4	1	-0.289420	-0.240219
			8	0.107856	-0.003342				2	-0.258687	-0.232349
			9	0.667655	0.545234				3	-0.205024	-0.207450
E(LU)				0.11929957					4	1.753131	0.680018
E(CP)				0.01087297		E(LU)				0.64778295	
E(LB)				0.08799386		E(CP)				0.29204583	
	12	10	1	0.006411	-0.080881	E(LB)				0.23448055	
			2	0.015598	-0.085171		13	5	1	-0.176109	-0.189177
			3	0.025675	-0.083952				2	-0.156637	-0.186371
			4	0.036799	-0.078714				3	-0.122893	-0.170454
			5	0.049211	-0.069610				4	-0.078337	-0.144971
			6	0.063256	-0.056237				5	1.533976	0.690983
			7	0.07947	-0.037675	E(LU)				0.39459617	
			8	0.098522	-0.012272	E(CP)				0.1799724	
			9	0.121752	0.022956	E(LB)				0.18310709	
			10	0.503338	0.481555		13	6	1	-0.109140	-0.154711
E(LU)				0.10573191					2	-0.095246	-0.154785
E(CP)				-0.00210755					3	-0.072165	-0.144347
E(LB)				0.07557504					4	-0.041997	-0.126268
	12	11	1	0.012382	-0.069798				5	-0.004940	-0.101028
			2	0.024957	-0.074285				6	1.323488	0.681140
			3	0.034105	-0.074131	E(LU)				0.26460952	
			4	0.043790	-0.070617	E(CP)				0.11109896	
			5	0.054149	-0.063891	E(LB)				0.14867755	
			6	0.065515	-0.053621		13	7	1	-0.066358	-0.129743
			7	0.078264	-0.039034				2	-0.055414	-0.131538
			8	0.092952	-0.018715				3	-0.038503	-0.124701
			9	0.110521	0.009948				4	-0.016879	-0.111609
			10	0.137666	0.052280				5	0.009416	-0.092649
			11	0.347033	0.401864				6	0.040810	-0.067475
E(LU)				0.09775217					7	1.126930	0.657714
E(CP)				-0.01134890		E(LU)				0.19187273	
E(LB)				0.06487266		E(CP)				0.06864731	
	12	12	1	0.022771	-0.059449	E(LB)				0.12390133	
			2	0.031776	-0.063952		13	8	1	-0.037540	-0.110704
			3	0.040408	-0.064601				2	-0.028206	-0.113563
			4	0.049122	-0.062489				3	-0.015049	-0.109206
			5	0.058175	-0.057754				4	0.001231	-0.099644
			6	0.067800	-0.050137				5	0.020686	-0.085264
			7	0.078281	-0.039010				6	0.043677	-0.065581
			8	0.090017	-0.023199				7	0.070830	-0.039995
			9	0.103664	-0.000505				8	0.944372	0.623896
			10	0.120475	0.033696	E(LU)				0.14885020	
			11	0.143566	0.091751	E(CP)				0.04022462	
			12	0.193747	0.295648	E(LB)				0.10512398	
E(LU)				0.09348388							
E(CP)				-0.01785537							
E(LB)				0.05495436							
	13	2	1	-1.020378	-0.490105						
			2	2.020377	0.490105						
E(LU)				2.85169894							
E(CP)				1.03985071							
E(LB)				0.49001823							

Figure 1. The effect of the concentration of the *Agaricus bisporus* spores on the growth of *Agaricus bisporus* on the substrate.

[illegible]

TABLE OF WEIGHTS (CONTINUED)

N	M	i	A(N,M,i)	C(N,M,i)	N	M	i	A(N,M,i)	C(N,M,i)
14	7	1	-0.078656	-0.130915	14	12	1	0.008361	-0.065816
		2	-0.069666	-0.132521			2	0.015058	-0.069728
		3	-0.052554	-0.126123			3	0.022076	-0.069862
		4	-0.031776	-0.114051			4	0.029552	-0.067659
		5	-0.006522	-0.096788			5	0.037615	-0.063070
		6	0.023467	-0.074184			6	0.046411	-0.056130
		7	1.214708	0.674581			7	0.056132	-0.046558
E(LU)			0.20518434				8	0.067039	-0.033834
E(CP)			0.08030259				9	0.079506	-0.017101
E(LB)				0.12547311			10	0.094096	0.005064
							11	0.111723	0.035156
14	8	1	-0.048365	-0.112041			12	0.432431	0.449638
		2	-0.039964	-0.114637	E(LU)			0.08771669	
		3	-0.027495	-0.110509	E(CP)			-0.00506397	
		4	-0.011849	-0.101635	E(LB)				0.06168210
		5	0.006905	-0.088422					
		6	0.029002	-0.070735	14	13	1	0.014760	-0.057849
		7	0.054897	-0.048074			2	0.021453	-0.061764
		8	1.036868	0.646052			3	0.028064	-0.062506
E(LU)			0.15716466				4	0.034842	-0.061074
E(CP)			0.05038249				5	0.041933	-0.057693
E(LB)				0.10683049			6	0.069474	-0.052317
							7	0.057619	-0.044707
14	9	1	-0.027030	-0.097117			8	0.066569	-0.034420
		2	-0.019516	-0.100334			9	0.076605	-0.020713
		3	-0.009363	-0.097327			10	0.088151	-0.002338
		4	0.002928	-0.091298			11	0.101914	0.022943
		5	0.017368	-0.081103			12	0.119200	0.059643
		6	0.034165	-0.067124			13	0.299416	0.372795
		7	0.053685	-0.048921	E(LU)			0.08276211	
		8	0.076476	-0.025720	E(CP)			-0.01123278	
		9	0.871267	0.609445	E(LB)				0.05400148
E(LU)			0.12719148						
E(CP)			0.02941694		14	14	1	0.019487	-0.050186
E(LB)				0.09216556			2	0.026238	-0.054008
							3	0.032614	-0.055130
14	10	1	-0.011580	-0.084931			4	0.038947	-0.054419
		2	-0.004548	-0.082528			5	0.045399	-0.052075
		3	0.004100	-0.087207			6	0.052097	-0.048006
		4	0.014144	-0.082451			7	0.059168	-0.042197
		5	0.025647	-0.074573			8	0.066767	-0.034099
		6	0.038794	-0.063473			9	0.075102	-0.023149
		7	0.053879	-0.048768			10	0.084482	-0.008285
		8	0.071335	-0.029776			11	0.095426	0.012430
		9	0.091783	-0.005398			12	0.108942	0.043015
		10	0.716445	0.565105			13	0.127523	0.094166
E(LU)			0.10903536				14	0.167807	0.272004
E(CP)			0.01430729		E(LU)			0.07996685	
E(LB)				0.08024763	E(CP)			-0.01576372	
					E(LB)				0.04665712
14	11	1	-0.000170	-0.074686	15	2	1	-1.097617	-0.491458
		2	0.006622	-0.078499			2	2.097617	0.491458
		3	0.014283	-0.078064	E(LU)			3.17256460	
		4	0.022800	-0.074680	E(CP)			1.11445612	
		5	0.032273	-0.068624	E(LB)				0.49139327
		6	0.042866	-0.059816					
		7	0.054817	-0.047926	15	3	1	-0.558330	-0.325521
		8	0.068463	-0.032355			2	-0.507671	-0.310191
		9	0.084290	-0.012126			3	2.066007	0.635712
		10	0.103025	0.014349	E(LU)			1.38015851	
		11	0.570731	0.512429	E(CP)			0.56295169	
E(LU)			0.09566494		E(LB)				0.32168886
E(CP)			0.00320055						
E(LB)				0.07027548					

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
15	4	1	-0.329324	-0.241651	15	10	1	-0.019626	-0.086339
		2	-0.301829	-0.234806			2	-0.013383	-0.089664
		3	-0.252948	-0.213548			3	-0.005271	-0.088341
		4	1.884101	0.690005			4	0.004351	-0.083828
E(LU)			0.74642859				5	0.015475	-0.076474
E(CP)			0.33084387				6	0.028227	-0.066261
E(LB)			0.23669248				7	0.042832	-0.052943
15	5	1	-0.208525	-0.190823			8	0.059624	-0.036054
		2	-0.191357	-0.188323			9	0.079072	-0.014863
		3	-0.160491	-0.174645			10	0.808700	0.594768
		4	-0.119743	-0.153153	E(LU)			0.11121862	
		5	1.680121	0.706944	E(CP)			0.02177795	
E(LU)			0.45754555		E(LB)			0.08192516	
E(CP)			0.20933279		15	11	1	-0.007450	-0.076297
E(LB)			0.18556433				2	-0.001467	-0.079835
15	6	1	-0.136498	-0.156597			3	0.005652	-0.079332
		2	-0.124518	-0.156563			4	0.013759	-0.076068
		3	-0.103401	-0.147517			5	0.022893	-0.070355
		4	-0.075614	-0.132162			6	0.033174	-0.062181
		5	-0.041680	-0.111215			7	0.044787	-0.051331
		6	1.481712	0.704074			8	0.057997	-0.037396
E(LU)			0.30614004				9	0.073180	-0.019723
E(CP)			0.13734100				10	0.090865	0.002701
E(LB)			0.15135556				11	0.666610	0.549817
15	7	1	-0.090036	-0.131891	E(LU)			0.09681113	
		2	-0.080850	-0.133342	E(CP)			0.00989471	
		3	-0.065446	-0.127335	E(LB)			0.07212492	
		4	-0.045441	-0.116138	15	12	1	0.001756	-0.067695
		5	-0.021137	-0.100291			2	0.007624	-0.071342
		6	0.007597	-0.079774			3	0.014079	-0.071459
		7	1.295312	0.688771			4	0.021133	-0.069178
E(LU)			0.21929214				5	0.028861	-0.064779
E(CP)			0.09116039				6	0.037374	-0.058256
E(LB)			0.12679942				7	0.046827	-0.049425
15	8	1	-0.058390	-0.113143			8	0.057431	-0.037926
		2	-0.050767	-0.115520			9	0.069479	-0.023180
		3	-0.038897	-0.111607			10	0.083393	-0.004
		4	-0.023825	-0.103332			11	0.099799	0.000250
		5	-0.005717	-0.091156			12	0.532243	0.497284
		6	0.015565	-0.075053	E(LU)			0.08723346	
		7	0.040351	-0.054703	E(CP)			0.00094612	
		8	1.121680	0.664514	E(LB)			0.06376409	
E(LU)			0.16646559		15	13	1	0.008779	-0.060130
E(CP)			0.05986446				2	0.014620	-0.063805
E(LB)			0.10825884				3	0.020637	-0.064394
15	9	1	-0.035972	-0.098361			4	0.026961	-0.062900
		2	-0.029235	-0.101322			5	0.033693	-0.059574
		3	-0.019633	-0.098904			6	0.040939	-0.054417
		4	-0.007812	-0.092773			7	0.048828	-0.047269
		5	0.006156	-0.083327			8	0.057528	-0.037821
		6	0.022403	-0.070544			9	0.067265	-0.025565
		7	0.041203	-0.054142			10	0.078368	-0.009694
		8	0.062969	-0.033595			11	0.091330	0.011113
		9	0.959920	0.632967			12	0.106947	0.039155
E(LU)			0.13300106				13	0.404106	0.435302
E(CP)			0.03779810		E(LU)			0.08092217	
E(LB)			0.09370837		E(CP)			-0.00585240	
					E(LB)			0.05644073	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(A,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
15	14	1	0.014143	-0.053241	16	5	1	-0.223015	-0.191470
		2	0.020013	-0.056879			2	-0.206788	-0.189099
		3	0.025750	-0.057827			3	-0.177158	-0.176323
		4	0.031576	-0.056973			4	-0.138048	-0.156390
		5	0.037611	-0.054542			5	1.745009	0.713282
		6	0.043958	-0.050539	E(LU)			0.48908000	
		7	0.050725	-0.044833	E(CP)			0.22342597	
		8	0.058045	-0.037157	E(LB)			0.18654151	
		9	0.066092	-0.027072					
		10	0.075114	-0.013872	16	6	1	-0.148725	-0.157331
		11	0.085490	0.003612			2	-0.137508	-0.157263
		12	0.097844	0.027465			3	-0.117232	-0.148785
		13	0.113340	0.061879			4	-0.090481	-0.134532
		14	0.280298	0.359980			5	-0.057883	-0.115196
E(LU)			0.07689745				6	1.551828	0.713108
E(CP)			-0.01102126		E(LU)			0.32746210	
E(LB)			0.04980248		E(CP)			0.14915808	
					E(LB)			0.15241337	
15	15	1	0.018170	-0.046538	16	7	1	-0.100621	-0.132718
		2	0.024108	-0.050064			2	-0.092121	-0.134040
		3	0.029685	-0.051279			3	-0.077354	-0.128381
		4	0.035191	-0.050957			4	-0.058057	-0.117942
		5	0.040762	-0.049293			5	-0.034624	-0.103296
		6	0.046496	-0.046315			6	-0.007020	-0.084506
		7	0.052488	-0.041899			7	1.369798	0.700883
		8	0.058844	-0.035827	E(LU)			0.23396225	
		9	0.065696	-0.027731	E(CP)			0.10131710	
		10	0.073230	-0.017008	E(LB)			0.12793461	
		11	0.081725	-0.002653	16	8	1	-0.067719	-0.114069
		12	0.091651	0.017156			2	-0.060754	-0.116260
		13	0.103914	0.046191			3	-0.049415	-0.112545
		14	0.120784	0.094483			4	0.034868	-0.104798
		15	0.157255	0.261738			5	-0.017357	-0.093508
E(LU)			0.07477775				6	0.003178	-0.078726
E(CP)			-0.01488220				7	0.026573	-0.060251
E(LB)			0.04337628				8	1.199963	0.680159
16	2	1	-1.132243	-0.492005	E(LU)			0.17650200	
		2	2.132243	0.492005	E(CP)			0.06874770	
E(LU)			3.32404220		E(LB)			0.10947376	
E(CP)			1.14801534		16	9	1	-0.044303	-0.099396
E(LB)			0.49194784				2	-0.038218	-0.102138
16	3	1	-0.581757	-0.326035			3	-0.029094	-0.099811
		2	-0.533457	-0.311694			4	-0.017697	-0.094037
		3	2.115214	0.637730			5	-0.004166	-0.085242
E(LU)			1.45938438				6	0.011570	-0.073467
E(CP)			0.58582769				7	0.029712	-0.058535
E(LB)			0.32245028				8	0.050576	-0.040084
16	4	1	-0.347172	-0.242220			9	1.041619	0.652711
		2	-0.321026	-0.235794	E(LU)			0.13966768	
		3	-0.274186	-0.215984	E(CP)			0.04566615	
		4	1.942384	0.693998	E(LB)			0.09501012	
E(LU)			0.79453329						
E(CP)			0.34828173						
E(LB)			0.23757701						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
16	10	1	-0.027135	-0.087496	16	14	1	0.008992	-0.055269
		2	-0.021550	-0.090585			2	0.014141	-0.058750
		3	-0.013895	-0.089277			3	0.019370	-0.059563
		4	-0.004646	-0.084992			4	0.024804	-0.058635
		5	0.006132	-0.078105			5	0.030525	-0.056268
		6	0.018515	-0.068653			6	0.036615	-0.052317
		7	0.032675	-0.056482			7	0.043164	-0.046878
		8	0.048869	-0.041268			8	0.050284	-0.039699
		9	0.067459	-0.022503			9	0.057124	-0.030467
		10	0.093576	0.619360			10	0.066884	-0.018695
E(LU)			0.11534960				11	0.076854	-0.003625
E(CP)				0.02881067			12	0.088469	0.015969
E(LB)				0.08332716			13	0.102433	0.042224
							14	0.379341	0.421953
								0.07514429	
								-0.00637294	
								0.05199709	
16	11	1	-0.014263	-0.077597	E(LU)				
		2	-0.008950	-0.080895	E(CP)				
		3	-0.002286	-0.080349	E(LB)				
		4	0.005469	-0.077213					
		5	0.014303	-0.071820	16	15	1	0.013547	-0.049291
		6	0.024297	-0.064207			2	0.018743	-0.052670
		7	0.035593	-0.054237			3	0.023778	-0.053739
		8	0.040404	-0.041625			4	0.02884	-0.053290
		9	0.063020	-0.025917			5	0.034060	-0.051538
		10	0.079847	-0.004432			6	0.039489	-0.048520
		11	0.754566	0.580293			7	0.045218	-0.044164
E(LU)			0.09897866				8	0.051338	-0.038307
E(CP)				0.01622073			9	0.057965	-0.030678
E(LB)				0.07364497			10	0.065253	-0.026850
							11	0.073425	-0.008153
							12	0.082818	0.008503
							13	0.093994	0.031075
							14	0.107995	0.063476
							15	0.263522	0.348149
								0.07182155	
								-0.01076262	
								0.04619787	
16	12	1	-0.004450	-0.069172	E(LU)				
		2	0.000732	-0.072584	E(CP)				
		3	0.006721	-0.072615	E(LB)				
		4	0.013424	-0.070383					
		5	0.020868	-0.066184	16	16	1	0.017016	-0.043375
		6	0.029134	-0.060054			2	0.022284	-0.046633
		7	0.038344	-0.051876			3	0.027208	-0.047890
		8	0.048668	-0.041398			4	0.032046	-0.047839
		9	0.060342	-0.028216			5	0.036912	-0.046675
		10	0.073692	-0.011716			6	0.041887	-0.044432
		11	0.089173	0.009035			7	0.047042	-0.041053
		12	0.623351	0.535164			8	0.052455	-0.036402
E(LU)			0.08784015				9	0.058216	-0.030249
E(CP)				0.00665801			10	0.064444	-0.022230
E(LB)				0.06543511			11	0.071304	-0.011772
							12	0.079051	0.002079
							13	0.088111	0.021044
							14	0.099315	0.048675
							15	0.114733	0.094419
							16	0.147977	0.252333
								0.06987019	
								-0.01409012	
								0.04052374	
16	13	1	0.003118	-0.061843	E(LU)				
		2	0.008256	-0.065297	E(CP)				
		3	0.013789	-0.065770	E(LB)				
		4	0.019747	-0.064259					
		5	0.026189	-0.061031	17	2	1	-1.164659	-0.492486
		6	0.033196	-0.056120			2	2.164659	0.492486
		7	0.040872	-0.049427				3.47015408	
		8	0.049357	-0.040731				1.17949167	
		9	0.058836	-0.029675				0.49243526	
		10	0.069568	-0.015710	E(LU)				
		11	0.081920	0.002010	E(CP)				
		12	0.096438	0.024833	E(LB)				
		13	0.498713	0.483018					
E(LU)			0.08025299						
E(CP)				-0.00069037					
E(LB)				0.05831799					

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
17	3	1	-0.603668	-0.326486	17	9	1	-0.052096	-0.100271
		2	-0.557497	-0.313014			2	-0.046565	-0.102825
		3	2.161166	0.639500			3	-0.037862	-0.100587
E(LU)			1.53642388				4	-0.026851	-0.095136
E(CP)			0.60729095				5	-0.013728	-0.086910
E(LB)				0.32311812			6	0.001531	-0.075995
							7	0.019069	-0.062288
17	4	1	-0.362861	-0.242716			8	0.079129	-0.045535
		2	-0.338922	-0.236662			9	1.117373	0.669546
		3	-0.293934	-0.218114	E(LU)			0.14699387	
		4	1.996717	0.697492	E(CP)			0.05307401	
E(LU)			0.84174810		E(LB)				0.09612512
E(CP)			0.36462724						
E(LB)				0.23835098	17	10	1	-0.034167	-0.088465
							2	-0.029139	-0.091350
17	5	1	-0.236557	-0.192031			3	-0.021881	-0.090064
		2	-0.221164	-0.189778			4	-0.012965	-0.085992
		3	-0.192661	-0.177793			5	-0.002507	-0.079521
		4	-0.155037	-0.159206			6	0.009531	-0.070728
		5	1.805419	0.718809			7	0.323273	-0.059520
E(LU)			0.52028442				8	0.038922	-0.045671
E(CP)			0.23663986				9	0.056761	-0.028822
E(LB)				0.18739415			10	0.972172	0.640135
					E(LU)			0.12022174	
17	6	1	-0.160149	-0.157965	E(CP)			0.03544569	
		2	-0.149601	-0.157871	E(LB)				0.08451762
		3	-0.130090	-0.149896					
		4	-0.104290	-0.136581	17	11	1	-0.020654	-0.078673
		5	-0.072907	-0.118639			2	-0.015906	-0.081761
		6	1.617037	0.720952			3	-0.009632	-0.081188
E(LU)			0.34893506				4	-0.002186	-0.078180
E(CP)			0.16024410				5	0.006378	-0.073083
E(LB)				0.15333326			6	0.016104	-0.065964
							7	0.027102	-0.056744
17	7	1	-0.110512	-0.133428			8	0.039540	-0.045224
		2	-0.102606	-0.134640			9	0.053648	-0.031078
		3	-0.088415	-0.129294			10	0.069744	-0.013827
		4	-0.069771	-0.119517			11	0.835861	0.605723
		5	-0.047139	-0.105901	E(LU)			0.10195092	
		6	-0.020560	-0.088568	E(CP)			0.02220540	
		7	1.439003	0.711349	E(LB)				0.07492279
E(LU)			0.24902198						
E(CP)			0.11085361		17	12	1	-0.010286	-0.070375
E(LB)				0.12891783			2	-0.005683	-0.073577
							3	-0.000086	-0.073546
17	8	1	-0.076441	-0.114859			4	0.006316	-0.071375
		2	-0.070039	-0.116891			5	0.013511	-0.067372
		3	-0.059173	-0.113357			6	0.021553	-0.061602
		4	-0.045110	-0.106076			7	0.030535	-0.053996
		5	-0.028154	-0.095554			8	0.140597	-0.044377
		6	-0.008307	-0.081890			9	0.051928	-0.032455
		7	0.014595	-0.064968			10	0.064785	-0.017797
		8	1.272528	0.693595			11	0.079517	0.000228
E(LU)			0.18708688				12	0.707314	0.566244
E(CP)			0.07709833		E(LU)			0.08930564	
E(LB)				0.11052085	E(CP)			0.01208216	
					E(LB)				0.06681358

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
17	13	1	-0.002231	-0.063202	17	16	1	0.012379	-0.045870
		2	0.002318	-0.066454			2	0.017617	-0.049609
		3	0.007448	-0.066839			3	0.022076	-0.050145
		4	0.013101	-0.065335			4	0.026538	-0.049982
		5	0.019298	-0.062220			5	0.031091	-0.048727
		6	0.026098	-0.057556			6	0.035799	-0.046430
		7	0.033584	-0.051282			7	0.040724	-0.043057
		8	0.041872	-0.043242			8	0.045932	-0.038508
		9	0.051113	-0.033181			9	0.051504	-0.032609
		10	0.061516	-0.020708			10	0.057542	-0.025690
		11	0.073364	-0.005250			11	0.064186	-0.015545
		12	0.087058	0.014056			12	0.071635	-0.003341
		13	0.585461	0.521211			13	0.080193	0.012556
E(LU)			0.08049558				14	0.090373	0.033974
E(CP)			0.00423893				15	0.103110	0.064588
E(LB)			0.05983608				16	0.248699	0.337194
								0.06738336	
17	14	1	0.004088	-0.056878				-0.01047916	
		2	0.008636	-0.060131				0.04307100	
		3	0.013446	-0.060836					
		4	0.018560	-0.059871					
		5	0.024028	-0.057487					
		6	0.029909	-0.053742					
		7	0.036278	-0.048586					
		8	0.043231	-0.041881					
		9	0.050892	-0.033402					
		10	0.059426	-0.022749					
		11	0.069060	-0.009558					
		12	0.080119	0.007112					
		13	0.093083	0.028459					
		14	0.469244	0.569601					
E(LU)			0.07436842						
E(CP)			-0.00189289						
E(LB)			0.05369960						
17	15	1	0.009066	-0.051176					
		2	0.013648	-0.054390					
		3	0.018244	-0.055341					
		4	0.022974	-0.054815					
		5	0.027908	-0.053042					
		6	0.033111	-0.050075					
		7	0.038648	-0.045871					
		8	0.044600	-0.040314					
		9	0.051065	-0.033203					
		10	0.058176	-0.024231					
		11	0.066111	-0.012936					
		12	0.075128	0.001394					
		13	0.085616	0.019905					
		14	0.098200	0.044587					
		15	0.357566	0.409507					
E(LU)			0.07016498						
E(CP)			-0.00670775						
E(LB)			0.04818440						
17	16	1	0.012379	-0.045870					
		2	0.017617	-0.049609					
		3	0.022076	-0.050145					
		4	0.026538	-0.049982					
		5	0.031091	-0.048727					
		6	0.035799	-0.046430					
		7	0.040724	-0.043057					
		8	0.045932	-0.038508					
		9	0.051504	-0.032609					
		10	0.057542	-0.025690					
		11	0.064186	-0.015545					
		12	0.071635	-0.003341					
		13	0.080193	0.012556					
		14	0.090373	0.033974					
		15	0.103110	0.064588					
		16	0.248699	0.337194					
E(LU)			0.06738336						
E(CP)			-0.01047916						
E(LB)			0.04307100						
17	17	1	0.015998	-0.040607					
		2	0.020706	-0.043624					
		3	0.025089	-0.044891					
		4	0.029378	-0.045031					
		5	0.033671	-0.044229					
		6	0.038035	-0.042531					
		7	0.042527	-0.039913					
		8	0.047204	-0.036289					
		9	0.052133	-0.031512					
		10	0.057392	-0.025352					
		11	0.063089	-0.017458					
		12	0.069375	-0.007282					
		13	0.076482	0.006082					
		14	0.084803	0.024262					
		15	0.095098	0.050618					
		16	0.109270	0.094076					
		17	0.139752	0.243681					
E(LU)			0.06572241						
E(CP)			-0.01337530						
E(LB)			0.03802109						
18	2	1	-1.195128	-0.492912					
		2	2.195128	0.492912					
			3.61129585						
			1.20912723						
			0.49286703						
E(LU)									
E(CP)									
E(LB)									
18	3	1	-0.624252	-0.326884					
		2	-0.580008	-0.314183					
		3	2.204260	0.641066					
			1.61137253						
			0.62748837						
			0.32370865						
E(LU)									
E(CP)									
E(LB)									
18	4	1	-0.379529	-0.243153					
		2	-0.355679	-0.237429					
		3	-0.312382	-0.215992					
		4	2.047590	0.700574					
			0.88805128						
			0.38000703						
			0.23903395						
E(LU)									
E(CP)									
E(LB)									

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)		
18	5	1	-0.249266	-0.192523	18	10	1	-0.040776	-0.089291		
		2	-0.234618	-0.190376			2	-0.036223	-0.091997		
		3	-0.207148	-0.179091			3	-0.029314	-0.090739		
		4	-0.170883	-0.161679			4	-0.020701	-0.086863		
		5	1.861914	0.723670			5	-0.010540	-0.080764		
E(LU)			0.55118001				6	0.001172	-0.072544		
E(CP)				0.24907530			7	0.014523	-0.062157		
E(LB)				0.18814472			8	0.029671	-0.049465		
	16	6	1	-0.170868	-0.158518			9	0.046841	-0.034147	
		2	-0.160910	-0.158405	E(LU)			10	1.045347	0.657947	
		3	-0.142100	-0.150876	E(CP)				0.12567798		
		4	-0.117175	-0.138383	E(LB)				0.04172006		
		5	-0.086906	-0.121647					0.08554362		
		6	1.677960	0.727829		18	11	1	-0.026669	-0.079582	
E(LU)			C.37044855				2	-0.022402	-0.082484		
E(CP)				0.17068152			3	-0.016466	-0.081896		
E(LB)				0.15414076			4	-0.009294	-0.079012		
	18	7	1	-0.119793	-0.134044			5	-0.000979	-0.074183	
		2	-0.112406	-0.135163			6	0.008496	-0.067503		
		3	-0.098738	-0.130098			7	0.019212	-0.058930		
		4	-0.080698	-0.120904			8	0.031300	-0.048324		
		5	-0.058807	-0.108183			9	0.044947	-0.035451		
		6	-0.033165	-0.092095			10	0.060404	-0.019962		
		7	1.503605	0.720486			11	0.911469	0.627325		
E(LU)			0.26434202		E(LU)			0.10556433			
E(CP)				0.11983020	E(CP)			0.02787638			
E(LB)				0.12977806	E(LB)				0.07601539		
	18	8	1	-0.084626	-0.115541		18	12	1	-0.015793	-0.071378
		2	-0.078711	-0.117434				2	-0.011677	-0.074393	
		3	-0.062272	-0.114068				3	-0.006416	-0.074315	
		4	-0.054656	-0.107202				4	-0.000278	-0.072211	
		5	-0.038217	-0.097349				5	0.006695	-0.068395	
		6	-0.019006	-0.084645				6	0.014529	-0.062952	
		7	0.003084	-0.069031				7	0.023297	-0.055848	
		8	1.340405	0.705270				8	0.033110	-0.046959	
E(LU)			0.19807869					9	0.044122	-0.036073	
E(CP)				0.08497296				10	0.056540	-0.022877	
E(LB)				0.11143310				11	0.070637	-0.006924	
	18	9	1	-0.059414	-0.101022			12	0.785235	0.592326	
		2	-0.054359	-0.103411	E(LU)			0.09145851			
		3	-0.046030	-0.101260	E(CP)			0.01723593			
		4	-0.035375	-0.096099	E(LB)				0.06798859		
		5	-0.022631	-0.088374		18	13	1	-0.007289	-0.064317	
		6	-0.007819	-0.078203				2	-0.003236	-0.067387	
		7	0.009161	-0.065532				3	0.001550	-0.067701	
		8	0.028495	-0.050186				4	0.006940	-0.066218	
		9	1.187973	0.684067				5	0.012925	-0.063222	
E(LU)			0.15482946					6	0.019540	-0.058792	
E(CP)				0.06006815				7	0.026851	-0.052898	
E(LB)				0.09709201				8	0.034957	-0.045430	
								9	0.043969	-0.036200	
								10	0.054072	-0.024926	
								11	0.065486	-0.011201	
								12	0.070516	0.005561	
								13	0.665728	0.552731	
									0.05146655		
									0.00893995		
									0.06110111		

TABLE OF WEIGHTS (CONTINUED)

[illegible]

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
19	5	1	-0.261237	-0.192958	19	10	1	-0.047007	-0.09C004
		2	-0.247259	-0.190909			2	-0.042865	-0.092551
		3	-0.220739	-0.180245			3	-0.036265	-0.091324
		4	-0.185724	-0.163869			4	-0.027929	-0.087629
		5	1.914959	0.727980			5	-0.018045	-0.081863
E(LU)			0.58171310				6	-0.006641	-0.074147
E(CP)			0.26081700				7	0.006343	-0.064468
E(LB)			0.18881359				8	0.021029	-0.052718
							9	0.037595	-0.038703
19	6	1	-0.180964	-0.159004			10	1.117786	0.673407
		2	-0.171530	-0.158877	E(LU)			0.13159684	
		3	-0.153365	-0.151748	E(CP)			0.04766707	
		4	-0.129250	-0.139981	E(LB)			0.08643819	
		5	-0.100003	-0.124297					
		6	1.735111	0.733908	19	11	1	-0.032345	-0.08C360
E(LU)			0.39192137				2	-0.028492	-0.083057
E(CP)			0.18053993				3	-0.022852	-0.082502
E(LB)			0.15435543				4	-0.015928	-0.079736
							5	-0.007843	-0.075152
19	7	1	-0.128533	-0.134583			6	0.001395	-0.068861
		2	-0.121602	-0.135622			7	0.011842	-0.060851
		3	-0.108414	-0.130811			8	0.023603	-0.051025
		4	-0.090935	-0.122136			9	0.036827	-0.039209
		5	-0.069730	-0.110197			10	0.051716	-0.025147
		6	-0.044949	-0.095185			11	0.982076	0.645940
		7	1.564162	0.728535	E(LU)			0.10969257	
E(LU)			0.27982455		E(CP)			0.03326000	
E(CP)			0.12832890		E(LB)			0.07696225	
E(LB)			0.13053726						
					19	12	1	-0.020995	-0.072230
19	8	1	-0.092336	-0.116135			2	-0.017298	-0.075078
		2	-0.086846	-0.117908			3	-0.012331	-0.074965
		3	-0.076795	-0.114696			4	-0.006425	-0.072929
		4	-0.063593	-0.108201			5	0.000344	-0.069228
		5	-0.047637	-0.098937			6	0.007984	-0.064141
		6	-0.029016	-0.087065			7	0.016548	-0.057480
		7	-0.007670	-0.072570			8	0.026124	-0.049218
		8	1.403893	0.715513			9	0.036839	-0.039200
E(LU)			0.20936888				10	0.048859	-0.027194
E(CP)			0.09242024				11	0.062404	-0.012872
E(LB)			0.11223593				12	0.857947	0.614595
								0.09416748	
19	9	1	-0.066309	-0.101674	E(LU)			0.02213853	
		2	-0.061667	-0.103918	E(CP)			0.06899532	
		3	-0.053675	-0.101850	E(LB)				
		4	-0.043347	-0.096952					
		5	-0.030960	-0.089671	19	13	1	-0.012077	-0.065253
		6	-0.016565	-0.080147			2	-0.008453	-0.068158
		7	-0.000103	-0.068365			3	-0.003960	-0.068416
		8	0.018570	-0.054204			4	0.001201	-0.066962
		9	1.254056	0.696782			5	0.006996	-0.064084
E(LU)			0.16305851				6	0.013442	-0.059872
E(CP)			0.06668914				7	0.020588	-0.054320
E(LB)			0.09793914				8	0.028511	-0.047351
							9	0.037316	-0.038827
							10	0.047141	-0.028538
							11	0.058169	-0.016185
							12	0.070640	-0.001353
							13	0.740487	0.579318
					E(LU)			0.08302831	
					E(CP)			0.01342381	
					E(LB)			0.06217738	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
19	14	1	-0.004989	-0.059169	19	17	1	0.008968	-0.044464
		2	-0.001384	-0.062091			2	0.012677	-0.047270
		3	0.002773	-0.062636			3	0.016326	-0.048344
		4	0.007387	-0.061652			4	0.020023	-0.048319
		5	0.012453	-0.059399			5	0.023825	-0.047390
		6	0.017997	-0.055961			6	0.027772	-0.045626
		7	0.024066	-0.051334			7	0.031706	-0.043028
		8	0.030726	-0.045450			8	0.036272	-0.039552
		9	0.038064	-0.038185			9	0.040920	-0.035112
		10	0.046194	-0.029351			10	0.045913	-0.029573
		11	0.055267	-0.018676			11	0.051331	-0.022740
		12	0.065482	-0.005781			12	0.057280	-0.014330
		13	0.077109	0.009882			13	0.063906	-0.003928
		14	0.628854	0.539802			14	0.071419	0.009098
E(LU)			C.07498023				15	0.080136	0.025759
E(CP)			0.00651543				16	0.090563	0.047806
E(LB)			0.05624730				17	0.320763	0.387016
					E(LU)		0.06200679		
					E(CP)		-0.00702291		
					E(LB)		0.04198714		
19	15	1	0.000692	-0.053779	19	18	1	0.011941	-0.040244
		2	0.004313	-0.056686			2	0.015709	-0.042966
		3	0.008234	-0.057456			3	0.019289	-0.044136
		4	0.012444	-0.056855			4	0.022835	-0.044327
		5	0.016963	-0.055121			5	0.026412	-0.043716
		6	0.021823	-0.052332			6	0.030068	-0.042366
		7	0.027068	-0.048486			7	0.033841	-0.040281
		8	0.032757	-0.043523			8	0.037772	-0.037423
		9	0.038961	-0.037334			9	0.041903	-0.033716
		10	0.045774	-0.029749			10	0.046286	-0.029044
		11	0.053320	-0.020523			11	0.050984	-0.023232
		12	0.061762	-0.009310			12	0.055083	-0.016030
		13	0.071323	0.004394			13	0.061695	-0.007067
		14	0.082316	0.021334			14	0.067989	0.004227
		15	0.522250	0.495426			15	0.075216	0.018774
E(LU)			0.06915784				16	0.083802	0.039205
E(CP)			0.00099208				17	0.094526	0.065788
E(LB)			0.05100764				18	0.223648	0.317554
					E(LU)		0.05998848		
					E(CP)		-0.00988868		
					E(LB)		0.03791809		
19	16	1	0.005271	-0.043924					
		2	0.008929	-0.051792					
		3	0.012687	-0.052735					
		4	0.016601	-0.052449					
		5	0.020708	-0.051151					
		6	0.025048	-0.048913					
		7	0.029663	-0.045735					
		8	0.034603	-0.041566					
		9	0.039929	-0.036308					
		10	0.045717	-0.029809					
		11	0.052068	-0.021870					
		12	0.059114	-0.012118					
		13	0.067036	-0.000151					
		14	0.076094	0.014738					
		15	0.086669	0.033642					
		16	0.419861	0.445119					
E(LU)			0.06496979						
E(CP)			-0.00344791						
E(LB)			0.04630055						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
19	19	1	0.014282	-0.035995	20	7	1	-0.136790	-0.135060
		2	0.018115	-0.038600			2	-0.130264	-0.136029
		3	0.021661	-0.039833			3	-0.117518	-0.131448
		4	0.025107	-0.040204			4	-0.100561	-0.123220
		5	0.028531	-0.039873			5	-0.079995	-0.111990
		6	0.031980	-0.038897			6	-0.056007	-0.097918
		7	0.035494	-0.037282			7	1.621135	0.735661
		8	0.039109	-0.034997	E(LU)			0.29539488	
		9	0.042861	-0.031977	E(CP)			0.13637533	
		10	0.046794	-0.028121	E(LB)			0.13121241	
		11	0.050958	-0.023280					
		12	0.055419	-0.017234	20	8	1	-0.099621	-0.116659
		13	0.060267	-0.009660			2	-0.094504	-0.118326
		14	0.065629	-0.000055			3	-0.084808	-0.115255
		15	0.071704	-0.012400			4	-0.071993	-0.109093
		16	0.078826	0.079177			5	-0.056488	-0.103352
		17	0.087648	0.053305			6	-0.038416	-0.089210
		18	0.099799	0.092832			7	-0.017755	-0.075681
		19	0.125817	0.228292			8	1.463535	0.724575
E(LU)			0.05874886		E(LU)			0.22087332	
E(CP)			-0.01213794		E(CP)			0.09948206	
E(LB)			0.03383684		E(LB)			0.11294771	
20	2	1	-1.251068	-0.493634	20	9	1	-0.072826	-0.102246
		2	2.251068	0.493634			2	-0.068544	-0.104362
E(LU)			3.88005370				3	-0.060858	-0.102371
E(CP)			1.26365389				4	-0.050834	-0.097711
E(LB)			0.49359782				5	-0.038781	-0.090828
20	3	1	-0.662014	-0.327555			6	-0.024779	-0.081874
		2	-0.621129	-0.316157			7	-0.008798	-0.070863
		3	2.283144	0.643713			8	0.009270	-0.057714
E(LU)			1.75538518		E(LU)			0.17159045	
E(CP)			0.66462201		E(CP)			0.07297238	
E(LB)			0.32470597		E(LB)			0.09868793	
20	4	1	-0.408252	-0.243885	20	10	1	-0.052900	-0.090626
		2	-0.386289	-0.238726			2	-0.049115	-0.093031
		3	-0.345972	-0.223154			3	-0.042792	-0.091837
		4	2.140513	0.705766			4	-0.034710	-0.088309
E(LU)			0.97791855				5	-0.025087	-0.082842
E(CP)			0.40827717				6	-0.013973	-0.075573
E(LB)			0.24018443				7	-0.001335	-0.066511
20	5	1	-0.272551	-0.193344			8	0.012921	-0.055584
		2	-0.259179	-0.191385			9	0.028939	-0.042651
		3	-0.233536	-0.181278			10	1.178052	0.686964
		4	-0.199675	-0.165821	E(LU)			0.13788300	
		5	1.964941	0.731828	E(CP)			0.05331635	
E(LU)			0.61184794		E(LB)			0.08722579	
E(CP)			0.27193675		20	11	1	-0.037716	-0.081036
E(LB)			0.18940540				2	-0.034222	-0.083625
20	6	1	-0.190502	-0.159435			3	-0.028845	-0.083028
		2	-0.181539	-0.159298			4	-0.022146	-0.080373
		3	-0.163969	-0.152528			5	-0.014276	-0.076014
		4	-0.140605	-0.141408			6	-0.005262	-0.070070
		5	-0.112303	-0.126651			7	0.004930	-0.062554
		6	1.788917	0.739321			8	0.016382	-0.053398
E(LU)			0.41329354				9	0.029216	-0.042476
E(CP)			0.18987852				10	0.043593	-0.029594
E(LB)			0.15549251		E(LU)			1.048347	0.662168
					E(CP)			0.11423656	
					E(LB)			0.03838053	
								0.07779186	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
20	12	1	-0.025922	-0.072964	20	15	1	-0.003203	-0.054744
		2	-0.022589	-0.075662			2	0.000035	-0.057513
		3	-0.017879	-0.075522			3	0.003690	-0.058213
		4	-0.012183	-0.073554			4	0.007695	-0.057596
		5	-0.005600	-0.070076			5	0.012048	-0.055899
		6	0.001858	-0.065197			6	0.016769	-0.053209
		7	0.010227	-0.058928			7	0.021892	-0.049537
		8	0.019578	-0.051211			8	0.027467	-0.044842
		9	0.030012	-0.041931			9	0.033552	-0.039043
		10	0.041668	-0.030912			10	0.040230	-0.032010
		11	0.054724	-0.017911			11	0.047602	-0.023560
		12	0.026107	0.633868			12	0.055904	-0.013436
E(LU)			0.09732994				13	0.065012	-0.001280
E(CP)			0.02680890				14	0.075467	0.013416
E(LB)				0.06987174			15	0.595940	0.527466
					E(LU)			0.06951916	
					E(CP)			0.00461910	
					E(LB)			0.05207861	
20	13	1	-0.016619	-0.066052	20	16	1	0.001656	-0.050002
		2	-0.013364	-0.068809			2	0.004926	-0.052742
		3	-0.009129	-0.069021			3	0.008410	-0.053608
		4	-0.004170	-0.067601			4	0.012111	-0.053287
		5	0.001453	-0.064835			5	0.016048	-0.051997
		6	0.007742	-0.060825			6	0.020247	-0.049816
		7	0.014732	-0.055581			7	0.024742	-0.046757
		8	0.022485	-0.049051			8	0.029575	-0.042785
		9	0.031087	-0.041132			9	0.034801	-0.037825
		10	0.040654	-0.031666			10	0.040482	-0.031763
		11	0.051333	-0.020429			11	0.046707	-0.024422
		12	0.063321	-0.007116			12	0.053585	-0.015601
		13	0.810474	0.602120			13	0.061262	-0.004939
E(LU)			0.08507430				14	0.069938	0.008023
E(CP)			0.01779390				15	0.079893	0.023984
E(LB)				0.06310742			16	0.495616	0.483548
					E(LU)			0.06467887	
					E(CP)			-0.00010333	
					E(LB)			0.04747110	
20	14	1	-0.009191	-0.060043	20	17	1	0.005617	-0.045695
		2	-0.005961	-0.062821			2	0.008931	-0.048385
		3	-0.002065	-0.063307			3	0.012297	-0.049380
		4	0.002348	-0.062329			4	0.015773	-0.049304
		5	0.007248	-0.060148			5	0.019394	-0.048357
		6	0.012649	-0.056856			6	0.023192	-0.046613
		7	0.018585	-0.052465			7	0.027201	-0.044083
		8	0.025109	-0.046929			8	0.031459	-0.040736
		9	0.032297	-0.040154			9	0.036010	-0.036510
		10	0.040241	-0.031999			10	0.040910	-0.031298
		11	0.049069	-0.022261			11	0.046228	-0.024954
		12	0.058941	-0.010659			12	0.052055	-0.017265
		13	0.070069	0.003196			13	0.058509	-0.007934
		14	0.700660	0.566775			14	0.065756	0.003474
E(LU)			0.07610847				15	0.074029	0.017606
E(CP)			0.01045130				16	0.083671	0.035466
E(LB)				0.05724068			17	0.398968	0.433947
					E(LU)			0.06114864	
					E(CP)			-0.00394307	
					E(LB)			0.04329477	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
20	18	1	0.008847	-0.041706	20	20	1	0.013553	-0.034055
		2	0.012215	-0.044331			2	0.017039	-0.036484
		3	0.015502	-0.045422			3	0.020257	-0.037686
		4	0.018813	-0.045550			4	0.023376	-0.038123
		5	0.022197	-0.044896			5	0.026464	-0.037945
		6	0.025690	-0.043529			6	0.029565	-0.037211
		7	0.029324	-0.041460			7	0.032711	-0.035932
		8	0.033133	-0.038646			8	0.035932	-0.034091
		9	0.037162	-0.035086			9	0.039258	-0.031646
		10	0.041450	-0.030632			10	0.042720	-0.028527
		11	0.046055	-0.025168			11	0.046357	-0.024632
		12	0.051050	-0.018506			12	0.050215	-0.019814
		13	0.056532	-0.010374			13	0.054354	-0.013860
		14	0.062634	-0.000381			14	0.058856	-0.006460
		15	0.069547	0.012071			15	0.063842	0.002864
		16	0.077558	0.027938			16	0.069496	0.014902
		17	0.087131	0.048871			17	0.076128	0.031052
		18	0.095157	0.076826			18	0.084346	0.054203
E(LU)			0.001867				19	0.095649	0.092028
E(CP)			-0.00706723				20	0.119862	0.221415
E(LB)			0.03943688		E(LU)			0.05578958	
					E(CP)			-0.01159947	
					E(LB)			0.03207039	
20	19	1	0.011469	-0.037905	21	2	1	-1.276980	-0.493942
		2	0.014895	-0.040446			2	2.276880	0.493942
		3	0.018135	-0.041607				4.00827646	
		4	0.021329	-0.041903				1.28886132	
		5	0.024538	-0.041503				0.49390979	
		6	0.027802	-0.040467					
		7	0.031153	-0.038810	21	3	1	-0.679427	-0.327841
		8	0.034624	-0.036509			2	-0.670016	-0.316999
		9	0.038247	-0.033514			3	2.319443	0.644841
		10	0.042061	-0.029746				1.82463798	
		11	0.046112	-0.025085				0.68177635	
		12	0.050458	-0.019364				0.32513088	
		13	0.055176	-0.012340					
		14	0.060372	-0.002540	21	4	1	-0.421487	-0.244196
		15	0.066198	0.007217			2	-0.400349	-0.239279
		16	0.072887	0.021167			3	-0.361352	-0.224498
		17	0.080830	0.039737			4	2.183188	0.707973
		18	0.090746	0.066024				1.02150585	
		19	0.212971	0.308714				0.42133361	
E(LU)			0.05687410					0.24067351	
E(CP)			-0.00959610		E(LU)				
E(LB)			0.03577112		E(CP)				
					E(LB)				
					21	5	1	-0.283275	-0.193691
							2	-0.270454	-0.191814
							3	-0.245624	-0.182209
							4	-0.212831	-0.167572
							5	2.012185	0.735285
								0.64156176	
								0.28249590	
								0.18993997	
					21	6	1	-0.199541	-0.159820
							2	-0.191002	-0.159675
							3	-0.173984	-0.153231
							4	-0.151319	-0.142690
							5	-0.123892	-0.128756
							6	1.839738	0.744172
								0.43452074	
								0.19874861	
								0.15606403	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
21	7	1	-0.144615	-0.135485	21	12	1	-0.030601	-0.073604	
		2	-0.138450	-0.136392			2	-0.027584	-0.076167	
		3	-0.126112	-0.132021			3	-0.023103	-0.076006	
		4	-0.109643	-0.124225			4	-0.017596	-0.074104	
		5	-0.089672	-0.113595			5	-0.011187	-0.070777	
		6	-0.066419	-0.100351			6	-0.003901	-0.066142	
		7	1.674911	0.742070			7	0.004282	-0.060223	
E(LU)			0.31099565				8	0.013418	-0.052983	
E(CP)			0.14402019				9	0.023589	-0.044337	
E(LB)			0.13181685				10	0.034909	-0.034153	
	21	8	1	-0.106524	-0.117124			11	0.047525	-0.022243
		2	-0.101739	-0.118696			12	0.990248	0.650734	
		3	-0.092368	-0.115755	E(LU)			0.10086432		
		4	-0.079914	-0.109895	E(CP)			0.03126495		
		5	-0.064832	-0.101621	E(LB)			0.07064304		
		6	-0.047274	-0.091123		21	13	1	-0.020936	-0.066744
		7	-0.027245	-0.078439			2	-0.018002	-0.069367	
		8	1.519896	0.731652			3	-0.013994	-0.069541	
E(LU)			0.23252621				4	-0.009216	-0.068156	
E(CP)			0.10619473				5	-0.003750	-0.065499	
E(LB)			0.11358345				6	0.002392	-0.061675	
	21	9	1	-0.079003	-0.102752			7	0.009234	-0.056708
		2	-0.075039	-0.104752			8	0.016823	-0.056566	
		3	-0.067630	-0.102836			9	0.025231	-0.043172	
		4	-0.057890	-0.098393			10	0.034555	-0.034404	
		5	-0.046151	-0.091865			11	0.044917	-0.024094	
		6	-0.032519	-0.083417			12	0.056476	-0.012009	
		7	-0.016987	-0.073081			13	0.876270	0.621934	
		8	0.000523	-0.060807	E(LU)			0.08752028		
		9	1.374696	0.717905	E(CP)			0.02179399		
E(LU)			0.18035373		E(LB)			0.063921C0		
E(CP)			0.07894880			21	14	1	-0.013190	-0.060794
E(LB)			0.09935486				2	-0.010287	-0.063440	
	21	10	1	-0.058485	-0.091174			3	-0.005618	-0.063875
		2	-0.055015	-0.093453			4	-0.002385	-0.062909	
		3	-0.048942	-0.092291			5	0.002367	-0.060800	
		4	-0.041036	-0.088916			6	0.007636	-0.057647	
		5	-0.031718	-0.083721			7	0.013446	-0.053473	
		6	-0.020880	-0.076849			8	0.019842	-0.048247	
		7	-0.006567	-0.068330			9	0.026883	-0.041903	
		8	0.005230	-0.058118			10	0.034651	-0.034330	
		9	0.020804	-0.046107			11	0.043251	-0.025373	
		10	1.238610	0.698958			12	0.052814	-0.014822	
E(LU)			0.14446082				13	0.063513	-0.002388	
E(CP)			0.05869415				14	0.768077	0.590001	
E(LB)			0.08792500		E(LU)			0.07766021		
	21	11	1	-0.042812	-0.081628	E(CP)		0.01421994		
		2	-0.039631	-0.084084	E(LB)			0.05810297		
		3	-0.034490	-0.083419						
		4	-0.027998	-0.080939						
		5	-0.020328	-0.076784						
		6	-0.011527	-0.071153						
		7	-0.001577	-0.064073						
		8	0.009585	-0.055502						
		9	0.022055	-0.045346						
		10	0.035968	-0.033457						
		11	1.110755	0.676455						
E(LU)			0.11911746							
E(CP)			0.04325992							
E(LB)			0.07852549							

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
21	15	1	-0.006919	-0.055563	21	18	1	0.005853	-0.042848
		2	-0.004012	-0.058205			2	0.000874	-0.045374
		3	-0.000589	-0.058845			3	0.011911	-0.046394
		4	0.003237	-0.058219			4	0.015024	-0.046474
		5	0.007443	-0.056566			5	0.018245	-0.045796
		6	0.012039	-0.053974			6	0.021603	-0.044433
		7	0.017679	-0.050466			7	0.025124	-0.042403
		8	0.022516	-0.046017			8	0.028836	-0.0409694
		9	0.027357	-0.040565			9	0.032780	-0.036255
		10	0.032195	-0.034010			10	0.036985	-0.032027
		11	0.04242	-0.026215			11	0.041512	-0.026894
		12	0.056225	-0.016982			12	0.046418	-0.020718
		13	0.059124	-0.006049			13	0.051789	-0.013292
		14	0.069130	0.006947			14	0.057729	-0.004339
		15	0.664991	0.554729			15	0.064392	0.006557
E(LU)			0.07032505				16	0.071987	0.020003
E(CP)				0.00810102			17	0.080826	0.036967
E(LB)				0.05299863			18	0.380111	0.423414
					E(LU)			0.05777143	
					E(CP)			-0.00431152	
					E(LB)			0.04064434	
21	16	1	-0.001802	-0.050903	21	19	1	0.008698	-0.039258
		2	0.001131	-0.053522			2	0.011772	-0.041717
		3	0.004378	-0.054323			3	0.014753	-0.042808
		4	0.007896	-0.053977			4	0.017739	-0.043048
		5	0.011684	-0.052704			5	0.020774	-0.042605
		6	0.015759	-0.050587			6	0.023891	-0.041546
		7	0.020147	-0.047646			7	0.027116	-0.039889
		8	0.024883	-0.043862			8	0.030478	-0.037622
		9	0.030017	-0.039172			9	0.034006	-0.034708
		10	0.035594	-0.033501			10	0.037735	-0.031080
		11	0.041700	-0.026708			11	0.041797	-0.026648
		12	0.048420	-0.018625			12	0.045971	-0.021282
		13	0.055879	-0.009004			13	0.050597	-0.014797
		14	0.064233	0.002489			14	0.055671	-0.006936
		15	0.073697	0.016331			15	0.061314	0.002673
		16	0.566382	0.515715			16	0.067704	0.014599
E(LU)			0.06485329				17	0.075101	0.029744
E(CP)				0.00311876			18	0.083931	0.049671
E(LB)				0.04846207			19	0.291040	0.367257
								0.05559063	
								-0.00706342	
								0.03717178	
21	17	1	0.002397	-0.046698					
		2	0.005370	-0.049278					
		3	0.008493	-0.050203					
		4	0.011778	-0.050089					
		5	0.015245	-0.049137					
		6	0.018916	-0.047426					
		7	0.022818	-0.044972					
		8	0.026981	-0.041760					
		9	0.031445	-0.037741					
		10	0.036263	-0.032831					
		11	0.041487	-0.026922					
		12	0.047201	-0.019846					
		13	0.053501	-0.011386					
		14	0.060520	-0.001230					
		15	0.068439	0.011065					
		16	0.077509	0.026154					
		17	0.471636	0.472299					
E(LU)			0.06077952						
E(CP)				-0.00096075					
E(LB)				0.04437683					

[illegible]

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
21	20	1	0.011028	-0.035816	22	4	1	-0.434070	-0.244476	
		2	0.014157	-0.038193			2	-0.413490	-0.239780	
		3	0.017105	-0.039333			3	-0.375918	-0.225713	
		4	0.020000	-0.039706			4	2.223678	-0.709969	
		5	0.022898	-0.039466	E(LU)			1.06422125		
		6	0.025833	-0.038674	E(CP)			0.43276212		
		7	0.028833	-0.037352	E(LB)			0.24111609		
		8	0.031923	-0.035486		22	5	1	-0.293467	-0.194003
		9	0.035133	-0.033042			2	-0.281150	-0.192202	
		10	0.038489	-0.029966			3	-0.257076	-0.183051	
		11	0.042026	-0.026176			4	-0.225276	-0.169152	
		12	0.045787	-0.021555			5	2.056969	0.738407	
		13	0.049824	-0.015938	E(LU)			0.67084108		
		14	0.054209	-0.009097	E(CP)			0.29254724		
		15	0.059038	-0.000691	E(LB)			0.19042304		
		16	0.064453	0.009794		22	6	1	-0.208130	-0.160166
		17	0.070670	0.023194			2	-0.199975	-0.160015	
		18	0.078048	0.040976			3	-0.183470	-0.153867	
		19	0.087254	0.066087			4	-0.161458	-0.143848	
		20	0.203293	0.300441			5	-0.134845	-0.130649	
E(LU)			0.05407008				6	1.887878	0.748545	
E(CP)			-0.00931060		E(LU)			0.45557033		
E(LB)			0.03385072		E(CP)			0.20719220		
	21	1	0.012894	-0.032310	E(LB)			0.15657969		
		2	0.016080	-0.034581		22	7	1	-0.152049	-0.135866
		3	0.019015	-0.035746			2	-0.146209	-0.136718	
		4	0.021851	-0.036228			3	-0.134250	-0.132539	
		5	0.024653	-0.036168			4	-0.118236	-0.125119	
		6	0.027458	-0.035622			5	-0.098823	-0.115041	
		7	0.030295	-0.034606			6	-0.076253	-0.102533	
		8	0.033186	-0.033114			7	1.725817	0.747815	
		9	0.036159	-0.031116	E(LU)			0.32658258		
		10	0.039235	-0.028564	E(CP)			0.15130047		
		11	0.042446	-0.025388	E(LB)			0.13236123		
		12	0.045824	-0.021484		22	8	1	-0.113082	-0.117539
		13	0.049414	-0.016709			2	-0.108593	-0.119026	
		14	0.053270	-0.010860			3	-0.099523	-0.116206	
		15	0.057470	-0.003637			4	-0.087407	-0.110619	
		16	0.062124	0.005419			5	-0.072723	-0.102765	
		17	0.067404	0.017050			6	-0.055645	-0.092840	
		18	0.073603	0.032626			7	-0.036204	-0.080900	
		19	0.081287	0.054878			8	1.513176	0.739897	
		20	0.091876	0.091146	E(LU)			0.24427569		
		21	0.114456	0.215004	E(CP)			0.11258985		
E(LU)			0.05311439		E(LB)			0.11415483		
E(CP)			-0.01110585			22	9	1	-0.084872	-0.103202
E(LB)			0.03047836				2	-0.081190	-0.105100	
	22	2	-1.301440	-0.494222			3	-0.074136	-0.103253	
E(LU)			2.301440	0.494222			4	-0.064360	-0.099008	
E(CP)			4.13275081				5	-0.053119	-0.092802	
E(LB)			1.31287156				6	-0.039835	-0.084805	
			0.49419277				7	-0.024723	-0.075066	
	22	3	-0.695987	-0.328100			8	-0.007729	-0.063556	
		2	-0.657136	-0.317763			9	1.430063	0.726792	
		3	2.352223	0.645863	E(LU)			0.18129138		
E(LU)			1.89217469		E(CP)			0.08464553		
E(CP)			0.69810867		E(LB)			0.09995287		
E(LB)			0.32551588							

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
22	10	1	-0.063797	-0.091660	22	14	1	-0.017003	-0.061447
		2	-0.060601	-0.093825			2	-0.014385	-0.063972
		3	-0.054757	-0.092695			3	-0.010918	-0.064365
		4	-0.047129	-0.089463			4	-0.006845	-0.063413
		5	-0.037983	-0.084513			5	-0.002229	-0.061375
		6	-0.027405	-0.077998			6	0.002917	-0.058353
		7	-0.015399	-0.069960			7	0.008610	-0.054576
		8	-0.001917	-0.060373			8	0.014879	-0.049432
		9	0.013133	-0.049161			9	0.021782	-0.043466
		10	1.295854	0.709648			10	0.029381	-0.036397
E(LU)			0.15126968				11	0.037767	-0.028103
E(CP)			0.06382371				12	0.047049	-0.018422
E(LB)			0.08855022				13	0.057369	-0.007137
							14	0.831624	0.610259
								0.07956563	
22	11	1	-0.047658	-0.082152	E(LU)			0.01783144	
		2	-0.044752	-0.084487	E(CP)			0.05886035	
		3	-0.039824	-0.083898	E(LB)				
		4	-0.033522	-0.081446					
		5	-0.026041	-0.077478	22	15	1	-0.010467	-0.056269
		6	-0.017442	-0.072129			2	-0.007849	-0.058795
		7	-0.007722	-0.065437			3	-0.004630	-0.059383
		8	0.003165	-0.057379			4	-0.000964	-0.058755
		9	0.015297	-0.047887			5	0.003111	-0.057145
		10	0.028784	-0.036846			6	0.007593	-0.054649
		11	1.169717	0.689139			7	0.012499	-0.051296
E(LU)			0.12427189				8	0.017862	-0.047069
E(CP)			0.04791797				9	0.023724	-0.041928
E(LB)			0.07917935				10	0.030145	-0.035792
							11	0.037196	-0.028555
22	12	1	-0.035052	-0.074167			12	0.044975	-0.020066
		2	-0.032313	-0.076608			13	0.053597	-0.010126
		3	-0.028036	-0.076431			14	0.063218	0.001536
		4	-0.022704	-0.074593			15	0.729991	0.578292
		5	-0.016456	-0.071406	E(LU)			0.07150301	
		6	-0.009333	-0.066992	E(CP)			0.01144432	
		7	-0.001327	-0.061386	E(LB)			0.05380054	
		8	0.007603	-0.054568					
		9	0.017525	-0.046475	22	16	1	-0.005110	-0.051672
		10	0.028533	-0.037005			2	-0.002471	-0.054179
		11	0.040749	-0.026013			3	0.000569	-0.054921
		12	1.050810	0.665643			4	0.003924	-0.054559
E(LU)			0.10470500				5	0.007582	-0.053308
E(CP)			0.03552320				6	0.011543	-0.051259
E(LB)			0.07132781				7	0.015838	-0.048429
							8	0.020484	-0.044819
22	13	1	-0.025047	-0.067350			9	0.025520	-0.040385
		2	-0.022395	-0.069850			10	0.031004	-0.035054
		3	-0.018588	-0.069993			11	0.036998	-0.028725
		4	-0.013974	-0.068645			12	0.043567	-0.021274
		5	-0.008653	-0.065089			13	0.050828	-0.012503
		6	-0.002649	-0.062438			14	0.058901	-0.002170
		7	0.004050	-0.057127			15	0.067958	0.010067
		8	0.011483	-0.051924			16	0.832864	0.553188
		9	0.019706	-0.044989	E(LU)			0.06541674	
		10	0.028801	-0.036822	E(CP)			0.00622046	
		11	0.038870	-0.027293	E(LB)			0.04931689	
		12	0.050045	-0.016224					
		13	0.938350	0.639340					
E(LU)			0.09029856						
E(CP)			0.02570744						
E(LB)			0.06463988						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
22	17	1	-0.000692	-0.047541	22	19	1	0.006009	-0.040322
		2	0.001982	-0.050015			2	0.008777	-0.042695
		3	0.004893	-0.050970			3	0.011534	-0.043723
		4	0.008014	-0.050736			4	0.014342	-0.043917
		5	0.011345	-0.049789			5	0.017230	-0.043447
		6	0.014906	-0.048115			6	0.020225	-0.042380
		7	0.018711	-0.045743			7	0.023341	-0.040750
		8	0.022792	-0.042661			8	0.026624	-0.038526
		9	0.027167	-0.038846			9	0.030059	-0.035724
		10	0.031923	-0.034195			10	0.033736	-0.032232
		11	0.037042	-0.028684			11	0.037624	-0.028048
		12	0.042658	-0.022124			12	0.041834	-0.023001
		13	0.048810	-0.014389			13	0.046370	-0.017006
		14	0.055631	-0.005227			14	0.051344	-0.009632
		15	0.063253	0.005668			15	0.056833	-0.001233
		16	0.071871	0.018749			16	0.062987	0.009193
		17	0.083692	0.0504527			17	0.069992	0.022017
E(LU)			0.06081663				18	0.078134	0.038155
E(CP)			0.00192009				19	0.086307	0.0413471
E(LB)			0.04529672		E(LU)			0.05476281	
					E(CP)			-0.00458357	
					E(LB)			0.03829068	
22	18	1	0.002969	-0.043785	22	20	1	0.008533	-0.037073
		2	0.005687	-0.046214			2	0.011352	-0.039379
		3	0.008507	-0.047171			3	0.014069	-0.040459
		4	0.011449	-0.047212			4	0.016778	-0.040780
		5	0.014531	-0.046521			5	0.019519	-0.040500
		6	0.017772	-0.045174			6	0.022321	-0.039681
		7	0.021193	-0.043196			7	0.025204	-0.038351
		8	0.024827	-0.040573			8	0.028200	-0.036496
		9	0.028687	-0.037286			9	0.031317	-0.034104
		10	0.032827	-0.033268			10	0.034600	-0.031120
		11	0.037279	-0.028441			11	0.038064	-0.027481
		12	0.042106	-0.022691			12	0.041759	-0.023097
		13	0.047371	-0.015865			13	0.045722	-0.017840
		14	0.053169	-0.007753			14	0.050022	-0.011535
		15	0.059619	0.001940			15	0.054736	-0.003933
		16	0.066884	0.013632			16	0.059977	0.005317
		17	0.075192	0.027940			17	0.065907	0.016757
		18	0.084933	0.0461640			18	0.072766	0.031243
E(LU)			0.05735061				19	0.080947	0.050259
E(CP)			-0.00163612				20	0.088209	0.058253
E(LB)			0.04164798		E(LU)			0.05286705	
					E(CP)			-0.00702486	
					E(LB)			0.03514712	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)		N	M	I	A(N,M,I)	C(N,M,I)
22	21	1	0.010614	-0.033940		23	4	1	-0.446061	-0.244730
		2	0.013486	-0.036167				2	-0.426381	-0.240237
		3	0.016181	-0.037280				3	-0.389748	-0.226817
		4	0.018819	-0.037707				4	2.262191	0.711785
		5	0.021451	-0.037592	E(LU)				1.10608938	
		6	0.024107	-0.036993	E(CP)				0.44561957	
		7	0.026810	-0.035935	E(LB)				0.24151852	
		8	0.029588	-0.034409		23	5	1	-0.303177	-0.194285
		9	0.032449	-0.032401				2	-0.291322	-0.192554
		10	0.035435	-0.029863				3	-0.267953	-0.183817
		11	0.038552	-0.026747				4	-0.237079	-0.170584
		12	0.041849	-0.022960				5	2.099531	0.741241
		13	0.045351	-0.018398	E(LU)				0.69967926	
		14	0.049118	-0.012895	E(CP)				0.30213653	
		15	0.053206	-0.006235	E(LB)				0.19086173	
		16	0.057712	0.001909		23	6	1	-0.216311	-0.160479
		17	0.062764	0.012027				2	-0.208505	-0.160324
		18	0.068562	0.024916				3	-0.192480	-0.154445
		19	0.075443	0.041976				4	-0.171078	-0.144898
		20	0.084022	0.065013				5	-0.145224	-0.132362
		21	0.194480	0.292681				6	1.933598	0.752500
E(LU)			0.05153187		E(LU)				0.47641869	
E(CP)			-0.00903424		E(CP)				0.21524910	
E(LB)			0.03212313		E(LB)				0.15704731	
22	22	1	0.01	-0.030733		23	7	1	-0.159128	-0.136209
		2	0.01	-0.032859				2	-0.153582	-0.137013
		3	0.01	-0.033986				3	-0.141975	-0.133009
		4	0.020566	-0.034499				4	-0.126391	-0.125931
		5	0.023056	-0.034529				5	-0.107499	-0.116350
		6	0.025607	-0.034130				6	-0.085566	-0.104499
		7	0.028178	-0.033325				7	1.774142	0.753011
		8	0.030794	-0.032106	E(LU)				0.34212138	
		9	0.033464	-0.030463	E(CP)				0.15824839	
		10	0.036226	-0.028354	E(LB)				0.13285412	
		11	0.039082	-0.025735		23	8	1	-0.119329	-0.117912
		12	0.042076	-0.022528				2	-0.115104	-0.119324
		13	0.045226	-0.018638				3	-0.106313	-0.116615
		14	0.048580	-0.013922				4	-0.094514	-0.111278
		15	0.052185	-0.008184				5	-0.080205	-0.103803
		16	0.056116	-0.001137				6	-0.063578	-0.094391
		17	0.060475	0.007660				7	-0.044683	-0.083112
		18	0.065424	0.018928				8	1.623725	0.746435
		19	0.071237	0.033950	E(LU)				0.25608069	
		20	0.078445	0.055370	E(CP)				0.11869505	
		21	0.088381	0.090709	E(LB)				0.11467125	
		22	0.109526	0.209011		23	9	1	-0.090463	-0.103606
E(LU)			0.05068421					2	-0.087031	-0.105411
E(CP)			-0.01065184					3	-0.080117	-0.103629
E(LB)			0.02903621					4	-0.070117	-0.099566
23	2	1	-1.324862	-0.494478				5	-0.059713	-0.093651
		2	2.324862	0.494478				6	-0.046768	-0.088060
E(LU)			4.25371176					7	-0.032050	-0.076851
E(CP)			1.33579271					8	-0.015537	-0.066015
E(LB)			0.49445062					9	1.482569	0.734790
23	3	1	-0.711775	-0.328336	E(LU)				0.19835768	
		2	-0.674982	-0.318458	E(CP)				0.09008641	
		3	2.386757	0.646794	E(LB)				0.10049225	
E(LU)			1.95807953							
E(CP)			0.71369343							
E(LB)			0.32586633							

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
23	10	1	-0.068856	-0.092095	23	14	1	-0.020644	-0.067022
		2	-0.065905	-0.094156			2	-0.013278	-0.054436
		3	-0.060269	-0.093058			3	-0.014991	-0.064792
		4	-0.052846	-0.089957			4	-0.011061	-0.063857
		5	-0.043918	-0.085232			5	-0.006570	-0.061888
		6	-0.033587	-0.079038			6	-0.001537	-0.058966
		7	-0.021873	-0.071429			7	0.004039	-0.055193
		8	-0.008741	-0.062395			8	0.010191	-0.050500
		9	0.005880	-0.051880			9	0.016959	-0.044870
		10	1.350115	0.719241			10	0.024395	-0.038243
E(LU)			0.15826056				11	0.032581	-0.030518
E(CP)				0.06872565			12	0.041605	-0.021572
E(LB)				0.08911283			13	0.051586	-0.011236
							14	0.891725	0.628112
								0.08176810	
								0.02129585	
								0.05953202	
23	11	1	-0.052275	-0.082619	E(LU)				
		2	-0.049614	-0.084845	E(CP)				
		3	-0.044879	-0.084262	E(LB)				
		4	-0.038754	-0.081902					
		5	-0.031451	-0.078106	23	15	1	-0.013858	-0.056886
		6	-0.023044	-0.073012			2	-0.011496	-0.059304
		7	-0.013543	-0.066668			3	-0.008457	-0.059848
		8	-0.002916	-0.059066			4	-0.004935	-0.059221
		9	0.008899	-0.050154			5	-0.000978	-0.057655
		10	0.021994	-0.039847			6	0.003395	-0.055253
		11	1.225582	0.700481			7	0.008206	-0.052040
E(LU)			0.12964842				8	0.013472	-0.048017
E(CP)				0.05237239			9	0.019220	-0.043159
E(LB)				0.07976613			10	0.025528	-0.037385
							11	0.032425	-0.030636
23	12	1	-0.039296	-0.074667			12	0.040015	-0.022775
		2	-0.036802	-0.076996			13	0.048387	-0.013657
		3	-0.032710	-0.076807			14	0.057669	-0.003074
		4	-0.027537	-0.075031			15	0.791406	0.598911
		5	-0.021441	-0.071973	E(LU)				
		6	-0.014473	-0.067761	E(CP)				
		7	-0.006638	-0.062438	E(LB)				
		8	0.002097	-0.055995					
		9	0.011784	-0.048387					
		10	0.022502	-0.039535					
		11	0.034352	-0.029328					
		12	1.108163	0.678918					
E(LU)			0.10879863						
E(CP)				0.03959874					
E(LB)				0.07194033					
23	13	1	-0.028970	-0.067886	23	16	1	-0.008277	-0.052337
		2	-0.026565	-0.070274			2	-0.005899	-0.054740
		3	-0.022939	-0.070396			3	-0.003041	-0.055433
		4	-0.018475	-0.069079			4	0.000172	-0.055058
		5	-0.013288	-0.066620			5	0.003709	-0.053835
		6	-0.007415	-0.063126			6	0.007575	-0.051846
		7	-0.000851	-0.058638			7	0.011777	-0.049129
		8	0.006430	-0.053149			8	0.016329	-0.045688
		9	0.014477	-0.046619			9	0.021298	-0.041465
		10	0.023356	-0.038975			10	0.026669	-0.036455
		11	0.033154	-0.030114			11	0.032560	-0.030526
		12	0.043981	-0.019898			12	0.038985	-0.023615
		13	0.997106	0.654769			13	0.046066	-0.015549
E(LU)			0.09335412				14	0.053887	-0.005157
E(CP)				0.02945680			15	0.022596	0.004820
E(LB)				0.06528043			16	0.695593	0.567114
								0.06630856	
								0.00920619	
								0.05006475	

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
23	17	1	-0.003655	-0.048263	23	19	1	0.003411	-0.041199
		2	-0.001244	-0.050639			2	0.005909	-0.043487
		3	0.001481	-0.051447			3	0.008471	-0.044457
		4	0.004455	-0.051283			4	0.011123	-0.044615
		5	0.007669	-0.050345			5	0.013887	-0.044125
		6	0.011133	-0.048710			6	0.016780	-0.043060
		7	0.014831	-0.046438			7	0.019798	-0.041470
		8	0.018871	-0.043448			8	0.022996	-0.039317
		9	0.023152	-0.039831			9	0.026380	-0.036600
		10	0.027817	-0.035444			10	0.030001	-0.033248
		11	0.032865	-0.030257			11	0.033825	-0.029295
		12	0.038384	-0.024144			12	0.037942	-0.024577
		13	0.044389	-0.017027			13	0.042427	-0.018580
		14	0.051034	-0.008672			14	0.047315	-0.012379
		15	0.058398	0.001120			15	0.052660	-0.004606
		16	0.066644	0.012681			16	0.058612	0.004662
		17	0.0603776	0.532147			17	0.055310	0.015808
E(LU)			0.06119601				18	0.072957	0.029414
E(CP)			0.00470017				19	0.430194	0.451531
E(LB)			0.04609331		E(LU)			0.05430916	
					E(CP)			-0.00217056	
23	18	1	0.000194	-0.044575					0.03922450
		2	0.002646	-0.046912					
		3	0.005275	-0.047812	23	20	1	0.006104	-0.038066
		4	0.008068	-0.047822			2	0.008651	-0.040298
		5	0.011028	-0.047126			3	0.011168	-0.041321
		6	0.014162	-0.045809			4	0.013716	-0.041509
		7	0.017515	-0.043866			5	0.016325	-0.041290
		8	0.021048	-0.041362			6	0.019011	-0.040466
		9	0.024872	-0.038183			7	0.021809	-0.039131
		10	0.028875	-0.034430			8	0.024700	-0.037336
		11	0.033363	-0.029780			9	0.027785	-0.034966
		12	0.038034	-0.024480			10	0.030958	-0.032134
		13	0.043231	-0.018136			11	0.034420	-0.028603
		14	0.048884	-0.010732			12	0.037984	-0.024527
		15	0.055157	-0.001905			13	0.041940	-0.019546
		16	0.062143	0.008368			14	0.046153	-0.013730
		17	0.070035	0.020767			15	0.050775	-0.006799
		18	0.515472	0.493878			16	0.055861	0.001462
E(LU)			0.05728653				17	0.061571	0.011459
E(CP)			0.00095448				18	0.068058	0.023716
E(LB)			0.04250454				19	0.075590	0.039106
							20	0.347421	0.404070
					E(LU)			0.05206387	
					E(CP)			-0.00478196	
					E(LB)			0.03618730	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
23	21	1	0.008356	0.035111	23	23	1	0.011749	-0.029300
		2	0.010952	-0.037277			2	0.014443	-0.031296
		3	0.013441	-0.038337			3	0.016915	-0.032383
		4	0.015912	-0.03818			4	0.019296	-0.032915
		5	0.018403	-0.038563			5	0.021637	-0.033014
		6	0.020936	-0.037940			6	0.023968	-0.032735
		7	0.023539	-0.036861			7	0.026314	-0.032093
		8	0.026213	-0.035349			8	0.028683	-0.031103
		9	0.029021	-0.033345			9	0.031120	-0.029730
		10	0.031907	-0.030890			10	0.033589	-0.027985
		11	0.034969	-0.027882			11	0.036174	-0.025797
		12	0.038215	-0.024224			12	0.038830	-0.023139
		13	0.041650	-0.019928			13	0.041635	-0.019922
		14	0.045352	-0.014781			14	0.044584	-0.016060
		15	0.049362	-0.008853			15	0.047728	-0.011412
		16	0.053758	-0.001297			16	0.051110	-0.005790
		17	0.058642	0.007615			17	0.054801	0.001083
		18	0.064166	0.018608			18	0.058897	0.009633
		19	0.070550	0.032491			19	0.063548	0.020550
		20	0.078160	0.050676			20	0.069018	0.035063
		21	0.266495	0.349764			21	0.075800	0.055713
E(LU)			0.05040338				22	0.085149	0.089235
E(CP)			-0.00696129				23	0.105012	0.203397
E(LB)			0.03332701					0.04846684	
								-0.01023295	
								0.02772378	
23	22	1	0.010228	-0.032246	24	2	1	-1.347247	-0.494711
		2	0.012873	-0.034337			2	2.347247	0.494711
		3	0.015348	-0.035418				4.37137282	
		4	0.017763	-0.035883	E(LU)			1.35771886	
		5	0.020166	-0.035864	E(CP)			0.49468654	
		6	0.022582	-0.035420	E(LB)				
		7	0.025037	-0.034566					
		8	0.027534	-0.033327	24	3	1	-0.726858	-0.328551
		9	0.030133	-0.031642			2	-0.691234	-0.319094
		10	0.032777	-0.029557			3	2.418093	0.647644
		11	0.035580	-0.026947	E(LU)			2.02243176	
		12	0.038475	-0.023825	E(CP)			0.72859553	
		13	0.041565	-0.020057	E(LB)			0.32618670	
		14	0.044837	-0.015569					
		15	0.048365	-0.010179	24	4	1	-0.457513	-0.244962
		16	0.052188	-0.003701			2	-0.438482	-0.240654
		17	0.056406	0.004192			3	-0.402913	-0.227825
		18	0.061135	0.013968			4	2.298908	0.713442
		19	0.066561	0.026384	E(LU)			1.14713265	
		20	0.073001	0.042777	E(CP)			0.45695549	
		21	0.081024	0.065832	E(LB)			0.24198602	
		22	0.186420	0.285386					
E(LU)			0.04922310		24	5	1	-0.312447	-0.194542
E(CP)			-0.00876815				2	-0.301019	-0.192877
E(LB)			0.03056093				3	-0.278309	-0.184517
							4	-0.248301	-0.171890
							5	2.140076	0.743825
								0.72807462	
								0.31130369	
								0.19126190	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)	
24	6	1	-0.224126	-0.160763	24	11	1	-0.056685	-0.083038	
		2	-0.216634	-0.160605			2	-0.054241	-0.085164	
		3	-0.201057	-0.154973			3	-0.049681	-0.084589	
		4	-0.180228	-0.145857			4	-0.043721	-0.082316	
		5	-0.155085	-0.133918			5	-0.036586	-0.078677	
		6	1.977123	0.756116			6	-0.028363	-0.073816	
E(LU)			0.49704860				7	-0.019070	-0.067786	
E(CP)			0.22295192				8	-0.008690	-0.060589	
E(LB)			0.15747334				9	0.002829	-0.052190	
	24	7	1	-0.165886	-0.136519		10	0.015559	-0.042523	
		2	-0.160606	-0.137280	E(LU)		11	1.278649	0.710688	
		3	-0.149328	-0.133438	E(CP)			0.13520496		
		4	-0.134146	-0.126672	E(LB)			0.05663907		
		5	-0.115746	-0.117541				0.08029586		
		6	-0.094409	-0.106282	24	12	1	-0.043350	-0.075114	
		7	1.820121	0.757733			2	-0.041075	-0.077341	
E(LU)			0.35758552				3	-0.037150	-0.077143	
E(CP)			0.16489218				4	-0.032125	-0.075425	
E(LB)			0.13330255				5	-0.026171	-0.072488	
	24	8	1	-0.125290	-0.118250			6	-0.019351	-0.068461
		2	-0.121304	-0.119593			7	-0.011678	-0.063393	
		3	-0.112772	-0.116987			8	-0.003130	-0.057285	
		4	-0.101272	-0.111878			9	0.006334	-0.050108	
		5	-0.087317	-0.104747			10	0.016780	-0.041798	
		6	-0.071114	-0.095799			11	0.028293	-0.032267	
		7	-0.052731	-0.085111			12	1.162621	0.690824	
		8	1.671800	0.752364	E(LU)			0.11310142		
E(LU)			0.26790847		E(CP)			0.04350525		
E(CP)			0.12453462		E(LB)			0.07249181		
E(LB)			0.11514035		24	13	1	-0.032719	-0.068363	
	24	9	1	-0.095798	-0.103970			2	-0.030535	-0.070648
		2	-0.092592	-0.105691			3	-0.027071	-0.070743	
		3	-0.085890	-0.103970			4	-0.022744	-0.069468	
		4	-0.076896	-0.100075			5	-0.017683	-0.067099	
		5	-0.066000	-0.094425			6	-0.011934	-0.063752	
		6	-0.053356	-0.087200			7	-0.005499	-0.059470	
		7	-0.039009	-0.078467			8	0.001635	-0.054260	
		8	-0.022943	-0.068229			9	0.009515	-0.048088	
		9	1.532484	0.742027			10	0.018189	-0.040903	
E(LU)			0.20751570				11	0.027735	-0.032622	
E(CP)			0.09529249				12	0.038242	-0.023135	
E(LB)			0.10098133				13	1.052869	0.668551	
	24	10	1	-0.073685	-0.092486	E(LU)		0.09664182		
		2	-0.070954	-0.094454	E(CP)			0.03305372		
		3	-0.065509	-0.093387	E(LB)			0.06585529		
		4	-0.058278	-0.090406						
		5	-0.049557	-0.085886						
		6	-0.039461	-0.079984						
		7	-0.028021	-0.072761						
		8	-0.015218	-0.064218						
		9	-0.000998	-0.054317						
		10	1.401679	0.727899						
E(LU)			0.16539357							
E(CP)			0.07341826							
E(LB)			0.08962194							

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
24	14	1	-0.024127	-0.062531	24	17	1	-0.006499	-0.048891
		2	-0.021983	-0.064844			2	-0.004321	-0.051174
		3	-0.018857	-0.065168			3	-0.001761	-0.051934
		4	-0.015060	-0.064253			4	0.001076	-0.051760
		5	-0.010682	-0.062346			5	0.004211	-0.050811
		6	-0.005761	-0.059561			6	0.007533	-0.049264
		7	-0.000290	-0.055934			7	0.011242	-0.046993
		8	0.005750	-0.051466			8	0.015072	-0.044237
		9	0.012378	-0.046144			9	0.019386	-0.040701
		10	0.019668	-0.039899			10	0.023957	-0.036555
		11	0.027663	-0.032671			11	0.028939	-0.031656
		12	0.036447	-0.024354			12	0.034306	-0.025980
		13	0.046122	-0.014814			13	0.040200	-0.019361
		14	0.948731	0.643985			14	0.046700	-0.011667
E(LU)			0.08422122				15	0.053823	-0.002782
E(CP)			0.02462280				16	0.061755	0.007593
E(LB)			0.06013250				17	0.664373	0.556173
					E(LU)			0.06186649	
					E(CP)			0.00738246	
					E(LB)			0.04679261	
24	15	1	-0.017105	-0.057431	24	18	1	-0.002475	-0.045255
		2	-0.014969	-0.059749			2	-0.000259	-0.047504
		3	-0.012092	-0.060254			3	0.002201	-0.048354
		4	-0.008696	-0.059630			4	0.004866	-0.048336
		5	-0.004850	-0.058110			5	0.007700	-0.047659
		6	-0.000583	-0.055800			6	0.010794	-0.046318
		7	0.004161	-0.052701			7	0.014016	-0.044587
		8	0.009290	-0.048895			8	0.017417	-0.042119
		9	0.014974	-0.044259			9	0.021386	-0.038895
		10	0.021148	-0.038824			10	0.025182	-0.035448
		11	0.027900	-0.032498			11	0.029642	-0.031020
		12	0.035313	-0.025177			12	0.034054	-0.026209
		13	0.043457	-0.016750			13	0.039415	-0.020075
		14	0.052436	-0.007059			14	0.044838	-0.013352
		15	0.849616	0.617138			15	0.050958	-0.005370
E(LU)			0.07475231				16	0.057699	0.003929
E(CP)			0.01774484				17	0.065252	0.014885
E(LB)			0.05513653				18	0.577315	0.521587
					E(LU)			0.05752515	
					E(CP)			0.00346018	
					E(LB)			0.04324895	
24	16	1	-0.011313	-0.052921					
		2	-0.009163	-0.055227					
		3	-0.006469	-0.055875					
		4	-0.003385	-0.055494					
		5	0.000046	-0.054297					
		6	0.003828	-0.052365					
		7	0.007921	-0.049771					
		8	0.012411	-0.046465					
		9	0.017303	-0.042445					
		10	0.022558	-0.037723					
		11	0.028368	-0.032132					
		12	0.034638	-0.025703					
		13	0.041559	-0.018228					
		14	0.049152	-0.009617					
		15	0.057555	0.000342					
		16	0.754990	0.587928					
E(LU)			0.06747956						
E(CP)			0.01208139						
E(LB)			0.05072627						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
24	19	1	0.000905	-0.041941	24	21	1	0.006154	-0.036040
		2	0.003164	-0.044148			2	0.008506	-0.038142
		3	0.005555	-0.045066			3	0.010815	-0.039151
		4	0.008071	-0.045193			4	0.013140	-0.039493
		5	0.010734	-0.044684			5	0.015514	-0.039306
		6	0.013521	-0.043644			6	0.017945	-0.038667
		7	0.016435	-0.042115			7	0.020429	-0.037625
		8	0.019637	-0.039942			8	0.023099	-0.036040
		9	0.022803	-0.037505			9	0.025743	-0.034203
		10	0.026719	-0.033941			10	0.028697	-0.031687
		11	0.029997	-0.030672			11	0.031580	-0.028925
		12	0.034402	-0.025868			12	0.034836	-0.025342
		13	0.038730	-0.020747			13	0.038156	-0.021392
		14	0.043507	-0.014657			14	0.041933	-0.016415
		15	0.048732	-0.007553			15	0.045799	-0.010844
		16	0.054520	0.000812			16	0.050108	-0.004137
		17	0.060958	0.010675			17	0.054842	0.003809
		18	0.068216	0.022447			18	0.060165	0.013408
		19	0.493393	0.483741			19	0.066188	0.025170
E(LU)			0.05417052				20	0.073197	0.035844
E(CP)				0.00017117			21	0.333154	0.395179
E(LB)				0.04002428	E(LU)			0.04962788	
					E(CP)			-0.00492314	
					E(LB)			0.03429681	
24	20	1	0.003753	-0.038888	24	22	1	0.008175	-0.033339
		2	0.006057	-0.041046			2	0.010574	-0.035378
		3	0.008399	-0.042017			3	0.012864	-0.036413
		4	0.010808	-0.042259			4	0.015129	-0.036835
		5	0.013294	-0.041940			5	0.017403	-0.036782
		6	0.015900	-0.041093			6	0.019717	-0.036300
		7	0.018611	-0.039782			7	0.022047	-0.035464
		8	0.021436	-0.038014			8	0.024510	-0.034155
		9	0.024426	-0.035765			9	0.026977	-0.032554
		10	0.027521	-0.033081			10	0.029650	-0.030414
		11	0.031146	-0.029441			11	0.032257	-0.028021
		12	0.034308	-0.025968			12	0.035139	-0.024936
		13	0.038424	-0.021075			13	0.038322	-0.021171
		14	0.042551	-0.015682			14	0.041338	-0.017209
		15	0.047082	-0.009322			15	0.044935	-0.011998
		16	0.052019	-0.001870			16	0.048628	-0.006114
		17	0.057545	0.007016			17	0.052763	0.001032
		18	0.063743	0.017651			18	0.057327	0.009615
		19	0.070809	0.030651			19	0.062480	0.020215
		20	0.412170	0.441924			20	0.068458	0.033512
E(LU)			0.05159088				21	0.075549	0.050964
E(CP)				-0.00259469			22	0.255757	0.341745
E(LB)				0.03705876	E(LU)			0.04816352	
					E(CP)			-0.00687983	
					E(LB)			0.03168222	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
24	23	1	0.009865	-0.030709	25	3	1	-0.741297	-0.328748
		2	0.012311	-0.032676			2	-0.706762	-0.319677
		3	0.014593	-0.033724			3	2.448059	0.648426
		4	0.016814	-0.034214				2.08530608	
		5	0.019018	-0.034270	E(LU)			0.74287178	
		6	0.021232	-0.033942	E(CP)			0.32648069	
		7	0.023451	-0.033279	E(LB)				
		8	0.025757	-0.032215	25	4	1	-0.468472	-0.245175
		9	0.028049	-0.030887			2	-0.450043	-0.241037
		10	0.030536	-0.029034			3	-0.415470	-0.228750
		11	0.032941	-0.026957			4	2.333986	0.714962
		12	0.035565	-0.024275				1.18738033	
		13	0.038329	-0.021160	E(LU)			0.46781327	
		14	0.041191	-0.017439	E(CP)			0.24222296	
		15	0.044281	-0.013616	E(LB)				
		16	0.047572	-0.007758	25	5	1	-0.321316	-0.194777
		17	0.051172	-0.001443			2	-0.310282	-0.193172
		18	0.055132	0.006201			3	-0.288191	-0.185159
		19	0.059561	0.015675			4	-0.258993	-0.173084
		20	0.064672	0.027621			5	2.178782	0.746191
		21	0.070703	0.043424				0.75602911	
		22	0.078235	0.065561	E(LU)			0.32008373	
		23	0.179020	0.278512	E(CP)			0.19162842	
E(LU)			0.04711383		E(LB)				
E(CP)			-0.00851289		25	6	1	-0.231589	-0.161021
E(LB)			0.02914162				2	-0.224397	-0.160862
24	24	1	0.011248	-0.027993			3	-0.209240	-0.155458
		2	0.013739	-0.029871			4	-0.188950	-0.146734
		3	0.016021	-0.030917			5	-0.164473	-0.135339
		4	0.018216	-0.031460			6	2.018650	0.759414
		5	0.020370	-0.031614	E(LU)			0.51744819	
		6	0.022514	-0.031424	E(CP)			0.23032985	
		7	0.024647	-0.030730	E(LB)			0.15786311	
		8	0.026838	-0.030091	25	7	1	-0.172349	-0.136802
		9	0.029015	-0.028989			2	-0.167311	-0.137524
		10	0.031329	-0.027477			3	-0.156342	-0.133831
		11	0.033589	-0.025584			4	-0.141540	-0.127351
		12	0.035989	-0.023440			5	-0.123602	-0.118629
		13	0.038543	-0.020740			6	-0.102823	-0.107905
		14	0.041131	-0.017557			7	1.863966	0.762043
		15	0.043928	-0.013710	E(LU)			0.37295445	
		16	0.046862	-0.009153	E(CP)			0.17125667	
		17	0.050034	-0.003639	E(LB)			0.13371230	
		18	0.053531	0.003056	25	3	1	-0.130991	-0.118557
		19	0.057380	0.011390			2	-0.127221	-0.119837
		20	0.061783	0.021945			3	-0.118931	-0.117327
		21	0.066927	0.036007			4	-0.107714	-0.112428
		22	0.073331	0.055932			5	-0.094093	-0.105611
		23	0.082153	0.088238			6	-0.078289	-0.097082
		24	0.100863	0.198122			7	-0.060385	-0.086925
E(LU)			0.04643549				8	1.717625	0.757767
E(CP)			-0.00984533		E(LU)			0.27973288	
E(LB)			0.02652435		E(CP)			0.13012998	
25	2	1	-1.368683	-0.494926	E(LB)			0.11556839	
		2	2.368683	0.494926					
E(LU)			4.48592812						
E(CP)			1.37873247						
E(LB)			0.49490321						

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
25	9	1	-0.100902	-0.104300	25	13	1	-0.036308	-0.068792
		2	-0.097898	-0.105944			2	-0.034320	-0.070982
		3	-0.091397	-0.104281			3	-0.031004	-0.071058
		4	-0.082624	-0.100540			4	-0.026804	-0.069819
		5	-0.071979	-0.095134			5	-0.021861	-0.067534
		6	-0.059629	-0.088240			6	-0.016228	-0.064321
		7	-0.045632	-0.079936			7	-0.009922	-0.060231
		8	-0.029985	-0.070233			8	-0.002924	-0.055270
		9	1.58004	0.748609			9	0.004794	-0.049420
E(LU)			0.21673546				10	0.013273	-0.042642
E(CP)			0.10028244				11	0.022584	-0.034867
E(LB)				0.10142692			12	0.032798	-0.026010
							13	1.105923	0.680946
25	10	1	-0.078304	-0.092840	E(LU)			0.10012423	
		2	-0.075769	-0.094722	E(CP)			0.03650889	
		3	-0.070501	-0.093684	E(LB)				0.06637441
		4	-0.063450	-0.090817					
		5	-0.054925	-0.086485	25	14	1	-0.027463	-0.062987
		6	-0.045053	-0.080848			2	-0.025518	-0.065206
		7	-0.033874	-0.073973			3	-0.022537	-0.065502
		8	-0.021382	-0.065870			4	-0.018860	-0.064606
		9	-0.007535	-0.056515			5	-0.014588	-0.062761
		10	1.450793	0.735755			6	-0.003771	-0.060083
E(LU)			0.17263602				7	-0.004406	-0.056611
E(CP)			0.07791785				8	0.001530	-0.052347
E(LB)				0.09008494			9	0.008022	-0.047302
							10	0.015177	-0.041393
25	11	1	-0.060903	-0.083415			11	0.022982	-0.034605
		2	-0.058654	-0.085451			12	0.031548	-0.026830
		3	-0.054256	-0.084885			13	0.040941	-0.017971
		4	-0.048449	-0.082692			14	1.002942	0.658203
		5	-0.041474	-0.079199	E(LU)			0.08688651	
		6	-0.033425	-0.074550	E(CP)			0.02782135	
		7	-0.024332	-0.068804	E(LB)				0.06067302
		8	-0.014184	-0.061972					
		9	-0.002945	-0.054030	25	15	1	-0.020217	-0.057916
		10	0.009446	-0.044927			2	-0.018283	-0.060177
		11	1.329176	0.719926			3	-0.015551	-0.060613
E(LU)			0.14090683				4	-0.012269	-0.059993
E(CP)			0.06073226				5	-0.008537	-0.058526
E(LB)				0.08077665			6	-0.004338	-0.056280
							7	0.000300	-0.053317
25	12	1	-0.047230	-0.075517			8	0.005319	-0.049695
		2	-0.045150	-0.077650			9	0.017966	-0.045241
		3	-0.041377	-0.077446			10	0.016954	-0.040149
		4	-0.036489	-0.075783			11	0.023615	-0.034163
		5	-0.030670	-0.072958			12	0.030844	-0.027321
		6	-0.023991	-0.069100			13	0.038774	-0.019482
		7	-0.016473	-0.064265			14	0.047483	-0.010542
		8	-0.008104	-0.058459			15	0.904940	0.633385
		9	0.001149	-0.051664	E(LU)			0.07673648	
		10	0.011340	-0.043833	E(CP)			0.02071714	
		11	0.022540	-0.034894	E(LB)				0.05570065
		12	1.214454	0.701568					
E(LU)			0.11757719						
E(CP)			0.04725515						
E(LB)				0.07299117					

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
25	16	1	-0.014226	-0.053437	25	19	1	-0.001511	-0.042582
		2	-0.012280	-0.055655			2	0.000536	-0.044712
		3	-0.009730	-0.056262			3	0.002777	-0.045580
		4	-0.006767	-0.055881			4	0.005148	-0.045706
		5	-0.003416	-0.054698			5	0.007784	-0.045118
		6	0.000228	-0.052868			6	0.010293	-0.044292
		7	0.004311	-0.050319			7	0.013648	-0.042297
		8	0.008740	-0.047138			8	0.016012	-0.040961
		9	0.013383	-0.043435			9	0.019203	-0.038460
		10	0.018781	-0.038783			10	0.024225	-0.034053
		11	0.024316	-0.033639			11	0.026723	-0.031592
		12	0.030527	-0.027559			12	0.030579	-0.027487
		13	0.037271	-0.020612			13	0.034843	-0.022690
		14	0.044668	-0.012645			14	0.040233	-0.016383
		15	0.052795	-0.003537			15	0.045011	-0.010159
		16	0.0811399	0.606468			16	0.050657	-0.002512
E(LU)			0.06888924				17	0.056882	0.006342
E(CP)			0.01485185				18	0.063787	0.016770
E(LB)			0.05131672				19	0.553170	0.511471
								0.05430050	
								0.00244102	
								0.04072222	
25	17	1	-0.009232	-0.049443	25	20	1	0.001479	-0.039587
		2	-0.007260	-0.051640			2	0.003569	-0.041673
		3	-0.004848	-0.052357			3	0.005756	-0.042596
		4	-0.002117	-0.052162			4	0.008031	-0.042816
		5	0.000879	-0.051264			5	0.010448	-0.042449
		6	0.004177	-0.049710			6	0.013025	-0.041554
		7	0.007815	-0.047517			7	0.015402	-0.040540
		8	0.011434	-0.044984			8	0.018347	-0.038621
		9	0.015921	-0.041405			9	0.021346	-0.036313
		10	0.020253	-0.037606			10	0.024325	-0.033953
		11	0.025191	-0.032939			11	0.028185	-0.030127
		12	0.030451	-0.027620			12	0.030435	-0.027632
		13	0.036231	-0.021444			13	0.035676	-0.021855
		14	0.042593	-0.014304			14	0.036707	-0.017912
		15	0.049500	-0.006173			15	0.043784	-0.011387
		16	0.057147	0.003248			16	0.048355	-0.004818
		17	0.721867	0.577320			17	0.053791	0.003245
E(LU)			0.06278626				18	0.059696	0.012672
E(CP)			0.00997094				19	0.066471	0.023804
E(LB)			0.04741317				20	0.473171	0.474112
								0.05139734	
								-0.00046792	
								0.03780750	
25	18	1	-0.005043	-0.045848					
		2	-0.003036	-0.048015					
		3	-0.000726	-0.048819					
		4	0.001824	-0.048779					
		5	0.004483	-0.048170					
		6	0.007751	-0.046642					
		7	0.010435	-0.045269					
		8	0.014601	-0.042266					
		9	0.017272	-0.040246					
		10	0.022055	-0.036060					
		11	0.026242	-0.032037					
		12	0.030231	-0.027809					
		13	0.035679	-0.021917					
		14	0.041032	-0.015644					
		15	0.047011	-0.008309					
		16	0.053506	0.000123					
		17	0.060779	0.009946					
		18	0.635905	0.545761					
E(LU)			0.05802293						
E(CP)			0.00588284						
E(LB)			0.04390460						

TABLE OF HEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
25	21	1	0.004015	-0.036813	25	23	1	0.007991	-0.01733
		2	0.006150	-0.038850			2	0.010217	-0.033654
		3	0.008301	-0.039812			3	0.012332	-0.034661
		4	0.010494	-0.040124			4	0.014413	-0.035114
		5	0.012767	-0.039913			5	0.016537	-0.035132
		6	0.015083	-0.039304			6	0.018615	-0.034796
		7	0.017547	-0.038195			7	0.020791	-0.034037
		8	0.019926	-0.036894			8	0.022797	-0.033205
		9	0.023362	-0.034198			9	0.025487	-0.031417
		10	0.024924	-0.033298			10	0.027226	-0.030315
		11	0.028334	-0.029964			11	0.030451	-0.027371
		12	0.032751	-0.025098			12	0.032439	-0.025277
		13	0.033983	-0.023707			13	0.034975	-0.022600
		14	0.038804	-0.017806			14	0.038427	-0.018207
		15	0.042477	-0.012817			15	0.040862	-0.014907
		16	0.046778	-0.006543			16	0.044536	-0.009371
		17	0.051285	0.000504			17	0.047835	-0.003905
		18	0.056394	0.009060			18	0.051722	0.003109
		19	0.062243	0.019180			19	0.056077	0.011315
		20	0.068693	0.031758			20	0.060755	0.021679
		21	0.095689	0.432743			21	0.066131	0.034261
E(LU)			0.04914458				22	0.073053	0.051189
E(CP)			-0.00293163				23	0.245889	0.234151
E(LB)			0.03511308		E(LU)			0.04611741	
					E(CP)			-0.00678580	
					E(LB)			0.03018924	
25	22	1	0.006168	-0.034211	25	24	1	0.009526	-0.029309
		2	0.008348	-0.036193			2	0.011794	-0.031162
		3	0.010476	-0.037183			3	0.013905	-0.032175
		4	0.012607	-0.037570			4	0.015953	-0.032683
		5	0.014776	-0.037485			5	0.017988	-0.032792
		6	0.017026	-0.036955			6	0.020022	-0.032574
		7	0.019221	-0.036171			7	0.022074	-0.032010
		8	0.021340	-0.035185			8	0.024017	-0.031278
		9	0.024679	-0.032515			9	0.026504	-0.029812
		10	0.025895	-0.032125			10	0.028155	-0.028849
		11	0.030229	-0.027673			11	0.031096	-0.026352
		12	0.031117	-0.027074			12	0.032808	-0.024695
		13	0.035583	-0.021713			13	0.035503	-0.021765
		14	0.038063	-0.018702			14	0.038100	-0.018724
		15	0.041779	-0.013661			15	0.040722	-0.015128
		16	0.045324	-0.008299			16	0.043591	-0.010706
		17	0.049433	-0.001734			17	0.046790	-0.005556
		18	0.053748	0.005862			18	0.050125	0.000586
		19	0.058821	0.015944			19	0.053932	0.007926
		20	0.064336	0.026491			20	0.057987	0.017243
		21	0.071016	0.040315			21	0.062967	0.028582
		22	0.320015	0.386798			22	0.068493	0.043984
E(LU)			0.04741691				23	0.075661	0.045216
E(CP)			-0.00501984				24	0.172188	0.272031
E(LB)			0.03258909		E(LU)			0.04517886	
					E(CP)			-0.00826855	
					E(LB)			0.02784672	

TABLE OF WEIGHTS (CONTINUED)

N	M	I	A(N,M,I)	C(N,M,I)	N	M	I	A(N,M,I)	C(N,M,I)
25	25	1	0.010788	-0.026796					
		2	0.013098	-0.028566					
		3	0.015213	-0.029573					
		4	0.017239	-0.030122					
		5	0.019234	-0.030313					
		6	0.021211	-0.030205					
		7	0.023185	-0.029800					
		8	0.025057	-0.029207					
		9	0.027393	-0.028041					
		10	0.029004	-0.027158					
		11	0.031672	-0.025206					
		12	0.033333	-0.023590					
		13	0.035757	-0.021260					
		14	0.038198	-0.018529					
		15	0.040571	-0.015429					
		16	0.043268	-0.011548					
		17	0.046011	-0.007108					
		18	0.048983	-0.001688					
		19	0.052348	0.004773					
		20	0.055864	0.013016					
		21	0.060199	0.023073					
		22	0.064907	0.036847					
		23	0.071049	0.056035					
		24	0.079353	0.087235					
		25	0.097036	0.193159					
E(LU)			-0.00009232						
E(CP)				-0.00948561					
E(LB)				0.02542407					

APPENDIX D

CRAMER-RAO EFFICIENCIES OF BEST LINEAR INVARIANT ESTIMATES OF PARAMETERS OF THE EXTREME-VALUE DISTRIBUTION

INTRODUCTION AND SUMMARY

The Weibull distribution, since it was empirically derived by W. Weibull [12] in 1939, has been shown in innumerable situations to provide an appropriate model for survival populations associated with life testing. This distribution, which had been derived earlier by Von Mises and Fisher and Tippett (see Gumbel [3]) using extreme-value considerations, is also known as the Fisher-Tippett type III distribution or the third asymptotic distribution of smallest values. This explains why the Weibull model is often applicable when the cause of failure is characterized by a weakest-link or severest-flaw phenomenon.

When there is no threshold below which a failure cannot occur, the following two-parameter form of the Weibull distribution may apply:

$$F_{\delta,b}(t) \begin{cases} = 1 - \exp[-(t/\delta)^{1/b}], & t \geq 0 \\ = 0 & \text{otherwise} . \end{cases}$$

Here $\delta > 0$ is a scale parameter and $b > 0$ determines the shape of the distribution. The location parameter present in the three-parameter form (when a lower failure threshold does exist) is assumed to be zero.

This two-parameter Weibull distribution can also be useful in providing a model for populations which are not of the survival type. A recent example is a study of the thrust build-up curves for a large rocket

engine. It was found that at any specified time from engine start the observed thrust levels for the specified engine system over many runs could be very well described by means of the two-parameter Weibull. It is not clear at this time why this distribution provides such a good model for the thrust build-up process.

If any random variable T has the Weibull distribution with parameters δ and b , then $X = \log T$ has the (first) extreme-value distribution of smallest values, with

$$P(X \leq x) = F_{u,b}(x) = 1 - \exp(-\exp((x-u)/b)), \quad b > 0.$$

The parameter b is a scale parameter of this distribution and $u = \log \delta$ is the mode, a location parameter. For any estimation problem, an analysis in terms of X rather than T will be more fruitful.

One of the difficulties encountered in dealing with the two-parameter Weibull or extreme-value distribution has been the fact that "good" estimates of the parameters are not easily obtained. The maximum-likelihood estimates are obtained only with considerable effort (iteratively), and the mean squared errors of these estimates are not known except in the asymptotic case. Furthermore, since the minimally sufficient statistic for either the Weibull or extreme-value distribution consists of all the available extreme-value observations (see [10]), the dimension of the sufficient statistic is equal to the number of observations made.

Therefore, the result of Rao [11], which guarantees that maximum-likelihood estimates are the minimum-variance estimates of their expected values (when the number of sufficient statistics is equal to the number of parameters to be estimated), is not applicable when more than two observations are made. Hence one cannot claim optimality properties for the maximum-likelihood estimates of the two Weibull parameters when the number of observations is greater than two, but not large enough for asymptotic theory to apply.

A method in widespread use for Weibull parameter estimation employs a graphical plot which is based on fitting a linear model by approximating the method of least squares. The Weibull plot is of unquestionable value in finding outliers or in determining whether the sample data indicate that the population is of the prescribed type. With respect to the problem of estimation, however, graphical procedures which involve visually fitting the least-squares line will obviously be inferior to analytical procedures which yield true Gauss-Markov least-squares estimates.

The least-squares or best linear unbiased estimates which, for limited sample sizes, can be found relatively easily for certain functions of the two extreme-value parameters, once appropriate weights (or coefficients) have been found, enjoy all the usual asymptotic properties of consistency, efficiency, and normality provided by the maximum-likelihood

estimates (see Blom [1]). Furthermore, if the weights for obtaining these estimates are available, the covariance matrices of the estimates are available as well. A recent result given in [9] allows one to calculate as simple functions of the least-squares estimates and their covariance matrices, linear estimates which have smallest expected loss among all linear estimates with expected loss invariant under transformations of location and scale. Here loss is defined to be squared error divided by the square of the extreme-value scale parameter. These estimates are uniformly better than the best linear unbiased (BLU) estimates and are, in fact, the unique admissible minimax linear estimates. They, of course, also have the asymptotic properties mentioned above plus the property of asymptotic unbiasedness.

Calculation of the weights for obtaining the best linear unbiased estimates (based on the results of Lieblein [7]), and from these the best linear invariant estimates of the two extreme-value parameters, has been completed for censored samples up to size 25. These calculated weights, along with the variances and covariances of the estimates, appear in [10]¹.

¹ Although the calculations were performed for sample size n ranging from 2 through 25 (an extension of tables of Lieblein [8] giving values for n ranging from 2 through 6) the results given in [10] are through n equal to 20 only.

In the present report expressions are derived for Cramér-Rao bounds for the expected squared error of regular invariant estimates of extreme-value location and scale parameters. The bounds are calculated and compared with the mean squared error of the best linear invariant estimates of the two extreme-value parameters and, in addition, similar comparisons are made for certain percentiles of the distribution, for censored samples up to size 25.

All of the estimation procedures considered above, along with all but the numerical results given below, are applicable to the general case in which any selection of observations is censored from a size n sample. In the following, however, it is assumed that only the largest $n-r$, $2 \leq r \leq n$, observations are censored. This assumption corresponds to the situation in life testing in which testing is terminated at the time of the r^{th} failure. Termination of a life test in this manner (by failure number) is called Type II censoring to distinguish it from the type of censoring (Type I) wherein testing is stopped at a specified time after the initiation of the test.

EFFICIENCIES OF BEST LINEAR INVARIANT ESTIMATES OF PARAMETERS OF THE EXTREME-VALUE DISTRIBUTION

Assume a population having the extreme-value distribution of smallest values given by

$$F_{u,b}(x) = 1 - \exp(-\exp((x-u)/b)), \quad b > 0. \quad (1)$$

The function $R_{u,b}(x) = 1 - F_{u,b}(x) = \exp(-\exp((x-u)/b))$ gives the proportion of the population lying to the right of the point x . Assume a specified value R for $R_{u,b}(x)$ and let x_R be the point defined by $R = \exp(-\exp((x_R-u)/b))$. Then $x_R = u + b \log \log(1/R)$ is the percentile above which 100% of the population lies. If $R = 1/e$, then $x_R = u$. In a life-testing situation $R(x)$ is the proportion of the population surviving at log time x , so that if a reliability or survival proportion R is specified, the corresponding x_R is the logarithm of the time at which 100% of the population will have survived.

Let a size n sample be chosen from the population with distribution (1) and let an estimate of x_R be based on $X_{(1,n)} \leq X_{(2,n)} \leq \dots \leq X_{(r,n)}$, the first r , $2 \leq r \leq n$, of the n ordered observations. In [10] there is considered the class of linear estimates of u , b , and x_R with expected loss invariant under location and scalar transformations, where loss is defined as squared error divided by b^2 . It is shown that

the best (minimum-expected-loss) estimates in this class are linear functions of the BLU estimates of u and b . Let u^* with variance Ab^2 and b^* with variance Cb^2 be the BLU estimates of u and b , respectively, and let Bb^2 be the covariance of the two estimates. The BLU estimate of $x_R = u + b \log \log(1/R)$ is $\bar{x}_R^* = u^* + b^* \log \log(1/R)$, with variance $Q_R b^2 = [A + 2B \log \log(1/R) + C(\log \log(1/R))^2]b^2$. The best linear invariant, BLI, estimate of x_R is $\tilde{x}_R = u^* - b^* [B/(1+C)] + [b^*/(1+C)] \log \log(1/R) \equiv \tilde{u} + \tilde{b} \log \log(1/R)$. The expected losses for \tilde{u} and \tilde{b} are $\tilde{A}b^2 = [A - B^2/(1+C)]b^2$ and $\tilde{C}b^2 = [C/(1+C)]b^2$, respectively, with $E(\tilde{u}\tilde{b} - ub) \equiv \tilde{B}b^2 = [B/(1+C)]b^2$. For \tilde{x}_R , the expected loss is thus $\tilde{Q}_R b^2 = [\tilde{A} + 2\tilde{B} \log \log(1/R) + \tilde{C}(\log \log(1/R))^2]b^2$ or $\tilde{Q}_R b^2 = \{A + 2B \log \log(1/R) + C(\log \log(1/R))^2 - [(B + C \log \log(1/R))^2/(1+C)]\}b^2$, clearly uniformly less than $Q_R b^2$. One may then inquire as to the efficiency of this estimate with respect to any nonlinear estimate which could be obtained.

Since the expected value of \tilde{x}_R is equal to $u + b \log \log(1/R) - [(B + C \log \log(1/R))/(1+C)]b$, this estimate is, in general, biased. Cramer-Rao bounds for the variance of unbiased estimates, therefore constitute for each r and n an incorrect standard with which to compare the mean squared error (MSE) of estimates with this given bias.

The variance $nQ_R^0 b^2 = n [A^0 + 2B^0 \log \log(1/R) + C^0 (\log \log(1/R))^2] b^2$ of an efficient estimate of $\sqrt{nx_R}$ based on $X_{(1,n)}, X_{(2,n)}, \dots, X_{(r,n)}$ depends upon r and n through $p = r/n$ only. The expression giving the appropriate lower bounds for the mean squared error of biased estimates of x_R as a function of A^0 , B^0 , and C^0 and any given bias is derived in Appendix D.2.

This expression for estimates of x_R with bias $-[(F+C \log \log(1/R))/(1+C)]b$ is

$$\begin{aligned} & \hat{A}^0 - \frac{2B(F^0)(1+C) - B^2(1+C^0)}{(1+C)^2} + \\ & \frac{2[B^0(1+C) + B(C-C^0)] \log \log(1/R)}{(1+C)^2} + \frac{C^0 + C^2}{(1+C)^2} (\log \log(1/R))^2 b^2 \\ & \equiv [\tilde{A}^0 + 2\tilde{B}^0 \log \log(1/R) + \tilde{C}^0 (\log \log(1/R))^2] b^2. \end{aligned}$$

This preliminary result is not, however, particularly meaningful as a lower bound, since other good invariant estimates which are nonlinear and have bias different from that specified may exist. A more meaningful lower bound would be one for the MSE of invariant estimates of x_R , a natural analogue to the classical bound Q_R^0 which provides the standard with which one may compare the variances of unbiased estimates of this parameter. Expressions giving the lower bounds for the MSE of invariant estimates of general location and scale parameters are therefore derived in Appendix D.1 and applied to the location parameter x_R .

(see footnote, p. 149) and the scale parameter b . These bounds for \bar{x}_R and b are

$$\begin{aligned}\bar{Q}_R^0 b^2 &= \{A^0 + 2B^0 \log \log (1/R) + C^0 (\log \log (1/R))^2 \\ &\quad - (B^0 + C^0 \log \log (1/R))^2 / (1+C^0)\} b^2 \\ &= \{\bar{A}^0 + 2\bar{B}^0 \log \log (1/R) + \bar{C}^0 (\log \log (1/R))^2\} b^2\end{aligned}$$

$$\text{and} \quad [C^0 / (1+C^0)] b^2 = \bar{C}^0 b^2,$$

respectively.

Table D.I gives values for \bar{Q}_R and \bar{Q}_R^0 , with $R = .90$ and $R = .95$, and \bar{A} , \bar{B} , \bar{C} , \bar{A}^0 , \bar{B}^0 , and \bar{C}^0 for $2 \leq n \leq 25$, $2 \leq r \leq n$. Table D.II gives values for A , B , C , A^0 , B^0 , C^0 , Q_R , and Q_R^0 for the same values of R , r , and n so comparisons can be made among the various sets of expected losses. The values for A , B , and C are obtained from [10] as are the expressions for A^0 , B^0 , and C^0 . The Cramér-Rao efficiency of \bar{x}_R for any combination of R , r , and n (and with b considered a nuisance parameter) is simply \bar{Q}_R^0 divided by \bar{Q}_R . Cramér-Rao efficiencies for \bar{u} (\bar{x}_R with $R = 1/e$ and b a nuisance parameter) will be given by \bar{A}^0/\bar{A} . Efficiencies for \bar{b} with \bar{x}_R a nuisance parameter will be given by \bar{C}^0/\bar{C} . The values of the efficiencies of $\bar{Q}_{.90}$ for $2 \leq n \leq 18$, $2 \leq r \leq n$ appear in Table D.III.

It can be seen from Table D.III that for $n \leq 18$ the Cramér-Rao efficiencies of $\tilde{Q}_{.90}$ are greater than .86 when r is greater than 2. When r is equal to 2 $(X_{(1,n)}, X_{(2,n)})$ is a complete sufficient statistic for x_R and b , as is shown in [10]. The estimates X_R^* and b^* , therefore, are the unique (with probability 1) uniformly minimum-variance unbiased estimates. It can be further inferred on the basis of the results of Appendix D.1 that, for $r = 2$, \tilde{X}_R and \tilde{b} are best in the class of all invariant estimates of x_R and b respectively, so that all the bounds given in Table D.I, as well as in Table D.II, are unrealistically low for r equal to 2 at least.

From Table D.I it can be observed that, for $r \geq 8$, all of the values given for expected loss indicate that the corresponding estimates have efficiencies of at least .84 with respect to their lower bounds.

A comparison of Table D.I and Table D.II shows that the discrepancy between the MSE of the BLI estimates and that of the BLU estimates is most pronounced when n is small and/or when there is extensive censoring and when a specified R is large.

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APPENDIX D.1

CRAMER-RAO LOWER BOUNDS FOR INVARIANT ESTIMATES OF LOCATION AND SCALE PARAMETERS

Let Y_1, Y_2, \dots, Y_r be the first r order statistics of a size n random sample chosen from a population with density $f_{\mu, \sigma}(x)$, where (μ, σ) is a location-scale parameter¹ with $\sigma > 0$. Let the joint density of Y_1, Y_2, \dots, Y_r be $h_{\mu, \sigma}(y_1, y_2, \dots, y_r)$, let $p = r/n$, and let $\hat{\mu}$ and $\hat{\sigma}$ be the maximum-likelihood estimates, based on Y_1, Y_2, \dots, Y_r , of μ and σ , respectively.

It is assumed that the regularity conditions given in [4] are satisfied so that the concentration ellipse of the joint distribution of any pair of regular unbiased estimates of $\sqrt{n}\mu$ and $\sqrt{n}\sigma$ (where the definition of regular estimation is given in Appendix B with $\theta = (\mu, \sigma)$) contains the fixed ellipse specified by the asymptotic variances and covariances of $\sqrt{n}\hat{\mu}$ and $\sqrt{n}\hat{\sigma}$. Thus, the variance of any regular unbiased estimate

¹Here, if a density $f(x|\theta)$ with respect to Lebesgue measure exists, $\theta = (\theta_1, \theta_2)$ is a location-scale parameter if and only if $f(x|\theta) = \frac{1}{\theta_2} g\left(\frac{x-\theta_1}{\theta_2}\right)$ for some function g . If $f(x|\theta)$ exists and (θ_1, θ_2) is a location-scale parameter, then for c a known constant, $(\theta_1 + c\theta_2, c\theta_2) = (\theta'_1, \theta'_2)$ is a location-scale parameter, since $f(x|\theta'_1, \theta'_2) = \frac{c}{\theta'_2} g\left(\frac{x-\theta'_1}{\theta'_2/c}\right) = \frac{1}{\theta'_2} g\left(\frac{x-\theta'_1}{\theta'_2}\right)$ for some η .

of $\sqrt{n}\mu$, where σ is considered a nuisance parameter, is greater than or equal to $n\alpha^0\sigma^2$, the asymptotic variance of $\sqrt{n}\hat{\mu}$, and likewise, the variance of any regular unbiased estimate of $\sqrt{n}\sigma$ is greater than or equal to $n\gamma^0\sigma^2$, the asymptotic variance of $\sqrt{n}\hat{\sigma}$ (see Cramér). The variances $n\alpha^0\sigma^2$ and $n\gamma^0\sigma^2$ depend upon r and n through $p = r/n$ only, but α^0 and γ^0 are functions of both r and n .

Let loss be defined as squared error divided by σ^2 and consider estimates of $\varphi = l\mu + m\sigma$ (l and m known constants) with expected loss invariant under transformations of location and scale. Such an estimate has expected loss (risk) independent of μ and σ for all μ and σ . It is desired to find an expression giving a lower bound for the risk of any regular invariant estimate $\bar{\varphi}$ of φ when $l = 1$, $m = 0$ or $m = 1$, $l = 0$.

The requirement of invariant risk prescribes a particular form for $\bar{\varphi}$. Let $R(\varphi, \bar{\varphi})$ represent the expected loss of $\bar{\varphi}$ in the general case in which $\varphi = l\mu + m\sigma$. $R(\varphi, \bar{\varphi})$ is independent of μ and σ for all values of μ and σ and is equal to

$$V(\bar{\varphi})/\sigma^2 + [E(\bar{\varphi} - \varphi)]^2/\sigma^2,$$

where $V(\bar{\varphi})$ is the variance of $\bar{\varphi}$ and $E(\bar{\varphi} - \varphi)$ is the bias of this estimate. Both terms are greater than or equal to zero so that each must be independent of μ and σ for all $\theta = (\mu, \sigma)$. Thus, since

$E(\bar{\varphi} - \varphi)$ is equal to $E[\bar{\varphi} - \mu - k\sigma]$, $\bar{\varphi}$ must be equal to $\mu^* + k\sigma^*$, where μ^* and σ^* are regular unbiased estimates of μ and σ , respectively, and k is independent of μ and σ for all θ . The risk of $\bar{\varphi}$ is therefore of the form

$$\frac{1}{\sigma^2} \left\{ k^2 V(\mu^*) + 2kC(\mu^*, \sigma^*) + k^2 V(\sigma^*) + [E(\mu^* + k\sigma^* - \mu - k\sigma)]^2 \right\},$$

where $V(\mu^*)$ is the variance of μ^* , $V(\sigma^*)$ is the variance of σ^* , and $C(\mu^*, \sigma^*)$ is the covariance of μ^* and σ^* . Furthermore,

$$\frac{1}{\sigma^2} V(\bar{\varphi}) = \frac{1}{\sigma^2} [k^2 V(\mu^*) + 2kC(\mu^*, \sigma^*) + k^2 V(\sigma^*)]$$

is independent of μ and σ for all θ . Therefore, $V(\mu^*)$, $C(\mu^*, \sigma^*)$, and $V(\sigma^*)$ are of the form α^2 , β^2 , and γ^2 , respectively, with α and γ positive, and for all μ and σ , either (1) α , β , and γ are all independent of μ and σ , (2) α is independent of μ and σ and $2k\beta(\mu, \sigma) = -k^2\gamma(\mu, \sigma)$, (3) γ is independent of μ and σ and $2k\beta(\mu, \sigma) = -k^2\alpha(\mu, \sigma)$ or (4) β is independent of μ and σ and $k^2\alpha(\mu, \sigma) = -k^2\gamma(\mu, \sigma)$. The estimate $\bar{\varphi}$ cannot, of course, be invariant if $V(\bar{\varphi}) = 0$ unless $\bar{\varphi} = \mu + k\sigma$ for all μ and σ .

One may now make use of the fact that the correlation coefficient of μ^* and σ^* is less than or equal to 1, which implies that $\beta^2 \leq \alpha\gamma$

and hence that $V(\tilde{\varphi})/\sigma^2 \leq l^2\alpha + |2lk\sqrt{\sigma\gamma}| + k^2\gamma$. Then, since $V(\tilde{\varphi})/\sigma^2$, l , and k are independent of μ and σ for all θ , if α is a constant, so is γ . Conversely, if γ is a constant, so is α . Also, $l^2\alpha > 0$ cannot be identically equal to $-k^2\gamma < 0$. Therefore α , β , and γ are all independent of μ and σ for all values of the parameters.

If $R(\varphi, \tilde{\varphi})$ is then minimized with respect to k , and the k which yields the minimum value for $R(\varphi, \tilde{\varphi})$ is substituted into the expression for $\tilde{\varphi}$, the resulting expression defines the best estimate $\tilde{\varphi}$ of φ among invariant estimates based on a given μ^* and σ^* . Since the minimizing k is equal to $(m-l\beta)/(1+\gamma)$, $\tilde{\varphi}$ is equal to $l\mu^* + [(m-l\beta)/(1+\gamma)]\sigma^*$ and $R(\varphi, \tilde{\varphi})$, the expected loss of $\tilde{\varphi}$, is equal to $l^2\alpha + 2lm\beta + m^2\gamma - (m\gamma + l\beta)^2/(1+\gamma)$.

The change in $R(\varphi, \tilde{\varphi})$ induced by changes in α , β , and γ , corresponding to changes in μ^* and σ^* , is now considered. Since $R(\varphi, \tilde{\varphi})$ cannot be negative, it is clearly smallest when α , β , and γ are all zero. Moreover, $\partial R(\varphi, \tilde{\varphi})/\partial\alpha$ is equal to $l^2 \geq 0$ and $\partial R(\varphi, \tilde{\varphi})/\partial\gamma$ is equal to $(m-l\beta)^2/(1+\gamma)^2 \geq 0$ so that $R(\varphi, \tilde{\varphi})$ is monotonically non-decreasing in both α and γ for fixed β . It can be shown, too, that for $m=1$, $l=0$ and for $l=1$, $m=0$, an increase in both α and γ will affect an increase in $R(\varphi, \tilde{\varphi})$, irrespective of any change in β .

Let $m = 1$, $l = 0$ so that $\varphi = \sigma$ and $\tilde{\varphi} = \tilde{\sigma}$. Then, since $\partial R(\varphi, \tilde{\varphi}) / \partial \beta = 2l(m-l\beta)/(1+\gamma)$, $R(\sigma, \tilde{\sigma})$ is monotonically increasing in γ , independently of changes in β . $R(\sigma, \tilde{\sigma})$ is also independent of α . Let $m = 0$, $l = 1$ so that $\varphi = \mu$ and $\tilde{\varphi} = \tilde{\mu}$. One may now again make use of the fact that $\beta^2 \leq \alpha\gamma$, which implies that $d\beta \leq |(\gamma/2\beta)d\alpha|$ and hence that $|\frac{\partial R}{\partial \beta} d\beta| = |[2\beta/(1+\gamma)]d\beta| \leq [\gamma/(1+\gamma)]|d\alpha|$. Then, $dR(\mu, \tilde{\mu}) \geq d\alpha - [\gamma/(1+\gamma)]|d\alpha| + [\beta^2/(1+\gamma)^2]d\gamma$ or $dR(\mu, \tilde{\mu}) \geq [1-\gamma/(1+\gamma)]d\alpha + [\beta^2/(1+\gamma)^2]d\gamma > 0$ for $d\alpha > 0$ and $d\gamma > 0$. Thus, an increase in both α and γ induces an increase in $R(\mu, \tilde{\mu})$. Therefore, the expected squared error of $\tilde{\mu}$, any regular invariant estimate of μ , is greater than or equal to $[\alpha^0 - \beta^{0^2}/(1+\gamma^0)]\sigma^2$ (where $n\beta^0$ is the asymptotic covariance of $\sqrt{n}\hat{\mu}$ and $\sqrt{n}\hat{\sigma}$), and the mean squared deviation of $\tilde{\sigma}$, any regular invariant estimate of σ , is greater than or equal to $[\gamma^0/(1+\gamma^0)]\sigma^2$, since $\gamma \geq \gamma^0$ and $\alpha \geq \alpha^0$.

In order to apply this result to the parameters of the extreme-value distribution, we let μ be the location parameter x_R (see footnote, p. 12) and σ be the scale parameter b . All regularity conditions are satisfied, and the asymptotic variance of the maximum-likelihood estimate of $\sqrt{n}x_R$ (corresponding to $n\alpha^0\sigma^2$) is $n[A^0 + 2B^0 \log \log(1/R) + C^0(\log \log(1/R))^2]b^2$. Likewise, $n[B^0 + C^0 \log \log(1/R)]b^2$ corresponds to $n\beta^0\sigma^2$ and nC^0b^2 corresponds to $n\gamma^0\sigma^2$. Therefore, the expected squared deviations of any regular

Invariant estimates of x_R and of b are less than or equal to

$$\begin{aligned}\tilde{Q}_R^0 b^2 &= \{A^0 + 2B^0 \log \log(1/R) + C^0 (\log \log(1/R))^2 \\ &\quad - (B^0 + C^0 \log \log(1/R))^2 / (1+C^0)\} b^2 \\ &= \{\tilde{A}^0 + 2\tilde{B}^0 \log \log(1/R) + \tilde{C}^0 (\log \log(1/R))^2\} b^2\end{aligned}$$

and $[C^0/(1+C^0)]b^2 \equiv \tilde{C}^0 b^2$, respectively.

APPENDIX D.2

CRAMÉR-RAO LOWER BOUNDS FOR ESTIMATES WITH GIVEN BIAS WHEN A NUISANCE PARAMETER IS PRESENT AND THE SAMPLE IS CENSORED

Let Y_1, Y_2, \dots, Y_r be the first r order statistics of a size n random sample chosen from a population with density $f_\theta(x)$, where $\theta = (\theta_1, \theta_2)$, and let the joint density of Y_1, Y_2, \dots, Y_r be given by $h_\theta(y_1, y_2, \dots, y_r)$. Suppose that all regularity conditions for $f_\theta(x)$ are satisfied (see Halperin [4]) so that the maximum-likelihood estimates $\hat{\theta}_1$ and $\hat{\theta}_2$ of θ_1 and θ_2 , respectively, based on Y_1, Y_2, \dots, Y_r , converge in probability to the true values as $n \rightarrow \infty$ with $p = r/n$ fixed. Moreover, the concentration ellipse of the joint asymptotic distribution of $\hat{\theta}_1$ and $\hat{\theta}_2$ lies wholly within the concentration ellipse of any pair of regular unbiased estimates of θ_1 and θ_2 . Under the same conditions, the asymptotic covariance matrix of the maximum-likelihood estimates of $\sqrt{n}\theta_1$ and $\sqrt{n}\theta_2$ is \underline{D}^{-1} where

$$\underline{D} = \{d_{i,j}\} = \lim_{\substack{n \rightarrow \infty \\ p \text{ fixed}}} \{\lambda_{i,j}/n\},$$

and

$$\lambda_{i,j} = -E \left[\frac{\partial^2 \log h_\theta(y_1, y_2, \dots, y_r)}{\partial \theta_i \partial \theta_j} \right].$$

Regular estimation of θ_1 and θ_2 is defined as in Halperin [4] and Cramér [2]. It is supposed that Y_1, Y_2, \dots, Y_r can be transformed to new variables $\lambda_1, \lambda_2, \dots, \lambda_{r-2}, \bar{\theta}_1, \bar{\theta}_2$ such that

$$h_{\theta}(y_1, y_2, \dots, y_r) \prod_{i=1}^r dy_i = g_{\theta}(\bar{\theta}_1, \bar{\theta}_2) q_{\theta}(\lambda_1, \lambda_2, \dots, \lambda_{r-2} | \bar{\theta}_1, \bar{\theta}_2) \prod_{i=1}^{r-2} d\lambda_i d\bar{\theta}_1 d\bar{\theta}_2,$$

where $g_{\theta}(\bar{\theta}_1, \bar{\theta}_2)$ is the joint density function of $\bar{\theta}_1$ and $\bar{\theta}_2$ and $q_{\theta}(\lambda_1, \lambda_2, \dots, \lambda_{r-2} | \bar{\theta}_1, \bar{\theta}_2)$ is the conditional density of $\lambda_1, \lambda_2, \dots, \lambda_{r-2}$ given $\bar{\theta}_1$ and $\bar{\theta}_2$. If $\partial h / \partial \theta_j$, $\partial q / \partial \theta_j$, and $\partial g / \partial \theta_j$ exist for every θ_j and if

$$\frac{\partial h}{\partial \theta_j} < H_0(y_1, y_2, \dots, y_r), \quad \frac{\partial q}{\partial \theta_j} < G_0(\bar{\theta}_1, \bar{\theta}_2), \quad \frac{\partial g}{\partial \theta_j} < M_0(\lambda_1, \lambda_2, \dots, \lambda_{r-2}, \bar{\theta}_1, \bar{\theta}_2),$$

$j = 1, 2$, where H_0 ; $\bar{\theta}_1 G_0$, $\bar{\theta}_2 G_0$, and G_0 ; and M_0 are integrable over the whole space of (y_1, y_2, \dots, y_r) ; $\bar{\theta}_1, \bar{\theta}_2$; and $\bar{\theta}_1, \bar{\theta}_2, \lambda_1, \lambda_2, \dots, \lambda_{r-2}$, respectively, then $\bar{\theta}_1$ and $\bar{\theta}_2$ will be called regular joint estimates of θ_1 and θ_2 .

The variance of any regular unbiased estimate of θ_1 is greater than or equal to $\frac{1}{n} d_{1,1}^{-1}$, the asymptotic variance of $\sqrt{n} \hat{\theta}_1$ (see Cramér, p. 494).

Furthermore, since a reparameterization of $f_{\theta}(x)$ may give

$\theta = (\eta(\theta_1, \theta_2), \theta_2)$, the variance of any regular unbiased estimate of

$\eta(\theta_1, \theta_2)$, η nonsingular, is less than that of $\sqrt{n}\eta(\hat{\theta}_1, \hat{\theta}_2)$ for $n \rightarrow \infty$.

It can now be shown that the following is true of the mean squared error (MSE) of $\bar{\theta}_1$, any regular estimate of θ_1 . If $\bar{\theta}_1$ is a regular estimate of θ_1 and the bias of $\bar{\theta}_1$ is $k_1\theta_1$, with k_1 independent of θ , then $MSE(\bar{\theta}_1) \geq \frac{1}{n}(1+k_1)^2 d_{1,1}^{-1} + (k_1\theta_1)^2$.

If the bias of θ_1 is $k_2\theta_2$, with k_2 independent of θ , then $MSE(\bar{\theta}_1) \geq \frac{1}{n}(d_{1,1}^{-1} + 2k_2 d_{1,2}^{-1} + k_2^2 d_{2,2}^{-1}) + (k_2\theta_2)^2$.

Proof:

If $\bar{\theta}_1$ has bias $k_1\theta_1$, then $E(\bar{\theta}_1) = \theta_1 + k_1\theta_1 = (1+k_1)\theta_1$. If a re-parameterization is made so that $\theta = ((1+k_1)\theta_1, \theta_2)$, then, since $h_{\theta_1, \theta_2}(y_1, y_2, \dots, y_r) = h_{(1+k_1)\theta_1, \theta_2}(y_1, y_2, \dots, y_r)$, $\sqrt{n}\bar{\theta}_1$ is by definition a regular unbiased estimate of $\sqrt{n}(1+k_1)\theta_1$ with variance greater than or equal to the variance of the maximum-likelihood estimate of $\sqrt{n}(1+k_1)\theta_1$ as $n \rightarrow \infty$, p fixed.

If $\bar{\theta}_1$ has bias $k_2\theta_2$, then $E(\bar{\theta}_1) = \theta_1 + k_2\theta_2$ and $\sqrt{n}\bar{\theta}_1$ is a regular unbiased estimate of $\sqrt{n}(\theta_1 + k_2\theta_2)$ with variance greater than or equal to the maximum-likelihood estimate of this parametric function of θ_1 and θ_2 as $n \rightarrow \infty$, p fixed. Then since the maximum-likelihood estimate of $c_1\theta_1 + c_2\theta_2$ is $c_1\hat{\theta}_1 + c_2\hat{\theta}_2$, with variance $c_1^2 \text{Var}(\hat{\theta}_1) + 2c_1c_2 \text{Cov}(\hat{\theta}_1, \hat{\theta}_2) + c_2^2 \text{Var}(\hat{\theta}_2)$, $MSE(\bar{\theta}_1) \geq \frac{1}{n}(1+k_1)^2 d_{1,1}^{-1} + (k_1\theta_1)^2$

when $E(\bar{\theta}_1) = (1+k_1)\theta_1$, and $MSE(\bar{\theta}_1) \geq \frac{1}{n}(d_{1,1}^{-1} + 2k_2 d_{1,2}^{-1} + k_2^2 d_{2,2}^{-1}) + (k_2 \theta_2)^2$
 when $E(\bar{\theta}_1) = \theta_1 + k_2 \theta_2$.

It should be noted that this result agrees with one concerning more general forms of bias, which could be fairly directly derived for the uncensored case on the basis of a lemma of Hodges appearing in [6]. If this derivation is made for the case of a single unknown parameter ($\theta = \theta_1$, with $E(\bar{\theta}_1) = \theta + \text{bias}$ as it is in [5] for a Gaussian distribution with unknown σ , the bound obtained is larger than that given by Cramér in [2] for the single-parameter case.

For the problem considered in this paper all regularity conditions are

satisfied. The parameter point $\theta = (\theta_1, \theta_2)$ is given by

$\theta_1 = x_R = u + b \log \log(1/R)$ and $\theta_2 = b$, and the prescribed bias is $[-(B+C \log \log(1/R)/(1+C))] b \equiv k_2 b$, with k_2 a function of R , r , and n .

The covariance matrix $\frac{1}{n} D^{-1}$ for joint efficient estimates of x_R and b is

$$\begin{bmatrix} [A^0 + 2B^0 \log \log(1/R) + C^0 \log^2 \log(1/R)]b^2 & [B^0 + C^0 \log \log(1/R)]b^2 \\ [B^0 + C^0 \log \log(1/R)]b^2 & C^0 b^2 \end{bmatrix}$$

Thus, the Cramér-Rao lower bound for mean squared error of estimates

of x_R with bias $k_2 b$, is

$$\left\{ A^0 - \frac{2BB^0(1+C) - B^2(1+C^0)}{(1+C)^2} + \frac{2[B^0(1+C) + B(C-C^0)] \log \log(1/R)}{(1+C)^2} + \frac{(C^0+C^2)(\log \log(1/R))^2}{(1+C)^2} \right\} b^2$$

Likewise, the corresponding bound for estimates of $b(\theta_1=b, \theta_2=x_R)$

with bias $[-C/(1+C)]b \equiv k_1 b$ is $[(C^0+C^2)/(1+C)^2]b^2$.

Table D.I - Factors for Calculating Cramér-Rao Efficiencies of BLI Estimates of a Scale Parameter
and $100(1-R)$ Percent Points of the Extreme-Value Distribution, $R = e^{-1}$, .90, .99,
Where $\frac{1-r}{n}$ of the Size n Ordered Sample is Censored From Above, $2 \leq n \leq 25$, $2 \leq r \leq n$

n	r	\tilde{A}	\tilde{A}^0	B	\tilde{B}^0	\tilde{C}	\tilde{C}^0	$\tilde{Q}_{.90}$	$\tilde{Q}_{.90}^0$	$\tilde{Q}_{.99}$	$\tilde{Q}_{.99}^0$
2	2	0.657130	0.541667	0.037574	-0.098554	0.415839	0.233107	2.593897	2.165725	1.1166	6.311769
3	2	0.795461	0.510573	0.257510	0.054933	0.450055	0.285418	1.915628	1.703733	7.950090	6.045004
3	3	0.462407	0.363452	-0.013422	-0.071238	0.256346	0.163498	1.783495	1.537373	5.996531	4.5114504
4	2	1.014778	0.589262	0.413509	0.163705	0.464388	0.300232	1.505415	1.372892	7.037457	5.434456
4	3	0.423151	0.333607	0.084776	0.007460	0.281729	0.203175	1.468320	1.378941	5.604971	4.564433
4	4	0.292477	0.273587	-0.024312	-0.055778	0.183862	0.131931	1.351007	1.192743	4.443728	3.578594
5	2	1.249210	0.698349	0.531791	0.247140	0.472308	0.307934	1.238599	1.145458	6.332866	4.940891
5	3	0.490293	0.356132	0.166129	0.070090	0.294192	0.215413	1.232423	1.131607	5.187363	4.269817
5	4	0.290628	0.250441	0.030763	-0.008314	0.202419	0.155572	1.177251	1.080768	4.291067	3.640222
5	5	0.230405	0.219377	-0.029135	-0.045832	0.142843	0.108405	1.084913	0.974634	3.521210	2.915043
6	2	1.481024	0.816546	0.631490	0.314617	0.477311	0.312700	1.056183	0.984097	5.772317	4.519131
6	3	0.575395	0.399459	0.237697	0.121773	0.301733	0.222413	1.056108	0.979975	4.819592	3.940287
6	4	0.315821	0.256166	0.080351	0.032039	0.212423	0.165465	1.024624	0.954972	4.071425	3.41425
6	5	0.223513	0.201595	0.008880	-0.014275	0.155905	0.126963	0.974134	0.908072	3.462147	3.017064
6	6	0.190304	0.183111	-0.027716	-0.038896	0.116577	0.092009	0.905408	0.824072	2.912221	2.417804
7	2	1.704680	0.936056	0.713666	0.371176	0.480823	0.315950	0.927623	0.865509	5.313623	4.207061
7	3	0.667587	0.452368	0.288854	0.164384	0.306813	0.227011	0.921279	0.852136	4.577628	3.743943
7	4	0.353402	0.275604	0.122608	0.066457	0.218847	0.172496	0.909847	0.850044	3.856465	3.314435
7	5	0.233167	0.201413	0.042126	0.013809	0.164973	0.134936	0.879020	0.822600	3.336658	2.929802
7	6	0.162699	0.169194	-0.001301	-0.016396	0.127606	0.104382	0.834770	0.741725	2.894988	2.571237
7	7	0.162191	0.157140	-0.025789	-0.033783	0.098365	0.079907	0.776397	0.713852	2.480999	2.158902
8	2	1.918615	1.053689	0.784533	0.419916	0.483377	0.318312	0.835503	0.776196	4.929591	3.927166
8	3	0.761587	0.509725	0.337341	0.201542	0.310477	0.230278	0.816007	0.768871	4.229463	3.578477
8	4	0.398056	0.307514	0.159281	0.096310	0.223358	0.176631	0.812293	0.763536	3.659187	3.154194
8	5	0.251921	0.210552	0.071292	0.038447	0.170378	0.140089	0.793878	0.746945	3.201459	2.871310
8	6	0.165598	0.164819	0.022472	0.004152	0.134224	0.111074	0.764590	0.720759	2.819615	2.521431
8	7	0.155051	0.146009	-0.005413	-0.016979	0.107264	0.091458	0.727116	0.685586	2.493909	2.271706
8	8	0.141360	0.137624	-0.023866	-0.029859	0.085017	0.070624	0.679311	0.629661	2.160004	1.906837
9	2	2.122722	1.169113	0.845804	0.462458	0.485330	0.320106	0.769266	0.707781	4.602115	3.617256

Table D.I (continued)

n	r	λ	\bar{A}	\bar{B}	\bar{B}^0	\bar{C}	\bar{C}^0	$\bar{Q}_{.90}$	$\bar{Q}_{.90}$	$\bar{Q}_{.99}$	$\bar{Q}_{.99}$
10	3	0.556217	0.568920	0.379959	0.214151	0.313246	3.237724	0.732451	0.693619	3.989204	3.339422
	4	0.446256	0.333664	0.191609	0.122602	0.226713	0.174627	0.731980	0.691703	3.490942	3.007594
	5	0.276050	0.225294	0.097154	0.060297	0.174294	0.143739	0.721440	0.681829	3.070514	2.712754
	6	0.195796	0.171019	0.043783	0.022614	0.138801	0.117496	0.701653	0.664259	2.730209	2.449346
	7	0.155472	0.142875	0.011395	-0.001303	0.112788	0.097927	0.675362	0.640431	2.437388	2.209473
	8	0.134568	0.128541	-0.009069	-0.016845	0.092364	0.080125	0.643529	0.610124	2.172946	1.979095
	9	0.125295	0.122421	-0.022094	-0.026751	0.074824	0.063273	0.603654	0.563247	1.911954	1.707493
	10	2.317441	1.278815	0.902322	0.500402	0.486871	0.321517	0.721920	0.654849	4.318679	3.478710
	11	0.949076	0.628545	0.417951	0.263181	0.315415	0.236226	0.665298	0.632219	3.778412	3.172216
11	2	0.456157	0.367223	0.220478	0.146098	0.229309	0.181987	0.651139	0.631462	3.320224	2.874511
	3	0.303445	0.243550	0.120331	0.079870	0.177275	0.146480	0.659619	0.625873	2.947760	2.608416
	4	0.209739	0.179442	0.062998	0.039269	0.142198	0.120708	0.646313	0.613982	2.639246	2.372490
	5	0.160661	0.144537	0.027627	0.013021	0.116706	0.107917	0.627333	0.596994	2.376135	2.160288
	6	0.134036	0.125239	0.004750	-0.004510	0.097048	0.084935	0.604125	0.575665	2.144009	1.964086
	7	0.119657	0.114879	-0.010439	-0.016385	0.081004	0.071240	0.576856	0.549392	1.929854	1.773149
	8	0.112522	0.110244	-0.020509	-0.024229	0.066793	0.057309	0.543773	0.509513	1.714628	1.545802
	9	2.503400	1.385672	0.952399	0.534571	0.488120	0.322655	0.688620	0.613693	4.070337	3.295284
	10	1.039956	0.687812	0.452207	0.289327	0.317159	0.236149	0.610933	0.581526	3.591040	3.023166
	11	0.546820	0.402057	0.245536	0.167212	0.231380	0.183928	0.608972	0.580457	3.174938	2.753762
	12	0.232828	0.264051	0.141299	0.097568	0.179627	0.148622	0.606576	0.577570	2.833985	2.511448
12	2	0.226409	0.190689	0.087450	0.054395	0.144934	0.123168	0.597787	0.569612	2.551136	2.296637
	3	0.169057	0.149433	0.042460	0.026121	0.119670	0.103752	0.583381	0.557288	2.317788	2.104655
	4	0.136694	0.125541	0.017517	0.006912	0.100438	0.088773	0.566508	0.541461	2.170976	1.929932
	5	0.118094	0.111660	0.005984	-0.006435	0.085031	0.075398	0.546077	0.527451	1.912100	1.766389
	6	0.107564	0.103886	-0.011097	-0.015782	0.072072	0.064995	0.522494	0.499503	1.734804	1.605419
	7	0.102120	0.100270	-0.019102	-0.022142	0.060304	0.052372	0.493479	0.465144	1.553971	1.412241
	8	2.681270	1.488744	0.997998	0.565642	0.489152	0.323593	0.666682	0.581665	3.850507	3.132344
	9	1.128571	0.746274	0.483387	0.313099	0.318594	0.237396	0.566382	0.539313	3.423147	2.889310
	10	0.557480	0.437605	0.270268	0.186462	0.233072	0.185325	0.561389	0.536906	3.043061	2.643942
	11	0.363389	0.285989	0.160426	0.113702	0.181531	0.150346	0.560657	0.535624	2.728878	2.421431
	12	0.244901	0.203866	0.096410	0.068224	0.146945	0.125121	0.555138	0.530442	2.467467	2.221921
	13	0.175679	0.156593	0.056079	0.038150	0.122006	0.105955	0.545139	0.521483	2.245549	2.047843
13	2	0.141866	0.128363	0.029301	0.017474	0.103043	0.090789	0.531815	0.509488	2.052977	1.889820
	3	0.119300	0.111217	0.010873	0.002876	0.087994	0.078335	0.515978	0.494975	1.881336	1.742441
	4	0.105732	0.100852	-0.002108	-0.007594	0.075575	0.067727	0.497941	0.478014	1.724395	1.607928
	5	0.097752	0.094840	-0.011349	-0.015130	0.064873	0.058229	0.477356	0.457815	1.574960	1.466240
	6	0.093484	0.091952	-0.017855	-0.020386	0.054954	0.049218	0.452143	0.427886	1.420669	1.299863
14	2	2.851697	1.588181	1.039851	0.594124	0.490018	0.324379	0.653132	0.556893	3.654220	2.986373
	3	1.214809	0.803682	0.511988	0.334886	0.319794	0.239437	0.529969	0.503931	3.271836	2.768285
	4	0.647783	0.473311	0.292046	0.204114	0.234481	0.186567	0.520808	0.499452	2.922805	2.543413
	5	0.363389	0.285989	0.160426	0.113702	0.181531	0.150346	0.560657	0.535624	2.728878	2.421431

Table D.I (continued)

n	r	$\tilde{\lambda}$	$\tilde{\lambda}^0$	\tilde{B}	\tilde{B}^0	\tilde{C}	\tilde{C}^0	$\tilde{a}_{.90}$	$\tilde{a}_{.90}^0$	$\tilde{a}_{.99}$	$\tilde{a}_{.99}^0$
14	5	0.394596	0.308826	0.177997	0.178515	0.183107	0.151765	0.520760	0.493979	2.631767	2.338017
	6	0.264610	0.216375	0.111099	0.040946	0.148678	0.124713	0.517508	0.495757	2.398688	2.155087
	7	0.151873	0.165371	0.068647	0.049250	0.123901	0.107735	0.510365	0.489755	2.187220	1.992073
	8	0.148850	0.133011	0.040225	0.077262	0.105124	0.092774	0.500174	0.480133	2.003340	1.845417
	9	0.127503	0.112771	0.020463	0.011565	0.090307	0.080581	0.487707	0.468795	1.845150	1.711574
	10	0.106018	0.100000	0.005357	0.000136	0.078188	0.070333	0.473422	0.455568	1.702161	1.587102
	11	0.095836	0.092025	-0.003882	-0.008278	0.067951	0.061433	0.457474	0.440387	1.569496	1.469187
	12	0.085619	0.097267	-0.011361	-0.014474	0.058952	0.053330	0.439298	0.427477	1.441661	1.348953
	13	0.066197	0.084908	-0.015749	-0.018889	0.050470	0.044674	0.417168	0.396155	1.308307	1.204054
	2	3.015280	1.684168	1.078521	0.620412	0.490757	0.325048	0.646410	0.537950	3.477651	2.954650
	3	1.258658	0.859900	0.539401	0.354989	0.320813	0.239318	0.500102	0.474133	3.134045	2.658196
	4	0.697482	0.508933	0.312161	0.220407	0.235672	0.197613	0.496007	0.467042	2.812646	2.451277
15	5	0.426096	0.332701	0.194239	0.142200	0.184433	0.152955	0.485874	0.466785	2.541892	2.260660
	6	0.285120	0.233805	0.124694	0.092716	0.150126	0.128039	0.484164	0.454922	2.314764	2.090263
	7	0.205184	0.175323	0.080303	0.059542	0.125473	0.109198	0.479179	0.460339	2.121560	1.938311
	8	0.157165	0.139010	0.050382	0.036365	0.106830	0.094389	0.471412	0.455341	1.954311	1.801842
	9	0.127191	0.115813	0.029417	0.019680	0.092166	0.082373	0.461534	0.444389	1.876897	1.677880
	10	0.100035	0.100758	0.014307	0.007404	0.080248	0.072349	0.450028	0.433822	1.674554	1.563651
	11	0.095665	0.090956	0.003201	-0.001762	0.070275	0.063711	0.437146	0.421794	1.553345	1.456445
	12	0.087717	0.084662	-0.005064	-0.008659	0.061682	0.056179	0.422876	0.408139	1.439585	1.353162
	13	0.082762	0.080817	-0.011233	-0.013838	0.054001	0.049179	0.406790	0.392149	1.328853	1.248834
	14	0.079967	0.078867	-0.015764	-0.017595	0.046657	0.041616	0.387194	0.368807	1.212327	1.121401
	2	3.172565	1.776903	1.114456	0.644817	0.491393	0.325523	0.645184	0.523758	3.317793	2.735030
	3	1.380159	0.914668	0.562932	0.373646	0.321689	0.240074	0.475634	0.448958	3.008398	2.557510
16	4	0.746429	0.54285	0.330844	0.235531	0.236692	0.198508	0.456035	0.438853	2.711305	2.366408
	5	0.457646	0.355861	0.209333	0.154911	0.185564	0.153967	0.455220	0.438360	2.458518	2.188788
	6	0.306140	0.249862	0.137341	0.103661	0.151356	0.129160	0.454492	0.437357	2.245454	2.029348
	7	0.219292	0.186129	0.091160	0.069126	0.126799	0.110423	0.451135	0.434233	2.063840	1.896950
	8	0.166466	0.140023	0.059864	0.044861	0.108259	0.095733	0.445271	0.428919	1.906601	1.759124
	9	0.133001	0.119985	0.037798	0.027277	0.093708	0.081845	0.437435	0.421823	1.768246	1.643310
	10	0.111219	0.102740	0.021778	0.014237	0.081926	0.073974	0.428088	0.413279	1.644525	1.537151
	11	0.096811	0.091205	0.003895	0.004404	0.072125	0.065581	0.417529	0.403496	1.532039	1.438475
	12	0.087233	0.083498	-0.007546	-0.003094	0.063764	0.058273	0.405886	0.392530	1.477865	1.345114
	13	0.080922	0.078435	-0.005852	-0.008842	0.056441	0.051732	0.393087	0.380210	1.329130	1.254505
	14	0.076857	0.075267	-0.011021	-0.013232	0.049802	0.045619	0.378709	0.365845	1.232185	1.162377
	15	0.074578	0.073629	-0.014882	-0.016467	0.043376	0.039350	0.361223	0.344992	1.129400	1.049367
	2	3.374042	1.866582	1.148015	0.667589	0.491948	0.326124	0.648429	0.513482	3.172252	2.525796
17	3	1.459384	0.969564	0.585828	0.391049	0.322450	0.240730	0.455667	0.427651	2.893086	2.464975
	4	0.794533	0.579246	0.348282	0.249640	0.237577	0.189281	0.430136	0.414232	2.617694	2.287932
	5	0.489080	0.379630	0.223426	0.166774	0.186542	0.154939	0.428174	0.413151	2.380970	2.121862
	6	0.327462	0.266338	0.149158	0.113883	0.152413	0.130121	0.427986	0.412732	2.180440	1.972116

Table D.I (continued)

n	r	\bar{A}	\bar{B}	\bar{B}^0	\bar{C}	\bar{C}^0	$\bar{Q}_{.90}$	$\bar{Q}_{.90}^0$	$\bar{Q}_{.99}$	$\bar{Q}_{.99}^0$
17	7	0.233962	0.197559	0.101317	0.078089	0.127935	0.111476	0.425841	0.410632	1.838101
	8	0.176502	0.153801	0.063748	0.052820	0.109474	0.096871	0.421479	0.406641	1.717743
	9	0.139668	0.125027	0.045646	0.034409	0.095010	0.085081	0.415247	0.401021	1.608874
	10	0.115350	0.105673	0.029811	0.020672	0.083327	0.075321	0.407662	0.394070	1.509374
	11	0.098579	0.092471	0.016271	0.010235	0.073645	0.057061	0.398923	0.386015	1.417414
	12	0.081840	0.083414	0.006658	0.002700	0.065435	0.059925	0.389248	0.376982	1.331270
	13	0.068253	0.077277	-0.000690	-0.004038	0.058318	0.053626	0.379691	0.366971	1.249183
	14	0.075144	0.073080	-0.005373	-0.008896	0.051997	0.047921	0.367148	0.355797	1.168994
	15	0.071822	0.070436	-0.010763	-0.012662	0.046198	0.042533	0.354714	0.342818	1.086989
	16	0.069870	0.069043	-0.014090	-0.015476	0.040524	0.036605	0.339505	0.324067	0.986030
	17	3.470154	1.953397	1.179492	0.688931	0.492435	0.326564	0.555343	0.506458	2.525559
	2	1.536424	1.025943	0.607291	0.407353	0.273118	0.241304	0.439488	0.405612	2.379560
	3	0.841748	0.613738	0.364627	0.262858	0.238351	0.193954	0.407704	0.392652	2.215105
	4	0.520284	0.403381	0.216640	0.177893	0.187394	0.155594	0.404224	0.390757	2.059385
	5	0.348935	0.283079	0.160744	0.123470	0.153333	0.130955	0.404222	0.390539	1.918302
	6	0.249022	0.209440	0.110854	0.086502	0.128918	0.112381	0.402952	0.389232	1.791735
	7	0.187087	0.142160	0.077098	0.060299	0.110521	0.097848	0.399782	0.386286	1.677088
	8	0.146994	0.130745	0.053074	0.041123	0.096125	0.084134	0.394914	0.381855	1.575110
	9	0.120222	0.109354	0.035446	0.026742	0.084518	0.076458	0.388700	0.376189	1.491276
	10	0.101951	0.094542	0.022205	0.015752	0.074923	0.068296	0.381431	0.369509	1.394857
	11	0.089306	0.084187	0.012082	0.007231	0.066819	0.061278	0.373307	0.361964	1.314391
	12	0.080496	0.076929	0.004239	0.000556	0.059836	0.055132	0.364436	0.351625	1.238497
	13	0.074368	0.071875	-0.001893	-0.004707	0.053700	0.049644	0.354831	0.344462	1.165707
	14	0.070165	0.068427	-0.005708	-0.008864	0.048184	0.044620	0.344368	0.334293	1.094194
	15	0.067383	0.066192	-0.010479	-0.012128	0.043071	0.039833	0.332655	0.322495	1.020886
	16	0.065722	0.064995	-0.013375	-0.014597	0.038021	0.034526	0.318466	0.305536	0.929904
18	2	3.611296	2.037522	1.209127	0.709011	0.492867	0.326953	0.665289	0.502189	2.433176
	3	1.611373	1.072193	0.627488	0.422688	0.323709	0.241812	0.426524	0.394359	2.304406
	4	0.888051	0.647711	0.387007	0.275290	0.239034	0.197552	0.388245	0.373687	2.147296
	5	0.551180	0.427027	0.249075	0.188352	0.188145	0.156265	0.382952	0.370656	2.000918
	6	0.370449	0.299977	0.170682	0.132493	0.154141	0.131685	0.382849	0.370531	1.857639
	7	0.264342	0.221643	0.119838	0.094426	0.129778	0.113171	0.392194	0.369772	1.747755
	8	0.158079	0.170961	0.084973	0.067351	0.111433	0.098697	0.379953	0.367419	1.639981
	9	0.154829	0.136990	0.067068	0.047462	0.097092	0.077434	0.376167	0.364193	1.542305
	10	0.125678	0.113676	0.041720	0.032483	0.085544	0.077434	0.371113	0.359570	1.453395
	11	0.105764	0.097257	0.027976	0.020980	0.076015	0.069346	0.365054	0.354009	1.371693
	12	0.091459	0.085645	0.017236	0.012013	0.067949	0.062415	0.358191	0.347658	1.295909
	13	0.081467	0.077354	0.008940	0.004940	0.061101	0.056375	0.352656	0.340613	1.224875
	14	0.074363	0.071438	0.002403	-0.000695	0.055096	0.051023	0.342510	0.329739	1.157459
	15	0.069333	0.067247	-0.002784	-0.005180	0.049736	0.046194	0.333737	0.324497	1.092442
	16	0.065825	0.064345	-0.006912	-0.008774	0.044879	0.041735	0.324208	0.315185	1.024233
	17	0.063468	0.062634	-0.010185	-0.011629	0.040334	0.037451	0.313564	0.304428	0.961930

Table P I (continued)

n	π	\tilde{A}	A^0	\tilde{R}	B^0	\tilde{C}	\tilde{C}^0	$\tilde{A}_{.90}$	$\tilde{A}^0_{.90}$	$\tilde{Q}_{.99}$	$\tilde{Q}_{.99}$
18		0.062040	0.061395	-0.012727	-0.013813	0.035808	0.032670	0.300660	0.299009	0.936881	0.879824
19	2	3.747823	2.119125	1.237124	0.727969	0.493252	0.327330	0.677759	0.500225	2.803803	2.347701
	3	1.684328	1.122182	0.645559	0.437160	0.324735	0.242763	0.416309	0.381498	2.597033	2.226795
	4	0.933439	0.691137	0.394527	0.287022	0.239641	0.191080	0.371354	0.356545	2.374807	2.083964
	5	0.581713	0.450502	0.267817	0.198224	0.188811	0.155856	0.364011	0.352691	2.177511	1.945069
	6	0.391921	0.316930	0.180540	0.141012	0.154855	0.132330	0.363571	0.352414	2.007854	1.819871
	7	0.279225	0.234070	0.128329	0.101913	0.130537	0.113867	0.363111	0.352079	1.861508	1.706030
	8	0.209369	0.180055	0.092420	0.074019	0.112236	0.099442	0.361790	0.350548	1.734142	1.603441
	9	0.163059	0.143649	0.066689	0.053461	0.097939	0.083780	0.359887	0.347869	1.627076	1.510600
	10	0.131597	0.119371	0.047667	0.037923	0.086438	0.078283	0.354706	0.344125	1.522197	1.426040
	11	0.109693	0.100490	0.033260	0.025944	0.076962	0.070253	0.349747	0.339493	1.432318	1.348440
	12	0.094167	0.087661	0.022139	0.016562	0.068995	0.063387	0.343931	0.334127	1.350523	1.276543
	13	0.083028	0.078172	0.013424	0.009123	0.062177	0.057424	0.337487	0.328120	1.275284	1.209619
	14	0.074580	0.071621	0.006515	0.003148	0.056247	0.052164	0.330501	0.321549	1.205307	1.146419
	15	0.069158	0.066723	0.003992	-0.001630	0.051008	0.047463	0.323073	0.314421	1.139422	1.086109
	16	0.064570	0.063203	-0.003448	-0.005510	0.046301	0.043190	0.314961	0.306473	1.076475	1.027648
	17	0.062007	0.060731	-0.007023	-0.008447	0.044987	0.039192	0.306244	0.299123	1.015125	0.969646
	18	0.055588	0.059082	-0.009889	-0.011163	0.037918	0.035334	0.295518	0.292264	0.953366	0.909009
	19	0.058749	0.059173	-0.012138	-0.013178	0.033837	0.031004	0.286733	0.274179	0.886456	0.834962
20	2	3.880054	2.199359	1.263654	0.745922	0.493598	0.327610	0.492338	0.500230	2.699770	2.268339
	3	1.755385	1.171007	0.664622	0.450361	0.324706	0.242667	0.408459	0.370703	2.511890	2.158116
	4	0.977919	0.713999	0.408277	0.293128	0.240184	0.191552	0.356707	0.342256	2.304280	2.074644
	5	0.611448	0.473760	0.271937	0.207570	0.189405	0.157383	0.347111	0.336555	2.118028	1.894493
	6	0.413294	0.338890	0.187879	0.149080	0.155493	0.132905	0.346139	0.335971	1.956790	1.774758
	7	0.295395	0.246645	0.135375	0.109005	0.131212	0.114485	0.346085	0.335810	1.817334	1.664472
	8	0.220873	0.189479	0.093492	0.080340	0.112948	0.100102	0.345115	0.324823	1.695738	1.568626
	9	0.171590	0.150630	0.072972	0.059153	0.098688	0.088541	0.342932	0.329765	1.593595	1.480055
	10	0.137883	0.123496	0.053316	0.043091	0.087226	0.079028	0.339645	0.325909	1.493175	1.393385
	11	0.114237	0.104145	0.038381	0.030665	0.077792	0.071044	0.335446	0.325909	1.407307	1.325414
	12	0.097330	0.090131	0.024809	0.020805	0.067872	0.064230	0.330511	0.321357	1.327262	1.257096
	13	0.085074	0.079872	0.017704	0.013116	0.063107	0.058327	0.324979	0.316216	1.257633	1.193474
	14	0.076108	0.072313	0.010451	0.006856	0.057241	0.053140	0.318946	0.310563	1.191245	1.133747
	15	0.065519	0.066732	0.004619	0.001781	0.052079	0.048522	0.317464	0.304435	1.129077	1.077126
	16	0.064679	0.062625	-0.000103	-0.002355	0.047471	0.044351	0.305545	0.297826	1.070185	1.022826
	17	0.061149	0.059435	-0.003943	-0.005735	0.043295	0.040524	0.298147	0.290670	1.013603	0.969952
	18	0.058619	0.057509	-0.007047	-0.008495	0.039437	0.036936	0.294014	0.282790	0.958178	0.917274
	19	0.056874	0.056074	-0.009596	-0.010730	0.035771	0.033441	0.291214	0.273718	0.902127	0.862456
	20	0.055790	0.052773	-0.011599	-0.012472	0.032070	0.029500	0.277405	0.260797	0.841162	0.794273
21	2	4.008276	2.275345	1.288861	0.769972	0.493910	0.327991	0.708499	0.501921	2.602178	2.194419
	3	1.824638	1.218708	0.691776	0.463863	0.325131	0.243031	0.602656	0.361707	2.437309	2.093851
	4	1.021506	0.746293	0.421334	0.308659	0.240674	0.191977	0.344003	0.329254	2.238094	1.968936

Table D.I (continued)

n	r	\bar{A}	\bar{A}	\bar{B}	\bar{B}	\bar{C}	\bar{C}	$\bar{Q}_{.90}$	$\bar{Q}_{.90}$	$\bar{Q}_{.99}$
5	5	0.441562	0.496771	0.282496	0.218442	0.189940	0.157854	0.332008	0.322030	0.322030
6	6	0.43421	0.350804	0.198748	0.156740	0.156064	0.133419	0.330341	0.321014	0.321014
7	7	0.310996	0.255309	0.144020	0.115747	0.131817	0.115037	0.330340	0.320949	0.320949
8	8	0.222526	0.199047	0.106195	0.084347	0.113583	0.102690	0.329776	0.320332	0.320332
9	9	0.180354	0.157465	0.078949	0.064565	0.099355	0.089165	0.329174	0.319812	0.319812
10	10	0.144661	0.128424	0.054694	0.048009	0.087925	0.079483	0.325560	0.316397	0.316397
11	11	0.119117	0.108144	0.043260	0.035163	0.078525	0.071742	0.322081	0.313198	0.313198
12	12	0.100664	0.092077	0.031265	0.025931	0.070643	0.064370	0.317896	0.309338	0.309338
13	13	0.087520	0.081773	0.021794	0.016932	0.063921	0.059113	0.313137	0.304922	0.304922
14	14	0.077660	0.073428	0.014220	0.010389	0.058103	0.053980	0.307902	0.300031	0.300031
15	15	0.070325	0.067184	0.008101	0.005058	0.052999	0.049425	0.302258	0.294715	0.294715
16	16	0.064853	0.062510	0.003119	0.000696	0.048462	0.045333	0.296236	0.288995	0.288995
17	17	0.060780	0.059028	-0.002913	-0.000293	0.044377	0.041609	0.281835	0.282854	0.282854
18	18	0.057771	0.056462	-0.004312	-0.000883	0.040644	0.038168	0.281006	0.276225	0.276225
19	19	0.055591	0.054618	-0.007063	-0.008328	0.037172	0.034920	0.275625	0.268938	0.268938
20	20	0.054070	0.053359	-0.009311	-0.010325	0.033851	0.031739	0.267400	0.260560	0.260560
21	21	0.053114	0.052648	-0.011106	-0.011875	0.030478	0.028134	0.257444	0.248660	0.248660
22	22	4.132751	2.350272	1.312872	0.779203	0.494193	0.328145	0.725532	0.505062	0.505062
3	3	1.892175	1.265330	0.698109	0.476747	0.325516	0.243360	0.398635	0.354293	0.354293
4	4	1.064221	0.778020	0.433762	0.318701	0.241116	0.192361	0.334022	0.317776	0.317776
5	5	0.670241	0.519511	0.292547	0.224895	0.190423	0.1549283	0.314495	0.305937	0.305937
6	6	0.455570	0.367635	0.207197	0.164031	0.156580	0.133883	0.315997	0.307377	0.307377
7	7	0.326583	0.272016	0.151300	0.122157	0.132361	0.115534	0.315017	0.307302	0.307302
8	8	0.244276	0.208746	0.112590	0.092058	0.114155	0.101218	0.315636	0.306952	0.306952
9	9	0.189291	0.165296	0.084646	0.069725	0.099953	0.089723	0.314501	0.305850	0.305850
10	10	0.151270	0.134597	0.063824	0.052700	0.088550	0.080273	0.312448	0.303940	0.303940
11	11	0.124272	0.112423	0.047918	0.039457	0.079179	0.072363	0.309587	0.301297	0.301297
12	12	0.104705	0.096133	0.035523	0.028982	0.071328	0.065625	0.306039	0.299028	0.299028
13	13	0.090259	0.084008	0.025707	0.020584	0.064640	0.059806	0.301942	0.294224	0.294224
14	14	0.079566	0.074897	0.017831	0.013775	0.058860	0.054714	0.297303	0.290982	0.290982
15	15	0.071503	0.069007	0.011444	0.008205	0.053301	0.050208	0.292449	0.285342	0.285342
16	16	0.065417	0.062783	0.006220	0.003615	0.049317	0.046175	0.287168	0.280346	0.280346
17	17	0.060817	0.058824	0.001920	-0.000185	0.045297	0.042523	0.281564	0.275000	0.275000
18	18	0.057351	0.055841	-0.001636	-0.003344	0.041648	0.039176	0.275626	0.269283	0.269283
19	19	0.054763	0.053620	-0.004584	-0.005971	0.038291	0.036063	0.269303	0.263124	0.263124
20	20	0.052867	0.052007	-0.007025	-0.008152	0.035147	0.033108	0.262474	0.256365	0.256365
21	21	0.051532	0.050895	-0.009034	-0.009947	0.032123	0.030200	0.254969	0.248601	0.248601
22	22	0.050684	0.050261	-0.010652	-0.011369	0.029036	0.026890	0.245669	0.237603	0.237603
23	23	4.253712	2.423202	1.335793	0.794692	0.494451	0.323377	0.745637	0.509456	0.509456
3	3	1.958080	1.310915	0.713693	0.488755	0.325866	0.243660	0.396172	0.349241	0.349241
4	4	1.106068	0.809186	0.445620	0.328269	0.241519	0.192709	0.373560	0.307645	0.307645
5	5	0.659679	0.541966	0.302137	0.22937	0.190862	0.158670	0.306394	0.297107	0.297107

Table D.I (continued)

n	x	\bar{A}	\bar{A}^0	\bar{B}	\bar{B}^0	\bar{C}	\bar{C}^0	$\bar{Q}_{.90}$	$\bar{Q}_{.90}^0$	$\bar{Q}_{.99}$	$\bar{Q}_{.99}^0$	
24	6	0.476419	0.384356	0.215249	0.170486	0.157047	0.134303	0.307951	0.294922	1.419400	1.653264	
	7	0.342171	0.284731	0.158244	0.128277	0.132854	0.115483	0.307691	0.294746	1.697565	1.558902	
	8	0.256081	0.213536	0.113695	0.097530	0.114671	0.101694	0.302579	0.294574	1.597657	1.473217	
	9	0.158354	0.112477	0.097086	0.074651	0.100492	0.090225	0.301811	0.293905	1.476090	1.395351	
	10	0.158261	0.140465	0.068726	0.057182	0.089113	0.080805	0.300226	0.292315	1.411714	1.324328	
	11	0.129648	0.116933	0.052372	0.043562	0.079766	0.072919	0.297892	0.290146	1.335768	1.259222	
	12	0.108799	0.099546	0.039599	0.032764	0.071940	0.066210	0.294892	0.287393	1.266935	1.199204	
	13	0.093354	0.086522	0.029457	0.024082	0.065280	0.060421	0.291367	0.284115	1.203767	1.143550	
	14	0.081768	0.076663	0.021296	0.017023	0.059532	0.055364	0.287400	0.280419	1.145620	1.091627	
	15	0.072595	0.069144	0.014656	0.011228	0.054507	0.050896	0.283064	0.276355	1.091605	1.042877	
	16	0.066309	0.063383	0.009206	0.006436	0.050065	0.046907	0.278409	0.271943	1.041048	0.996794	
	17	0.061196	0.058962	0.004700	0.002749	0.046093	0.043309	0.273465	0.267265	0.992351	0.952910	
	18	0.057287	0.055575	0.003954	-0.000984	0.042505	0.040028	0.268240	0.262262	0.947960	0.910758	
	19	0.054309	0.052997	-0.002171	-0.003676	0.039225	0.037003	0.262717	0.256926	0.904323	0.869839	
	20	0.052064	0.051059	-0.004782	-0.006016	0.034187	0.034172	0.256844	0.251190	0.861932	0.829545	
	21	0.050403	0.049639	-0.006961	-0.007973	0.033327	0.031472	0.250597	0.244902	0.819495	0.788986	
	22	0.049223	0.048650	-0.008758	-0.009594	0.030561	0.028801	0.243451	0.237696	0.776604	0.746396	
	23	0.048467	0.048081	-0.010233	-0.010887	0.027724	0.025751	0.234920	0.227488	0.729285	0.693172	
	25	2	4.371373	2.494265	1.357719	0.809501	0.474687	0.328589	0.765809	0.514936	2.348202	1.999995
		3	2.022432	1.355507	0.728596	0.499342	0.324187	0.243934	0.395076	0.343618	2.221495	1.923382
		4	1.147133	0.839800	0.456955	0.337413	0.241886	0.193028	0.315445	0.298714	2.051647	1.820220
		5	0.728075	0.564126	0.311304	0.240534	0.191267	0.159023	0.295559	0.286416	1.911353	1.715375
		6	0.457049	0.400946	0.222952	0.177634	0.157473	0.134495	0.291070	0.283528	1.774177	1.616781
		7	0.357586	0.297424	0.164892	0.134128	0.133303	0.116391	0.290514	0.283173	1.651394	1.526402
8		0.267908	0.228382	0.124535	0.102752	0.115140	0.102126	0.290500	0.283104	1.558681	1.444158	
9		0.207516	0.180572	0.095292	0.079364	0.100981	0.090680	0.290014	0.282503	1.447700	1.369317	
10		0.165394	0.146489	0.073418	0.061472	0.089622	0.081283	0.288817	0.281452	1.396447	1.300999	
11		0.135205	0.121632	0.056639	0.047494	0.080296	0.073421	0.286914	0.279696	1.313780	1.238352	
12		0.113101	0.103174	0.043505	0.036388	0.072492	0.066735	0.284405	0.277359	1.246867	1.190607	
13		0.096642	0.089271	0.033054	0.027439	0.065855	0.060972	0.281377	0.274551	1.186126	1.130171	
14		0.084221	0.078681	0.024673	0.020142	0.060132	0.055943	0.277921	0.271332	1.130171	1.077207	
15		0.074752	0.070546	0.017745	0.014136	0.055137	0.051507	0.274197	0.267763	1.079250	1.030447	
16		0.067480	0.064261	0.012081	0.009152	0.050726	0.047553	0.269990	0.263846	1.029765	0.986347	
17		0.061866	0.059390	0.007382	0.004990	0.046793	0.043996	0.265605	0.259731	0.984142	0.944488	
18		0.057525	0.055611	0.003460	0.001497	0.043249	0.040744	0.260971	0.255311	0.940898	0.904479	
19		0.054171	0.052687	0.001171	-0.001466	0.040024	0.037800	0.256089	0.250621	0.899565	0.865894	
20		0.051591	0.050441	-0.002595	-0.003930	0.037059	0.035051	0.250940	0.245632	0.859677	0.828321	
21		0.049628	0.048739	-0.004923	-0.006027	0.034297	0.032466	0.245470	0.240275	0.820690	0.791207	
22		0.048164	0.047479	-0.006980	-0.007792	0.031682	0.029787	0.239572	0.234609	0.791900	0.753742	
23		0.047114	0.046596	-0.009513	-0.009264	0.029142	0.027524	0.233006	0.227683	0.747112	0.714303	
24		0.046435	0.046083	-0.009845	-0.010445	0.026524	0.024705	0.225070	0.218199	0.698307	0.664959	
		2	4.485528	2.561561	1.378732	0.823689	0.494903	0.328783	0.786885	0.521362	2.274010	1.942874
	3	2.085306	1.399146	0.747872	0.510152	0.326481	0.244185	0.395186	0.339676	2.159445	1.872879	

Table D.I (continued)

r	\tilde{A}	\tilde{A}^0	\tilde{B}	\tilde{B}^0	\tilde{C}	\tilde{C}^0	$\tilde{Q}_{.90}$	$\tilde{Q}_{.90}^0$	$\tilde{Q}_{.99}$	$\tilde{Q}_{.99}^0$
4	1.187380	0.869873	0.467813	0.346170	0.242223	0.193319	0.309531	0.290854	2.009130	1.775911
5	0.756029	0.585987	0.320084	0.248003	0.191628	0.159346	0.285953	0.275765	1.846284	1.676272
6	0.517448	0.417388	0.230330	0.194000	0.157863	0.135035	0.280238	0.273088	1.738946	1.582048
7	0.372954	0.310074	0.171757	0.139731	0.133712	0.116763	0.279313	0.272489	1.626878	1.495380
8	0.279733	0.238258	0.130130	0.107755	0.115569	0.102520	0.279308	0.272456	1.528084	1.416337
9	0.216735	0.189350	0.100292	0.083881	0.101427	0.091095	0.279032	0.272141	1.440440	1.344306
10	0.172636	0.152637	0.077918	0.065585	0.090085	0.081718	0.278152	0.271288	1.362092	1.278495
11	0.140907	0.126486	0.067732	0.051266	0.080777	0.073875	0.276632	0.269864	1.291497	1.219118
12	0.117577	0.106481	0.047255	0.039867	0.072991	0.067211	0.274533	0.267915	1.227409	1.162461
13	0.100124	0.092218	0.036509	0.030662	0.066374	0.061469	0.271938	0.265506	1.158805	1.110893
14	0.086887	0.080913	0.027821	0.023141	0.060673	0.054454	0.269927	0.262703	1.111846	1.062962
15	0.076736	0.072174	0.020717	0.016934	0.055701	0.052053	0.265571	0.259563	1.064835	1.017888
16	0.068889	0.065378	0.014852	0.011770	0.051317	0.048128	0.261921	0.256132	1.019160	0.975543
17	0.062786	0.060066	0.009971	0.007443	0.047413	0.044603	0.258017	0.252441	0.974379	0.935445
18	0.058023	0.055904	0.005883	0.003799	0.043905	0.041410	0.253885	0.248512	0.932981	0.897240
19	0.054300	0.052645	0.002441	0.001901	0.040722	0.038491	0.249538	0.244350	0.893581	0.860586
20	0.051397	0.050101	-0.000468	-0.001901	0.037808	0.035799	0.244966	0.239946	0.855761	0.825136
21	0.049145	0.048130	-0.002932	-0.004124	0.035113	0.033288	0.240157	0.235270	0.819158	0.790503
22	0.047417	0.046624	-0.005020	-0.006013	0.032589	0.030917	0.235046	0.230256	0.793231	0.750195
23	0.046117	0.045502	-0.006786	-0.007512	0.030189	0.028634	0.229541	0.224769	0.747395	0.721472
24	0.045179	0.044708	-0.008269	-0.008954	0.027847	0.026357	0.223413	0.218483	0.710527	0.684837
25	0.044554	0.044243	-0.009386	-0.010037	0.025424	0.023740	0.215997	0.209638	0.669832	0.638952

Table D.II - Factors for Calculating Cramér-Rao Efficiencies of BLU Estimates of a Scale Parameter
and $100(1-R)$ Percent Points of the Extreme-Value Distribution, $R = e^{-1}$, .90, .99,
When $\frac{n-r}{n}$ of the Size n Ordered Sample is Censored From Above, $2 \leq n \leq 25$, $2 \leq r \leq n$

n	r	A	A^0	B	B^0	C	C^0	$Q_{.90}$	$Q_{.90}^0$	$Q_{.99}$	$Q_{.99}^0$
2	2	0.655547	0.554332	0.064322	-0.128511	0.711857	0.303364	3.975007	2.672744	15.131652	8.148960
3	2	0.516039	0.514756	0.468246	0.076874	0.818365	0.399419	2.952912	2.191524	13.925769	8.249781
3	3	0.402864	0.369555	-0.024772	-0.085674	0.344712	0.202642	2.260028	1.781363	7.925348	5.445973
4	2	1.334019	0.627559	0.772030	0.233942	0.847022	0.429045	2.250049	1.747407	12.579493	7.554420
4	3	0.433157	0.333677	0.118027	0.009362	0.392233	0.254980	1.888275	1.582802	7.647457	5.643279
4	4	0.293459	0.277166	-0.034670	-0.064256	0.225283	0.151982	1.590458	1.336022	5.379916	4.084480
5	2	1.789172	0.786604	1.011559	0.357105	0.895046	0.444949	1.769062	1.432654	11.422934	6.946842
5	3	0.529395	0.362392	0.235374	0.089321	0.416816	0.274556	1.580857	1.350778	7.184278	5.350604
5	4	0.291814	0.250523	0.033571	-0.009858	0.253791	0.185638	1.403454	1.234990	5.307521	4.269577
5	5	0.221395	0.221731	-0.033991	-0.051404	0.166647	0.121585	1.229305	1.068818	4.070604	3.267584
6	2	2.244005	0.960564	1.208225	0.457758	0.913293	0.454968	1.431160	1.204346	10.454506	6.376806
6	3	0.652941	0.418373	0.331249	0.155961	0.432116	0.285030	1.341378	1.164935	6.731123	5.036280
6	4	0.323719	0.257398	0.107022	0.038437	0.269716	0.199709	1.230427	1.095762	5.092651	4.129891
6	5	0.223607	0.201827	0.010533	-0.016292	0.186107	0.145295	1.118673	1.010952	4.064971	3.476370
6	6	0.191174	0.184777	-0.031373	-0.042837	0.131960	0.101321	1.000642	0.890691	3.272275	2.722987
7	2	2.685691	1.137462	1.374610	0.542615	0.926126	0.461881	1.189981	1.034331	9.636960	5.919293
7	3	0.787954	0.487326	0.416705	0.212661	0.442612	0.294779	1.153933	1.017435	6.320432	4.745446
7	4	0.372647	0.280941	0.156958	0.080311	0.280158	0.208454	1.084385	0.975126	4.857122	3.953224
7	5	0.235293	0.201634	0.050448	0.015963	0.197566	0.155984	1.008744	0.919716	3.951929	3.355507
7	6	0.187701	0.169495	-0.001401	-0.018348	0.146271	0.119046	0.930151	0.854945	3.271719	2.857493
7	7	0.162928	0.158381	-0.028603	-0.036717	0.109096	0.086847	0.844142	0.763441	2.734710	2.333989
8	2	3.109991	1.312232	1.518578	0.615848	0.735646	0.466946	1.013527	0.905150	8.938174	5.527468
8	3	0.927077	0.562496	0.489237	0.261937	0.450277	0.292170	1.005371	0.890081	5.954377	4.494368
8	4	0.430722	0.313780	0.205090	0.116971	0.287595	0.214523	0.964092	0.873701	4.629738	3.777210
8	5	0.256047	0.212771	0.085933	0.044711	0.205369	0.142912	0.911306	0.836048	3.813329	3.268352
8	6	0.186582	0.166839	0.024955	0.004491	0.155033	0.127490	0.854874	0.791401	3.228495	2.871640
8	7	0.155098	0.146327	-0.007184	-0.018688	0.120152	0.107665	0.795897	0.740220	2.763772	2.449474
8	8	0.141983	0.138583	-0.026083	-0.032128	0.092916	0.075991	0.729918	0.668011	2.348191	2.042740
9	2	3.515995	1.482672	1.645332	0.680191	0.942991	0.470518	0.886242	0.805608	8.333433	5.187875

Table D.II (continued)

n	r	A	A ⁰	B	B ⁰	C	C ⁰	Q _{.90}	Q ⁰ _{.90}	Q _{.99}	Q ⁰ _{.99}
10	3	1.066436	0.640376	0.553268	0.305172	0.456126	0.303312	0.862716	0.802898	5.628458	4.251204
	4	0.493734	0.351987	0.247785	0.149453	0.293180	0.210010	0.863227	0.788441	4.191130	3.611536
	5	0.287481	0.225540	0.117661	0.070418	0.111085	0.147868	0.826847	0.762713	3.671814	3.131981
	6	0.186222	0.171599	0.050839	0.025625	0.161172	0.133140	0.785409	0.730508	3.140912	2.753261
	7	0.155618	0.142877	0.012844	-0.001443	0.127127	0.107533	0.741601	0.693937	2.727624	2.431707
	8	0.135059	0.128850	-0.003992	-0.018312	0.101763	0.087105	0.695372	0.652381	2.380427	2.140585
	9	0.125823	0.123185	-0.023881	-0.028558	0.080876	0.067547	0.642873	0.593788	2.056979	1.815374
	10	3.504149	1.647877	1.759472	0.737531	0.948830	0.473876	0.194751	0.728229	7.804222	4.890250
	3	1.204241	0.719043	0.610517	0.343860	0.460738	0.305552	0.789717	0.723843	5.337162	4.042479
	4	0.559271	0.393302	0.286078	0.178553	0.297537	0.222474	0.778479	0.716327	4.223449	3.454421
11	5	0.321045	0.251024	0.145259	0.093577	0.215474	0.171618	0.753965	0.698961	3.535140	3.021768
	6	0.214365	0.181196	0.073442	0.044640	0.165771	0.137278	0.723311	0.675389	3.046613	2.675302
	7	0.161525	0.144726	0.031277	0.014493	0.132126	0.112245	0.689857	0.647968	2.659720	2.395734
	8	0.134061	0.125262	0.005260	-0.004929	0.107479	0.092819	0.654675	0.617495	2.350063	2.134789
	9	0.119776	0.115168	-0.011359	-0.017641	0.088144	0.076704	0.617274	0.583010	2.089530	1.900645
	10	0.112573	0.110866	-0.021976	-0.025702	0.071573	0.060793	0.574340	0.534409	1.829746	1.631792
	2	4.275424	1.807564	1.860590	0.789216	0.953583	0.476353	0.730491	0.667836	7.334566	4.624926
	3	1.399428	0.797401	0.662244	0.378774	0.464470	0.309156	0.710991	0.654256	5.075415	3.854744
	4	0.625897	0.436355	0.320751	0.204873	0.301033	0.225233	0.706758	0.645886	4.045166	3.317691
	5	0.357166	0.275232	0.172238	0.114600	0.218957	0.174566	0.690803	0.643481	3.405968	2.914349
12	6	0.233577	0.194064	0.094075	0.062036	0.169364	0.140469	0.668254	0.626713	2.952429	2.595931
	7	0.171105	0.150195	0.048232	0.029145	0.135937	0.115763	0.642433	0.605264	2.603978	2.331758
	8	0.137035	0.125594	0.019467	0.007531	0.111652	0.096820	0.614839	0.581781	2.320632	2.104685
	9	0.118095	0.111705	0.000638	-0.006940	0.092934	0.081546	0.585851	0.555994	2.078823	1.901371
	10	0.107657	0.104152	-0.011959	-0.016853	0.077670	0.069484	0.554854	0.526962	1.841324	1.704516
	11	0.102509	0.100788	-0.020327	-0.023366	0.064174	0.055266	0.518982	0.485826	1.647530	1.485265
	2	4.630570	1.961760	1.953610	0.836245	0.957528	0.478400	0.687358	0.620733	6.919783	4.391657
	3	1.471483	0.874822	0.709395	0.410565	0.467553	0.311297	0.646442	0.603434	4.818895	3.694979
	4	0.692724	0.480282	0.352403	0.228879	0.303903	0.227484	0.645664	0.602173	3.891525	3.184603
	5	0.394033	0.301204	0.196008	0.133821	0.221794	0.176050	0.635855	0.595013	3.284974	2.814515
13	6	0.255797	0.209186	0.113018	0.077981	0.172258	0.143015	0.619475	0.582467	2.941218	2.518140
	7	0.183261	0.156221	0.063872	0.042672	0.138960	0.119517	0.599505	0.566357	2.536204	2.273517
	8	0.142823	0.128699	0.032668	0.019218	0.114881	0.099855	0.577570	0.547891	2.273312	2.044045
	9	0.119429	0.111224	0.011922	0.003121	0.096484	0.084993	0.554380	0.527601	2.051474	1.881093
	10	0.105737	0.100913	-0.002280	-0.008146	0.081754	0.072648	0.532011	0.505476	1.856731	1.713185
	11	0.097890	0.095083	-0.012136	-0.016065	0.069373	0.061829	0.503829	0.480501	1.675777	1.551776
	12	0.093821	0.092399	-0.018894	-0.021419	0.058150	0.050661	0.473337	0.445341	1.498182	1.361493
	2	4.571948	2.110639	2.038996	0.879375	0.960854	0.480120	0.660883	0.584208	6.555579	4.180131
	3	1.600181	0.950942	0.752696	0.439734	0.470142	0.311089	0.593368	0.557343	4.674008	3.530641
	4	0.759199	0.524529	0.381500	0.250929	0.306303	0.229357	0.593330	0.555665	3.731066	3.069473

Table D.II (continued)

n	r	A	A ⁰	B	B ⁰	C	C ⁰	Q _{.90}	Q ⁰ _{.90}	Q _{.99}	Q ⁰ _{.99}
14	5	0.433181	0.328297	0.217895	0.151599	0.324151	0.178919	0.587825	0.552472	3.172015	2.720550
	6	0.279108	0.225878	0.130502	0.092691	0.174643	0.145099	0.576174	0.543504	2.774142	2.463500
	7	0.197252	0.168590	0.078356	0.055197	0.141424	0.120743	0.560786	0.531175	2.469087	2.215152
	8	0.150658	0.133830	0.044950	0.030050	0.117473	0.102261	0.543253	0.516449	2.223001	2.071349
	9	0.122564	0.112916	0.022495	0.012578	0.094266	0.087643	0.524419	0.500144	2.016611	1.851844
	10	0.106122	0.100000	0.006897	0.001146	0.084820	0.075554	0.504625	0.482448	1.837595	1.699608
	11	0.095852	0.092093	-0.004165	-0.008920	0.072905	0.065454	0.483872	0.463261	1.676950	1.558335
	12	0.085757	0.087483	-0.012073	-0.015289	0.062645	0.056334	0.461341	0.441592	1.526497	1.420261
	13	0.086493	0.085282	-0.017639	-0.019771	0.053152	0.046764	0.435055	0.411044	1.373560	1.256763
	2	5.259468	2.254447	2.117889	0.919194	0.963698	0.481586	0.647723	0.556225	6.207424	3.388618
	3	1.725456	1.025563	0.792714	0.466672	0.472348	0.314510	0.549704	0.518430	4.427745	3.389671
	4	0.824573	0.563731	0.408412	0.271304	0.308338	0.230941	0.548291	0.517165	3.522325	2.959642
15	5	0.472356	0.356073	0.239164	0.167878	0.226141	0.180575	0.545653	0.514940	3.066621	2.632763
	6	0.303415	0.243663	0.146721	0.106330	0.176645	0.146840	0.537619	0.508717	2.691585	2.372723
	7	0.212558	0.179303	0.091824	0.066840	0.143475	0.122584	0.525864	0.499258	2.403887	2.154406
	8	0.160007	0.140471	0.056409	0.040155	0.119608	0.104227	0.511841	0.487563	2.177107	1.976614
	9	0.128145	0.116235	0.032403	0.021446	0.101522	0.089767	0.496431	0.474306	1.978378	1.819525
	10	0.108258	0.100817	0.015556	0.007981	0.087249	0.077992	0.480089	0.459858	1.811454	1.677874
	11	0.095676	0.090961	0.003442	-0.001882	0.075597	0.069104	0.462969	0.444318	1.653538	1.549443
	12	0.087744	0.084747	-0.005397	-0.009174	0.065737	0.059523	0.444936	0.427473	1.528480	1.428746
	13	0.082495	0.081018	-0.011974	-0.014554	0.057084	0.051723	0.423420	0.408454	1.400118	1.309464
	14	0.080228	0.079190	-0.015535	-0.018359	0.048941	0.043423	0.402490	0.381721	1.268706	1.165994
	2	5.614554	2.393457	2.191194	0.956168	0.966156	0.482851	0.645331	0.535229	5.900094	3.814216
	3	1.847337	1.098585	0.829902	0.491687	0.474250	0.315918	0.513842	0.485486	4.247769	3.260166
	4	0.889828	0.612647	0.433435	0.290245	0.310088	0.232297	0.509387	0.482723	3.463989	2.858044
	5	0.511450	0.384226	0.257028	0.183103	0.227844	0.181987	0.508472	0.481739	2.969209	2.559722
16	6	0.328367	0.262201	0.161836	0.119035	0.178350	0.149316	0.503178	0.477551	2.613557	2.305614
	7	0.228809	0.191501	0.104398	0.077707	0.145212	0.124136	0.494318	0.470404	2.341208	2.103455
	8	0.170484	0.148248	0.067137	0.049611	0.121402	0.105868	0.481137	0.461094	2.121875	1.932175
	9	0.134577	0.120797	0.041706	0.029774	0.103398	0.091519	0.470490	0.450259	1.939902	1.783535
	10	0.111735	0.102959	0.023721	0.015375	0.089237	0.079884	0.456882	0.438305	1.781870	1.651946
	11	0.096917	0.091726	0.010664	0.004713	0.077731	0.070184	0.442565	0.425435	1.643707	1.533052
	12	0.087234	0.083508	0.001011	-0.003286	0.068107	0.061879	0.427590	0.411663	1.519172	1.423192
	13	0.080558	0.078517	-0.006202	-0.009325	0.059817	0.054554	0.411794	0.396755	1.403830	1.318746
	14	0.077025	0.075450	-0.011599	-0.013865	0.052413	0.047800	0.394655	0.379918	1.292865	1.214524
	15	0.074809	0.073911	-0.015557	-0.017135	0.045343	0.040528	0.374452	0.356273	1.177461	1.089195
	2	5.918144	2.527944	2.259641	0.990671	0.968302	0.483953	0.651730	0.520007	5.619375	3.654580
	3	1.565907	1.169947	0.864627	0.515032	0.475906	0.317054	0.485514	0.457555	4.031917	3.140921
	4	0.953632	0.656116	0.456809	0.307924	0.311608	0.233473	0.475685	0.452575	3.344904	2.763734
	5	0.550447	0.412539	0.274662	0.197328	0.229319	0.183206	0.475573	0.452202	2.876183	2.473959
	6	0.352111	0.281248	0.175980	0.130918	0.179820	0.149585	0.472311	0.449540	2.539892	2.242184

Table D.II (continued)

n	r	A	A ⁰	B	B ⁰	C	C ⁰	Q _{0.90}	Q ⁰ _{0.90}	Q _{0.99}	Q ⁰ _{0.99}
17	7	0.245733	0.204422	0.116181	0.087886	0.146703	0.125462	0.465762	0.444227	2.241275	2.050790
	8	0.181809	0.156897	0.077199	0.054485	0.122932	0.107261	0.456901	0.435951	2.072956	1.988605
	9	0.141972	0.124321	0.050460	0.037609	0.104985	0.092992	0.445522	0.427991	1.839343	1.748154
	10	0.116255	0.101135	0.031430	0.022355	0.090902	0.081456	0.435159	0.418024	1.750700	1.674176
	11	0.099263	0.082593	0.017510	0.010970	0.079500	0.071981	0.423052	0.407228	1.620487	1.512765
	12	0.087888	0.083419	0.007124	0.002340	0.070017	0.053745	0.410399	0.395700	1.501997	1.410820
	13	0.080254	0.077244	-0.000733	-0.002666	0.061930	0.056665	0.397174	0.383477	1.397514	1.315609
	14	0.075187	0.073163	-0.006722	-0.009344	0.054849	0.050333	0.383207	0.370110	1.297718	1.224237
	15	0.071943	0.070603	-0.011284	-0.013224	0.048435	0.044423	0.368014	0.355085	1.200720	1.132314
	16	0.070077	0.069292	-0.014635	-0.016064	0.042235	0.037995	0.350057	0.334006	1.098947	1.021120
	17	6.211586	2.658180	2.323825	1.023009	0.970192	0.484922	0.665367	0.509604	5.361800	3.507796
	2	2.081279	1.239711	0.897189	0.536912	0.477363	0.318051	0.460707	0.433873	3.928523	3.030365
	3	1.016308	0.699035	0.479777	0.324499	0.312941	0.234502	0.446433	0.426104	3.234069	2.675926
	4	0.589197	0.440859	0.291211	0.210673	0.230609	0.184270	0.446371	0.425848	2.799969	2.402014
	5	0.379264	0.300621	0.189265	0.147075	0.181102	0.150688	0.444563	0.424286	2.470345	2.182253
	6	0.263129	0.217870	0.127260	0.097454	0.147997	0.125610	0.439848	0.420425	2.224130	2.000500
	7	0.193770	0.161190	0.086678	0.068840	0.124253	0.103461	0.432893	0.414625	2.025680	1.846427
	8	0.150110	0.132495	0.059718	0.049999	0.106346	0.092252	0.424396	0.407373	1.860351	1.713096
	9	0.121594	0.110128	0.038718	0.028956	0.092320	0.082788	0.414359	0.399054	1.719002	1.595629
	10	0.102484	0.094808	0.024004	0.016906	0.080991	0.073302	0.404599	0.389931	1.595520	1.490440
	11	0.089462	0.084242	0.012947	0.007703	0.071603	0.065278	0.393798	0.380153	1.485551	1.394752
	12	0.080515	0.076929	0.004509	0.000589	0.063644	0.058349	0.382527	0.369771	1.385835	1.306269
	13	0.074372	0.071898	-0.002000	-0.004953	0.056747	0.052237	0.370750	0.358725	1.293618	1.222869
	14	0.070212	0.068510	-0.007047	-0.009278	0.050624	0.046704	0.358296	0.346781	1.206316	1.142183
	15	0.067498	0.066346	-0.010951	-0.012611	0.045010	0.041485	0.344720	0.333280	1.120714	1.060437
	16	0.065908	0.065216	-0.013904	-0.015119	0.039524	0.035760	0.328641	0.314358	1.030307	0.961054
18	2	6.494147	2.704419	2.384241	1.053435	0.971869	0.485780	0.685006	0.503252	5.124511	3.372274
	3	2.193580	1.307840	0.927837	0.557497	0.478653	0.318933	0.461677	0.413822	3.786148	2.927771
	4	1.077217	0.741336	0.499374	0.340095	0.314119	0.234409	0.421012	0.402804	3.130615	2.593937
	5	0.627596	0.469074	0.306798	0.223236	0.231747	0.185206	0.420381	0.402262	2.709043	2.334459
	6	0.404989	0.320188	0.201785	0.152586	0.182230	0.151656	0.419549	0.401449	2.404643	2.125602
	7	0.280845	0.231658	0.137710	0.106476	0.149132	0.127614	0.416277	0.398730	2.169714	1.952562
	8	0.206205	0.175993	0.095629	0.074726	0.125408	0.109505	0.410888	0.394220	1.980191	1.805768
	9	0.158226	0.137458	0.066527	0.051997	0.107533	0.095343	0.403965	0.388312	1.822290	1.678760
	10	0.127581	0.114770	0.045623	0.035209	0.093546	0.083934	0.395976	0.381356	1.697399	1.566990
	11	0.106405	0.097730	0.030170	0.022544	0.082769	0.074513	0.387243	0.373614	1.569767	1.467128
	12	0.081777	0.085799	0.018493	0.012812	0.072949	0.065570	0.377967	0.365254	1.465329	1.376630
	13	0.081352	0.077362	0.009522	0.009235	0.065077	0.059743	0.368259	0.356367	1.371077	1.293457
	14	0.074369	0.071438	0.002543	-0.000722	0.058297	0.053766	0.358148	0.346968	1.284616	1.215851
	15	0.069341	0.067276	-0.002930	-0.005431	0.052340	0.048437	0.347584	0.336984	1.203876	1.142123
	16	0.065275	0.064425	-0.007237	-0.009156	0.046988	0.043552	0.336398	0.326190	1.126779	1.070292
	17	0.063577	0.062575	-0.010613	-0.012081	0.042029	0.038908	0.324183	0.313984	1.050608	0.997068

Table D.II (continued)

r	r	A	A ⁰	B	B ⁰	C	C ⁰	Q _{.90}	Q ⁰ _{.90}	Q _{.99}	Q ⁰ _{.99}
18	2	0.662208	0.061592	-0.013200	-0.014279	0.037138	0.033774	0.302689	0.296894	0.969538	0.907662
19	2	6.768016	2.906904	2.441302	1.082159	0.973368	0.485546	0.709650	0.500734	4.905119	3.246692
	3	2.302943	1.374393	0.956781	0.576928	0.479803	0.319719	0.426525	0.396896	3.653575	2.832170
	4	1.138147	0.782978	0.518870	0.354821	0.315168	0.216216	0.399914	0.382757	3.013789	2.517176
	5	0.665572	0.497104	0.371524	0.235101	0.232758	0.185037	0.397194	0.381097	2.612928	2.270901
	6	0.430438	0.339847	0.213620	0.162518	0.183230	0.152512	0.396943	0.380742	2.342509	2.072005
	7	0.258765	0.245791	0.147536	0.115008	0.150136	0.123499	0.394786	0.378708	2.117916	1.906897
	8	0.218990	0.186178	0.104105	0.082192	0.126425	0.110423	0.392681	0.375454	1.936533	1.746495
	9	0.167589	0.146782	0.073930	0.058609	0.108573	0.096299	0.395079	0.370668	1.785360	1.645169
	10	0.134084	0.119932	0.052177	0.041144	0.094617	0.084932	0.378402	0.364859	1.556258	1.538662
	11	0.110891	0.101214	0.036033	0.027904	0.083379	0.075561	0.370961	0.354276	1.543796	1.443461
	12	0.084694	0.087954	0.023779	0.017693	0.074108	0.067677	0.362967	0.351094	1.444155	1.357403
	13	0.083220	0.078461	0.014314	0.009578	0.066300	0.060923	0.354550	0.343423	1.354523	1.278626
	14	0.075025	0.071632	0.006904	0.003342	0.059600	0.055039	0.345775	0.335316	1.272719	1.205585
	15	0.069159	0.066725	0.001045	-0.001711	0.053749	0.049828	0.336548	0.326766	1.196949	1.136905
	16	0.064582	0.063235	-0.003615	-0.005759	0.048548	0.045129	0.327110	0.317693	1.125594	1.071204
	17	0.062058	0.060809	-0.007331	-0.008999	0.043827	0.040791	0.317000	0.307884	1.056949	1.006799
	18	0.060090	0.059212	-0.010278	-0.011572	0.039413	0.036678	0.305942	0.296787	0.988678	0.940788
	19	0.058901	0.058351	-0.012563	-0.013527	0.035022	0.031996	0.292800	0.281268	0.915596	0.859891
20	2	7.033320	3.025855	2.495356	1.109360	0.974715	0.487233	0.738490	0.500342	4.701608	3.129932
	3	2.409504	1.439417	0.984196	0.595327	0.480836	0.370423	0.414924	0.347678	3.529763	2.742818
	4	1.197301	0.821938	0.537337	0.369765	0.316109	0.236938	0.379713	0.364114	2.942937	2.445125
	5	0.703077	0.524893	0.335478	0.246339	0.233662	0.186778	0.376480	0.362060	2.561194	2.217987
	6	0.455986	0.355521	0.224839	0.171930	0.184177	0.153276	0.376466	0.361422	2.283674	2.071240
	7	0.316802	0.260644	0.156972	0.123098	0.151029	0.129286	0.375148	0.360756	2.058601	1.863398
	8	0.232030	0.196651	0.112149	0.089276	0.127329	0.111237	0.372092	0.358143	1.894488	1.729210
	9	0.177498	0.154469	0.089962	0.064899	0.109494	0.097142	0.367601	0.354317	1.749654	1.613038
	10	0.140997	0.125512	0.053411	0.046788	0.095561	0.085809	0.362040	0.349480	1.625802	1.510884
	11	0.115834	0.105157	0.041618	0.033010	0.084354	0.076478	0.355703	0.343842	1.517980	1.419825
	12	0.098103	0.090598	0.028873	0.022330	0.075171	0.068639	0.348801	0.337694	1.427578	1.337651
	13	0.085409	0.080055	0.018896	0.013928	0.067358	0.061079	0.341473	0.330338	1.336942	1.262633
	14	0.076224	0.072363	0.011086	0.007241	0.060716	0.055124	0.333805	0.323984	1.259048	1.193367
	15	0.063542	0.062635	0.004873	0.001872	0.056940	0.050996	0.325834	0.316540	1.197312	1.128656
	16	0.064679	0.062631	-0.000108	-0.002444	0.049837	0.046410	0.317549	0.308748	1.170296	1.047394
	17	0.061165	0.059670	-0.004122	-0.005978	0.045254	0.042736	0.308888	0.300462	1.056722	1.008435
	18	0.058671	0.057584	-0.007357	-0.008821	0.041056	0.038352	0.299698	0.291505	0.995162	0.950123
	19	0.056570	0.056193	-0.009957	-0.011101	0.037098	0.034598	0.289432	0.281367	0.933587	0.890475
	20	0.055929	0.055433	-0.011984	-0.012851	0.033133	0.030396	0.277655	0.267204	0.867323	0.816896
21	2	7.290623	3.141483	2.546703	1.135190	0.975932	0.487854	0.770861	0.502858	4.512268	3.021048
	3	2.513392	1.502965	1.010235	0.612796	0.481769	0.371058	0.405344	0.370817	3.413820	2.659000
	4	1.255295	0.864207	0.554878	0.382006	0.316957	0.237588	0.363052	0.348084	2.857488	2.377335

Table D.II (continued)

n	r	A	A ⁰	B	H ⁰	C	C ⁰	Q _{.90}	Q ⁰ _{.90}	Q _{.99}	Q ⁰ _{.99}
22	5	0.740078	0.552399	0.349735	0.257013	0.234476	0.187445	0.357941	0.344904	2.493460	2.154401
	6	0.481326	0.379154	0.235501	0.180872	0.184924	0.153960	0.357981	0.344777	2.227891	1.973094
	7	0.334887	0.274447	0.165837	0.130789	0.151831	0.129991	0.357168	0.344099	2.021625	1.821944
	8	0.245249	0.207337	0.119802	0.094014	0.128138	0.111964	0.354960	0.342203	1.854604	1.693279
	9	0.187274	0.162442	0.087658	0.070887	0.110315	0.097893	0.351402	0.339145	1.715216	1.581814
	10	0.148238	0.131428	0.064352	0.052166	0.096401	0.086588	0.346795	0.335135	1.596157	1.483706
	11	0.121148	0.109476	0.046946	0.037881	0.085217	0.077287	0.341409	0.330719	1.492541	1.396465
	12	0.101916	0.093647	0.033641	0.026770	0.076013	0.069485	0.335445	0.325042	1.400940	1.317743
	13	0.088028	0.082078	0.023282	0.017996	0.068286	0.062827	0.329051	0.319247	1.319848	1.244010
	14	0.077875	0.073542	0.015097	0.010982	0.061697	0.057060	0.322320	0.313075	1.244163	1.179969
	15	0.070394	0.067211	0.008554	0.005321	0.055965	0.051995	0.315307	0.306572	1.175981	1.118534
	16	0.064864	0.062511	0.003278	0.000719	0.050930	0.047486	0.308031	0.297750	1.112443	1.060740
23	17	0.060780	0.059036	-0.001005	-0.003040	0.046438	0.043414	0.300472	0.292591	1.052713	1.005737
	18	0.057791	0.056498	-0.004494	-0.006116	0.042366	0.039682	0.292567	0.284992	0.995668	0.952498
	19	0.055642	0.054690	-0.007336	-0.008629	0.038607	0.036183	0.284171	0.276765	0.940111	0.899769
	20	0.054160	0.053469	-0.009637	-0.010663	0.035037	0.032179	0.274964	0.267462	0.894247	0.845232
	21	0.053242	0.052794	-0.011455	-0.012239	0.031436	0.028949	0.263997	0.254480	0.823970	0.777996
	22	7.540436	3.253976	2.595597	1.159779	0.977038	0.498417	0.806213	0.507534	4.335635	2.919230
	2	2.614335	1.565091	1.035026	0.629423	0.482615	0.321633	0.400392	0.361022	3.304975	2.580402
	3	1.312151	0.903782	0.571579	0.394608	0.317725	0.239177	0.348631	0.333918	2.776943	2.313413
	4	0.776555	0.577595	0.361358	0.267174	0.235213	0.183047	0.341333	0.329418	2.429384	2.100860
	5	0.506469	0.398701	0.245657	0.189387	0.185648	0.154578	0.340983	0.329128	2.174977	1.927372
	6	0.352567	0.238888	0.174382	0.138113	0.152553	0.130625	0.340674	0.328183	1.976541	1.782414
	7	0.258586	0.218177	0.127099	0.102437	0.128865	0.112616	0.337142	0.327443	1.816209	1.658846
	8	0.197252	0.170637	0.094046	0.076598	0.111053	0.099566	0.336366	0.325045	1.692037	1.551712
	9	0.155739	0.137516	0.070024	0.057300	0.097153	0.087283	0.332576	0.321741	1.547388	1.457474
	10	0.126765	0.114102	0.052038	0.042535	0.085988	0.079004	0.329010	0.317709	1.457618	1.373531
24	11	0.106064	0.097032	0.038252	0.031018	0.076806	0.070234	0.322862	0.313107	1.379463	1.297916
	12	0.091005	0.084458	0.027484	0.021893	0.069107	0.063610	0.317275	0.308052	1.300542	1.279104
	13	0.079003	0.075097	0.019497	0.014572	0.062542	0.057881	0.311350	0.302632	1.229055	1.145879
	14	0.071041	0.068078	0.017095	0.012095	0.056860	0.052362	0.305151	0.296902	1.163591	1.107243
	15	0.065457	0.062797	0.015543	0.0103791	0.051875	0.048410	0.298712	0.290891	1.103010	1.052343
	16	0.060820	0.058824	0.012011	-0.000193	0.047446	0.044411	0.292042	0.284600	1.046337	1.000407
	17	0.057353	0.055853	-0.001707	-0.003480	0.043458	0.040773	0.285115	0.277997	0.992690	0.950685
	18	0.054785	0.053657	-0.004766	-0.006195	0.039815	0.037412	0.277865	0.270999	0.941190	0.902344
	19	0.052918	0.052076	-0.007281	-0.008431	0.036427	0.034242	0.270161	0.263431	0.890758	0.854258
	20	0.051616	0.050997	-0.009334	-0.010257	0.033189	0.031140	0.261702	0.254860	0.839823	0.804333
	21	0.050394	0.050394	-0.010970	-0.011693	0.029905	0.027533	0.251617	0.242913	0.784553	0.742633
	22	7.783723	3.363513	2.642260	1.183240	0.978046	0.488930	0.844089	0.514079	4.170447	2.823779
25	2	2.713654	1.625850	1.058682	0.645285	0.483385	0.322156	0.396743	0.353044	3.202559	2.506310
	3	1.367897	0.942670	0.587515	0.406630	0.318424	0.239711	0.336192	0.321406	2.700864	2.253012
	4	0.812499	0.606459	0.371405	0.276868	0.235883	0.188594	0.321447	0.315421	2.368661	2.050109

Table D.II (continued)

n	r	A	A ⁰	B	B ⁰	C	C ⁰	Q _{0.90}	Q _{0.90}	Q _{0.99}
6	0.531383	0.418128	0.255351	0.197513	0.186306	0.155139	0.325597	0.314820	2.124570	1.893893
7	0.371001	0.303145	0.182493	0.145107	0.153208	0.131200	0.325518	0.314674	1.914110	1.744687
8	0.271994	0.229125	0.134069	0.108570	0.129574	0.113206	0.324514	0.313771	1.779425	1.624843
9	0.207380	0.179003	0.109151	0.082055	0.111719	0.099173	0.322391	0.311923	1.650094	1.522713
10	0.163446	0.144022	0.075449	0.062209	0.097831	0.087909	0.319299	0.309221	1.539526	1.431959
11	0.132629	0.118380	0.056912	0.046989	0.086680	0.078555	0.315445	0.305817	1.443295	1.351116
12	0.110488	0.100696	0.047668	0.035087	0.077517	0.070905	0.311007	0.301851	1.358292	1.278325
13	0.094282	0.087139	0.031514	0.025631	0.069840	0.054307	0.306124	0.297439	1.282246	1.212141
14	0.082250	0.076969	0.022644	0.018021	0.063300	0.058609	0.300899	0.292668	1.213444	1.151470
15	0.073222	0.069777	0.015501	0.011831	0.057650	0.053626	0.295402	0.287599	1.150555	1.095277
16	0.066398	0.063427	0.009691	0.006753	0.052703	0.049216	0.289677	0.282271	1.092509	1.042777
17	0.061219	0.058968	0.006927	0.002559	0.048321	0.045269	0.283745	0.276791	0.938416	0.993385
18	0.057287	0.055576	0.004997	-0.000421	0.044391	0.041697	0.277406	0.270891	0.987499	0.946418
19	0.054314	0.053011	-0.002259	-0.003817	0.040826	0.038424	0.271230	0.264716	0.939031	0.901240
20	0.052088	0.051097	-0.004961	-0.005229	0.037546	0.035382	0.264457	0.258309	0.892260	0.857127
21	0.050454	0.049704	-0.007201	-0.008232	0.034476	0.032495	0.257456	0.251317	0.844267	0.813076
22	0.049302	0.048745	-0.009045	-0.009879	0.031524	0.029656	0.249654	0.243396	0.799614	0.767183
23	0.048575	0.048203	-0.010525	-0.011175	0.028514	0.026432	0.240344	0.233252	0.748807	0.710344
24	2	8.019406	3.470256	2.686884	1.205671	0.978970	0.499399	0.884105	0.522246	2.734091
3	1.810263	1.685296	1.081302	0.660447	0.484091	0.322635	0.325120	0.395120	0.346672	2.436387
4	1.422564	0.980880	0.602753	0.418122	0.319063	0.239200	0.325516	0.325516	0.310357	2.195928
5	1.147903	0.632980	0.384925	0.286136	0.236494	0.189093	0.313100	0.313100	0.302757	2.001923
6	0.956047	0.437411	0.244623	0.205283	0.186906	0.155549	0.311570	0.311570	0.301717	1.842449
7	0.808957	0.317784	0.190253	0.151795	0.153805	0.131722	0.311569	0.311569	0.301656	1.893297
8	0.285435	0.240141	0.140734	0.114432	0.130123	0.113742	0.310966	0.310966	0.301087	1.744167
9	0.217616	0.187499	0.105996	0.087279	0.112324	0.099723	0.309382	0.309382	0.299693	1.694789
10	0.171314	0.150602	0.080646	0.066911	0.098445	0.088175	0.306888	0.306888	0.297506	1.607258
11	0.138651	0.124067	0.061584	0.051258	0.087306	0.077238	0.303652	0.303652	0.294644	1.419621
12	0.115142	0.104593	0.046906	0.038990	0.078158	0.071508	0.299835	0.299835	0.291234	1.337520
13	0.097811	0.090073	0.035384	0.029270	0.070498	0.064731	0.295570	0.295570	0.287383	1.264102
14	0.084866	0.079110	0.026198	0.021336	0.063980	0.057359	0.290959	0.290959	0.283178	1.197735
15	0.075086	0.070757	0.018780	0.014904	0.058354	0.054304	0.286074	0.286074	0.279683	1.137151
16	0.067633	0.064349	0.017277	0.009609	0.053437	0.049727	0.280965	0.280965	0.273940	1.081340
17	0.061924	0.059416	0.007745	0.005220	0.050090	0.046020	0.275664	0.275664	0.268977	1.029473
18	0.057538	0.055613	0.003617	0.001560	0.045204	0.042497	0.270180	0.270180	0.263800	0.980842
19	0.054171	0.052689	0.000178	-0.001503	0.041693	0.039285	0.264508	0.264508	0.258399	0.934812
20	0.051598	0.050457	-0.002695	-0.004073	0.038485	0.036324	0.258619	0.258619	0.252738	0.890783
21	0.049653	0.048776	-0.005098	-0.006729	0.035515	0.033555	0.252450	0.252450	0.246740	0.848093
22	0.048212	0.047542	-0.007105	-0.008033	0.032719	0.030714	0.245883	0.245883	0.240250	0.805956
23	0.047188	0.046684	-0.009768	-0.009526	0.030016	0.028005	0.239660	0.239660	0.233897	0.763048
24	0.046535	0.046194	-0.010114	-0.010709	0.027247	0.025330	0.230037	0.230037	0.222670	0.716169
25	2	8.249372	3.574357	2.729640	1.227157	0.979819	0.489831	0.925937	0.531826	2.649639
3	2.904612	1.743482	1.102970	0.674959	0.484738	0.323074	0.395285	0.395285	0.341725	2.370267

Table D.II (continued)

r	A	A ⁰	B	B ⁰	C	C ⁰	Q ⁰ .90	Q ⁰ .99	Q ⁰ .99
4	1.476105	1.018425	0.617349	0.429129	0.319649	0.239648	0.316412	0.300644	2.560606
5	0.882770	0.659151	0.395961	0.295012	0.237055	0.189551	0.301136	0.291292	2.256217
6	0.580445	0.456530	0.273506	0.212726	0.187455	0.156116	0.293768	0.289702	2.030919
7	0.406810	0.332180	0.197690	0.158204	0.154391	0.132200	0.298715	0.289626	1.854278
8	0.258879	0.251196	0.147134	0.120764	0.130670	0.114231	0.298399	0.289370	1.710353
9	0.227927	0.196091	0.111602	0.092288	0.112876	0.100224	0.297256	0.288280	1.589758
10	0.179308	0.157321	0.085632	0.071421	0.099004	0.084990	0.295271	0.286531	1.496523
11	0.144919	0.129324	0.066069	0.055356	0.087875	0.079768	0.292572	0.284139	1.396618
12	0.119986	0.108685	0.050576	0.042740	0.078738	0.072053	0.289300	0.281215	1.317205
13	0.101552	0.093720	0.039104	0.032670	0.071093	0.064595	0.285580	0.277857	1.246209
14	0.087711	0.081480	0.029618	0.024526	0.064592	0.059843	0.281510	0.274149	1.182068
15	0.077191	0.072478	0.021939	0.017264	0.058986	0.054911	0.277164	0.270156	1.123574
16	0.069122	0.065524	0.015455	0.012365	0.054093	0.050561	0.272595	0.265922	1.069763
17	0.062891	0.060124	0.010467	0.007791	0.049773	0.046685	0.267839	0.261480	1.019856
18	0.058059	0.055919	0.006153	0.003963	0.045921	0.043198	0.262916	0.256847	0.973196
19	0.054307	0.052645	0.002545	0.000744	0.042451	0.04032	0.257832	0.252024	0.929215
20	0.051398	0.050105	-0.000486	-0.001972	0.039293	0.037128	0.252572	0.246998	0.887367
21	0.049153	0.048148	-0.003038	-0.004266	0.036391	0.034435	0.247117	0.241731	0.847188
22	0.047443	0.046661	-0.005189	-0.006205	0.033687	0.031903	0.241393	0.236152	0.808044
23	0.046165	0.045562	-0.006997	-0.007837	0.031129	0.029478	0.235299	0.230114	0.769272
24	0.045249	0.044791	-0.008505	-0.009196	0.028644	0.027070	0.228589	0.223270	0.729656
25	0.044646	0.044347	-0.009733	-0.010281	0.026087	0.024317	0.220562	0.213764	0.686237

Table D.III - Cramér-Rao Efficiencies of BLI Estimates of 10 Percent Points of the Extreme-Value Distribution, Where $\frac{n-r}{n}$ of the Size n Ordered Sample is Censored From Above, $2 \leq n \leq 18$, $2 \leq r \leq n$

n/r	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
2	.835																
3	.892	.862															
4	.912	.915	.883														
5	.925	.918	.918	.898													
6	.932	.928	.927	.928	.910												
7	.933	.936	.934	.936	.936	.919											
8	.929	.942	.940	.941	.943	.943	.927										
9	.920	.947	.945	.945	.947	.948	.948	.933									
10	.907	.950	.949	.949	.950	.952	.953	.952	.938								
11	.891	.952	.953	.952	.953	.954	.956	.957	.956	.943							
12	.872	.952	.955	.955	.956	.957	.958	.959	.960	.959	.946						
13		.951	.959	.958	.958	.959	.960	.961	.962	.963	.952	.950					
14	.852	.948	.961	.961	.960	.961	.962	.963	.963	.965	.965	.964	.953				
15	.812	.944	.962	.963	.962	.963	.963	.964	.965	.966	.967	.967	.966	.955			
16	.792	.939	.963	.965	.964	.964	.965	.966	.967	.968	.968	.969	.969	.968	.957		
17	.773	.932	.963	.967	.966	.966	.966	.967	.968	.969	.970	.970	.971	.971	.969	.959	
18	.755	.925	.963	.968	.968	.967	.968	.968	.969	.970	.971	.971	.972	.972	.972	.971	.961

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<p>This report gives results concerning estimation of location and scale parameters. Most of the work pertains to the first extreme-value distribution of smallest values, the distribution of the natural logarithms of failure times having the two-parameter Weibull distribution. Experimental designs are derived, under the assumption that log failure times are polynomial functions of the reciprocal of stress level and have the extreme-value distribution, for over-stress life tests. These designs yield least-squares curves with minimum variance at a specified (nominal) stress level below the levels at which the life test is conducted. An estimate of the extreme-value location parameter u associated with the nominal stress level and the relationship between u and stress level can be obtained from the least-squares curve. Other extreme-value results apply to a life test conducted at a single fixed stress level.</p>		

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